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ТИПОВЫЕ КОНСТРУКЦИИ, ИЗДЕЛИЯ И УЗЛЫ ЗДАНИЙ И СООРУЖЕНИЙ

СЕРИЯ 1.020.1-4

КОНСТРУКЦИИ РАМНОГО КАРКАСА МЕЖВИДОВОГО ПРИМЕНЕНИЯ ДЛЯ МНОГОЭТАЖНЫХ ОБЩЕСТВЕННЫХ ЗДАНИЙ, ПРОИЗВОДСТВЕННЫХ И ВСПОМОГАТЕЛЬНЫХ ЗДАНИЙ ПРОМЫШЛЕННЫХ ПРЕДПРИЯТИЙ

выпуск 0-9

Указания по подбору элементов каркаса.

(Вариант армирования изделий сталью классов Ат-IVС и Врп-I).

часть 3

стр. 240÷330

24166-03
Цена 7-07

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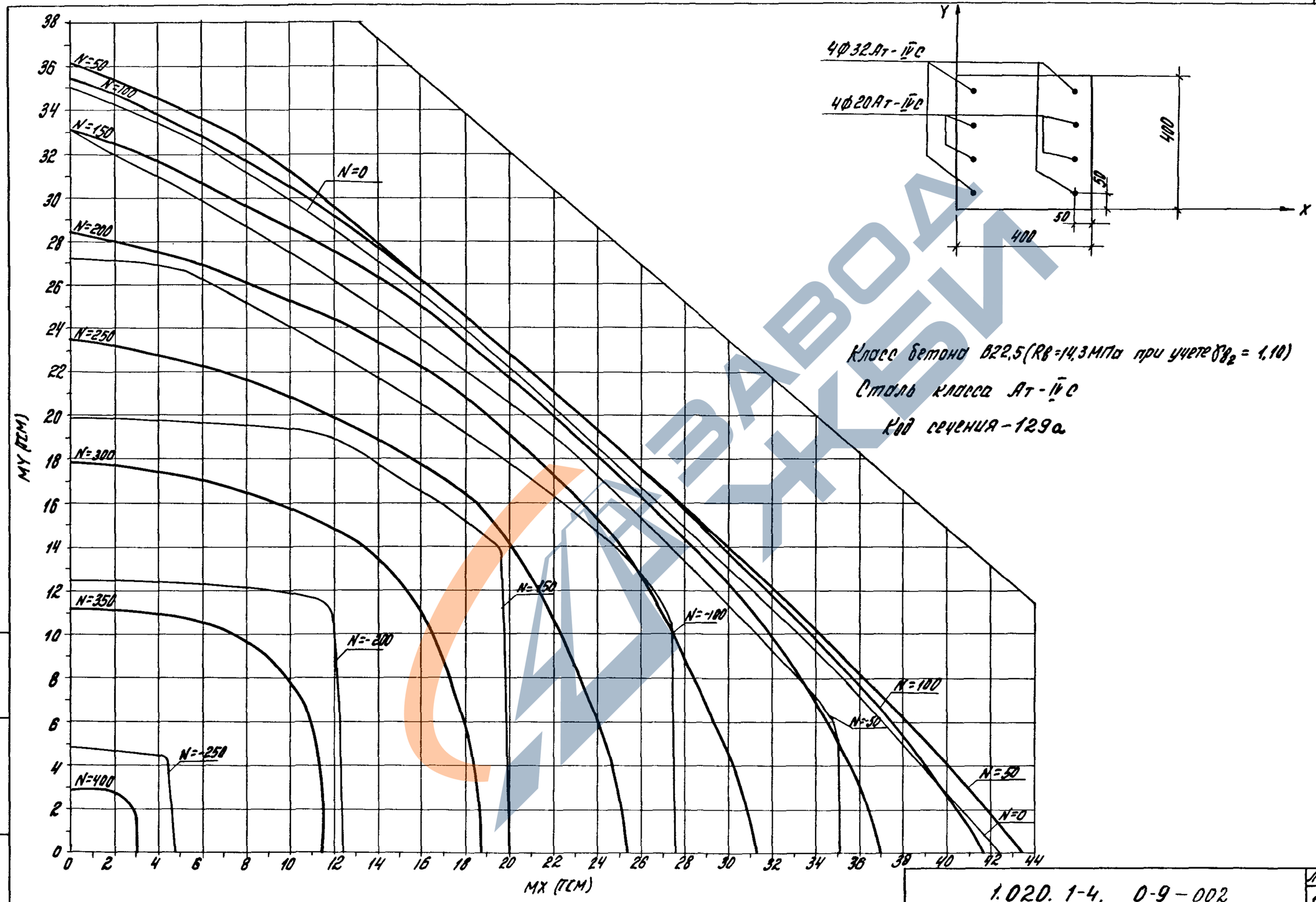

Класс бетона В22,5 (R_B = 14,3 МПа при учете γ_{B2} = 1,10)

Сталь класса Ат-IVС

Код сечения – 129а

Инв. № подл. | Подпись и дата | Взам. инв. №		
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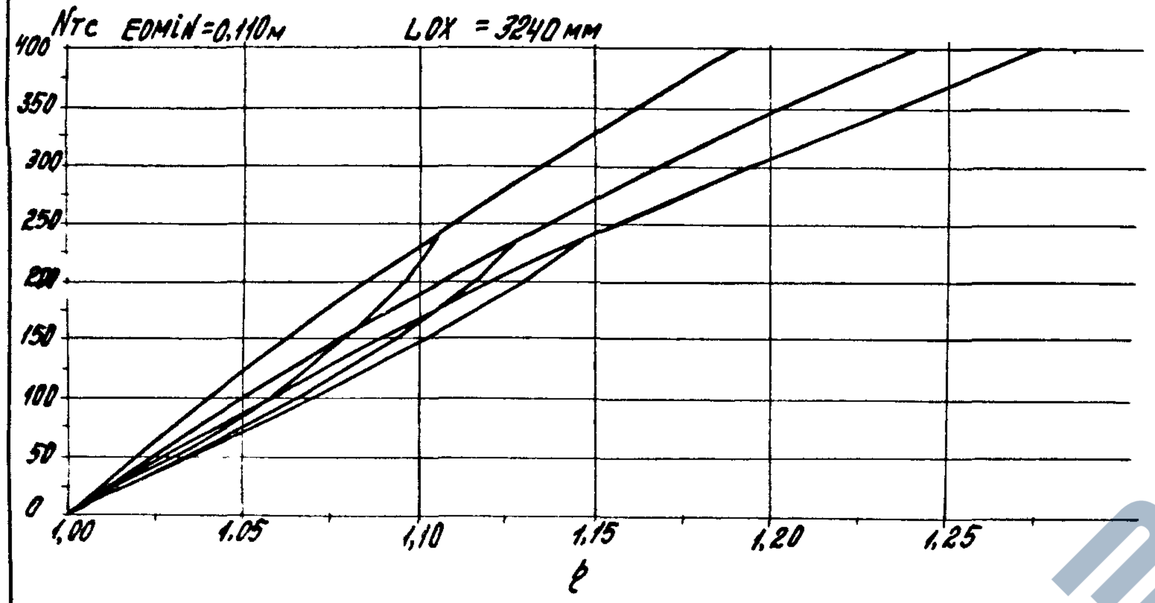

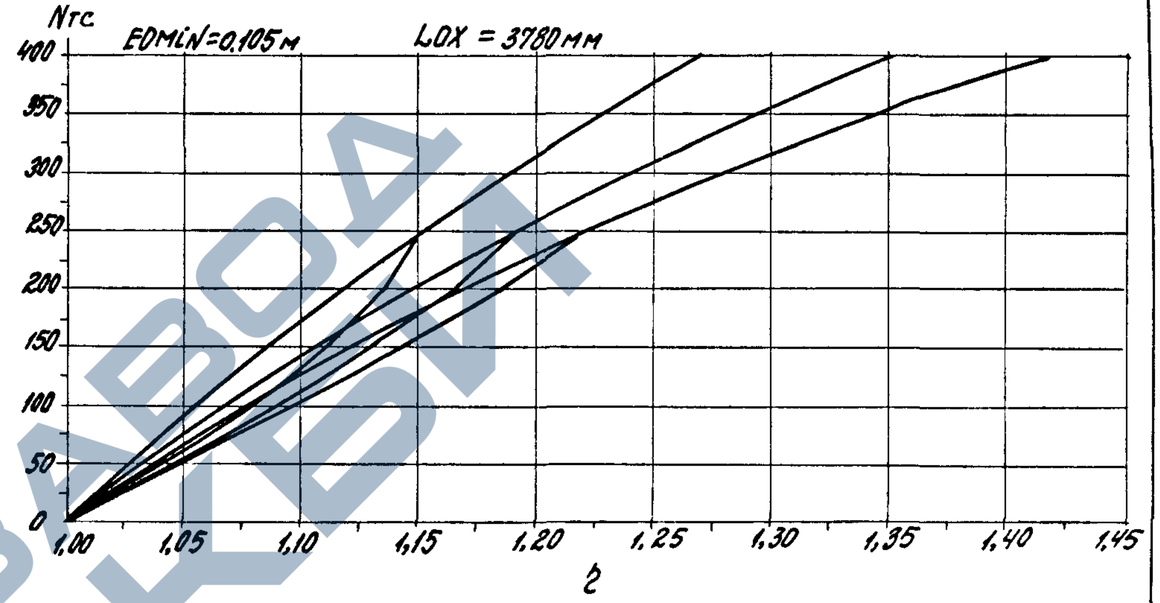

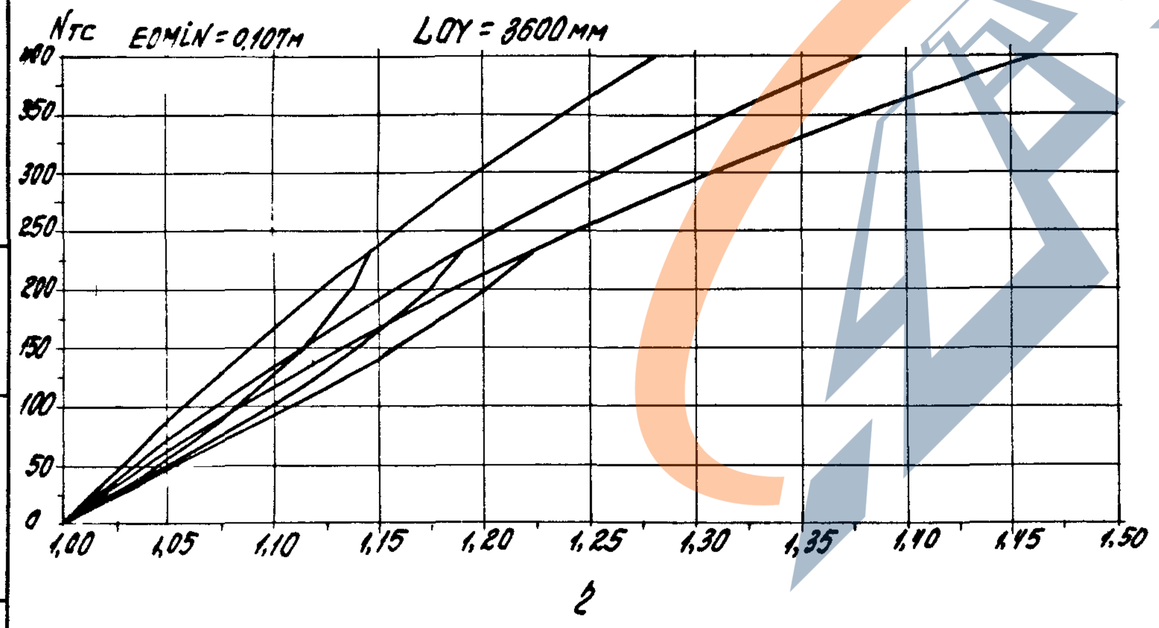

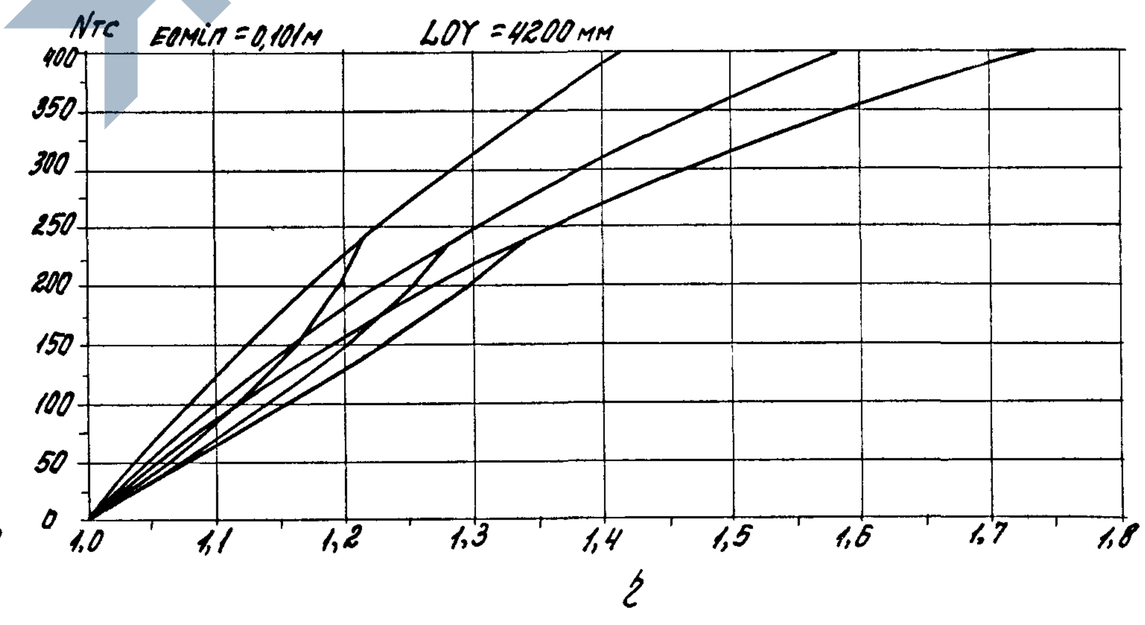

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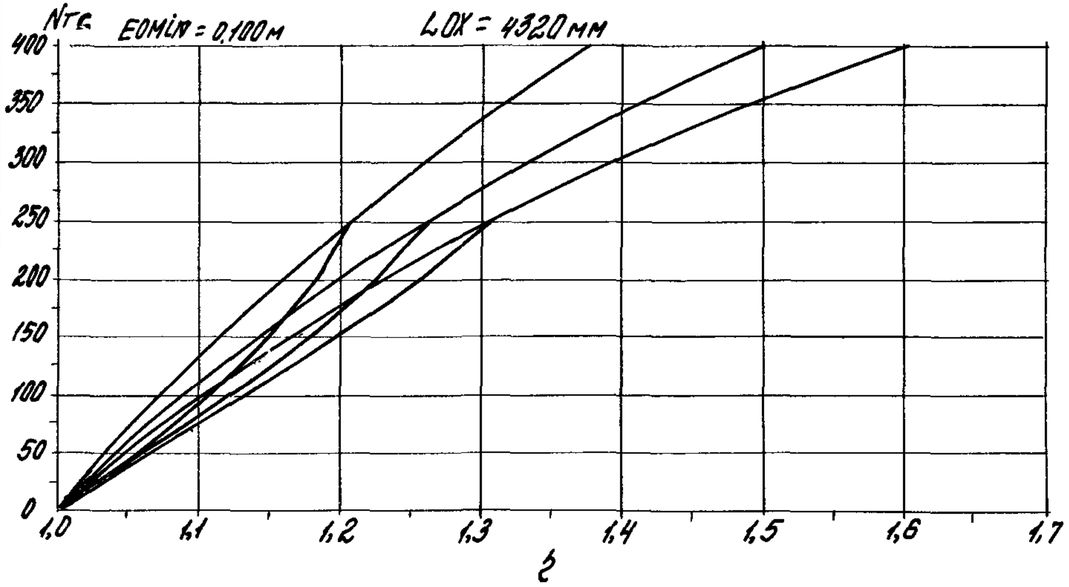

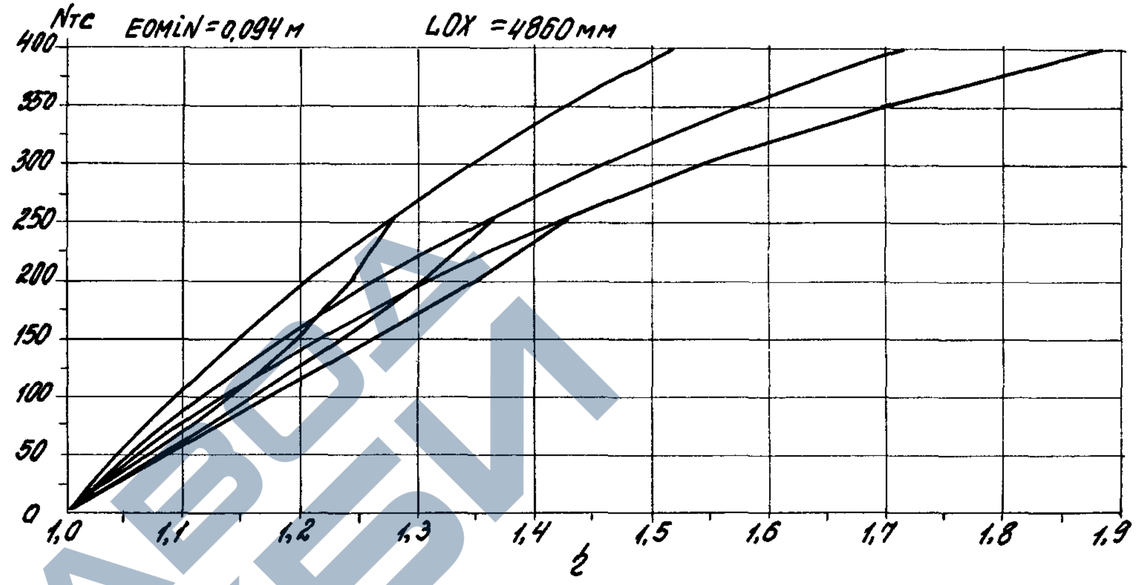

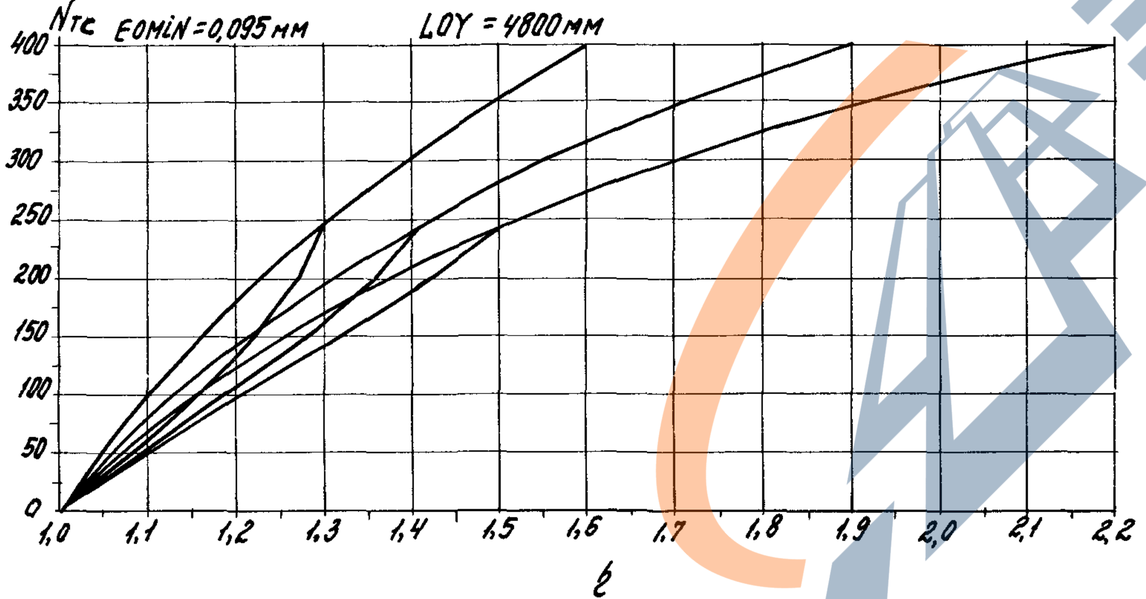

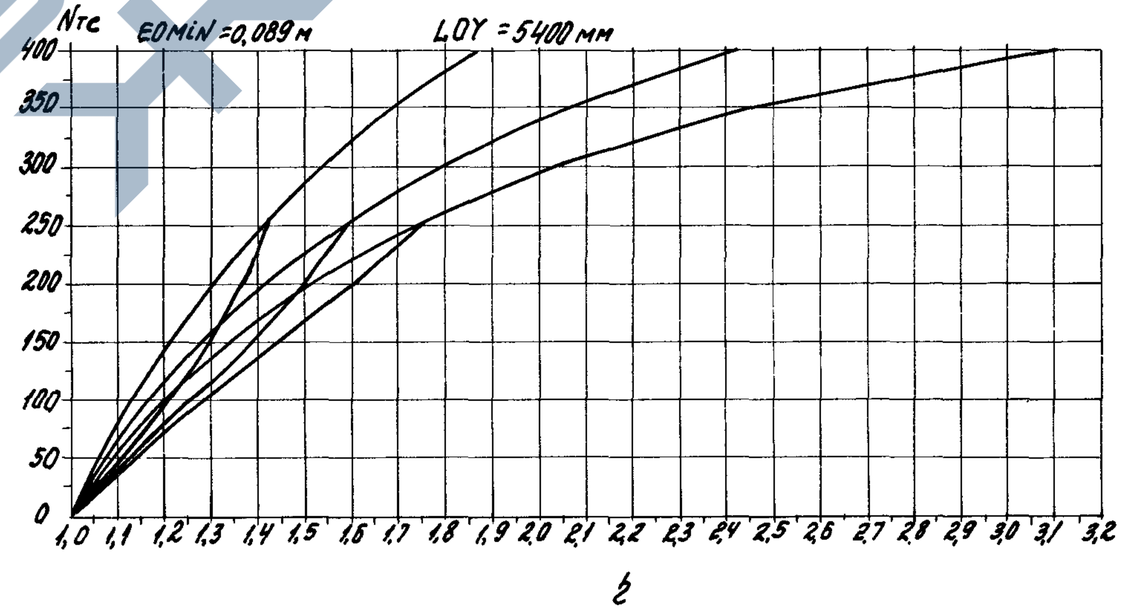

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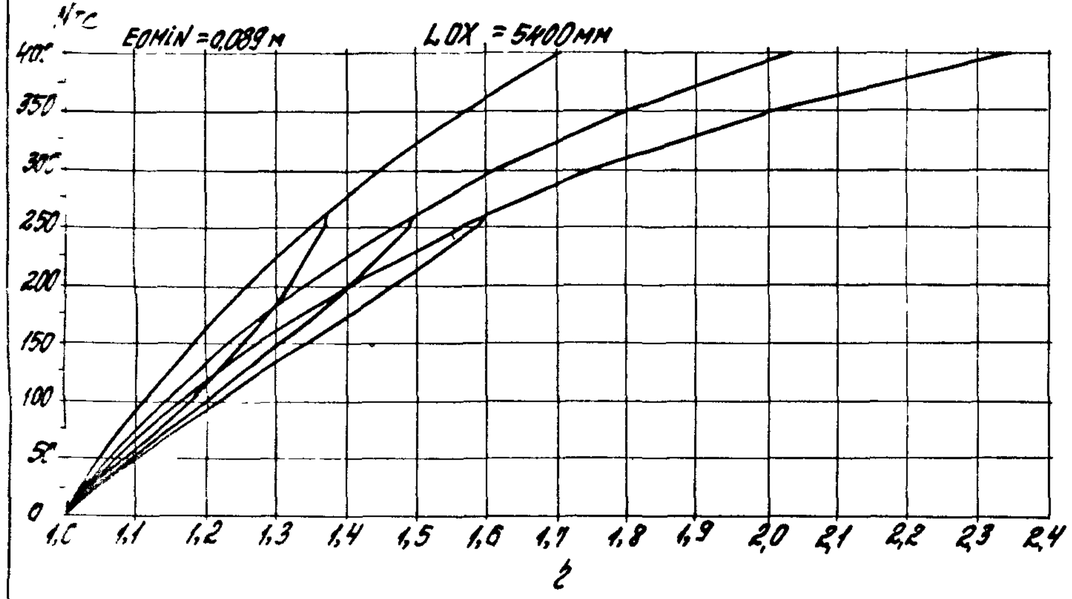

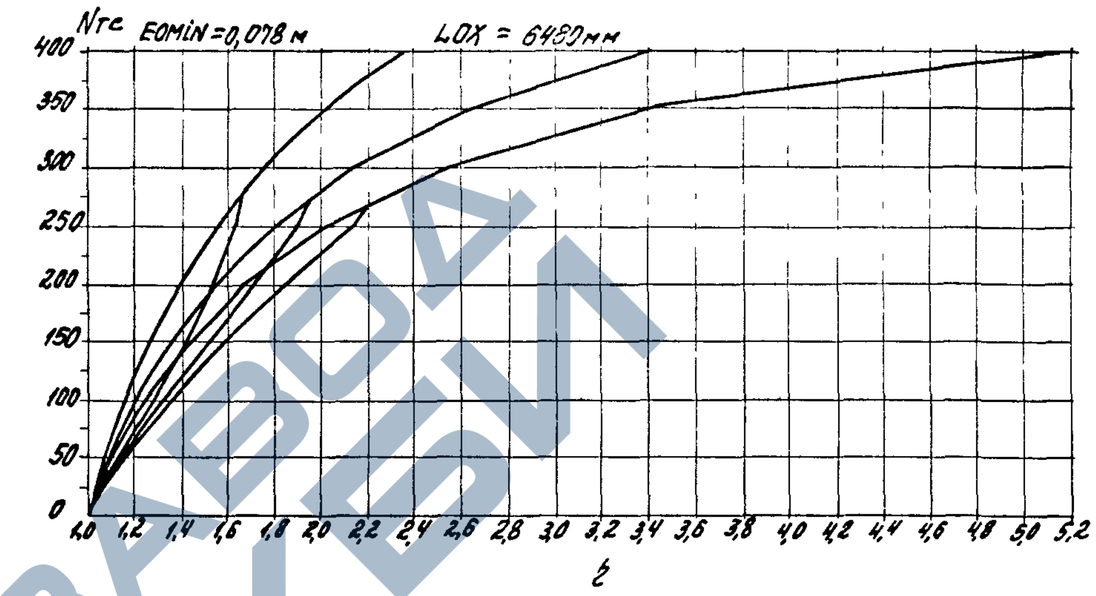

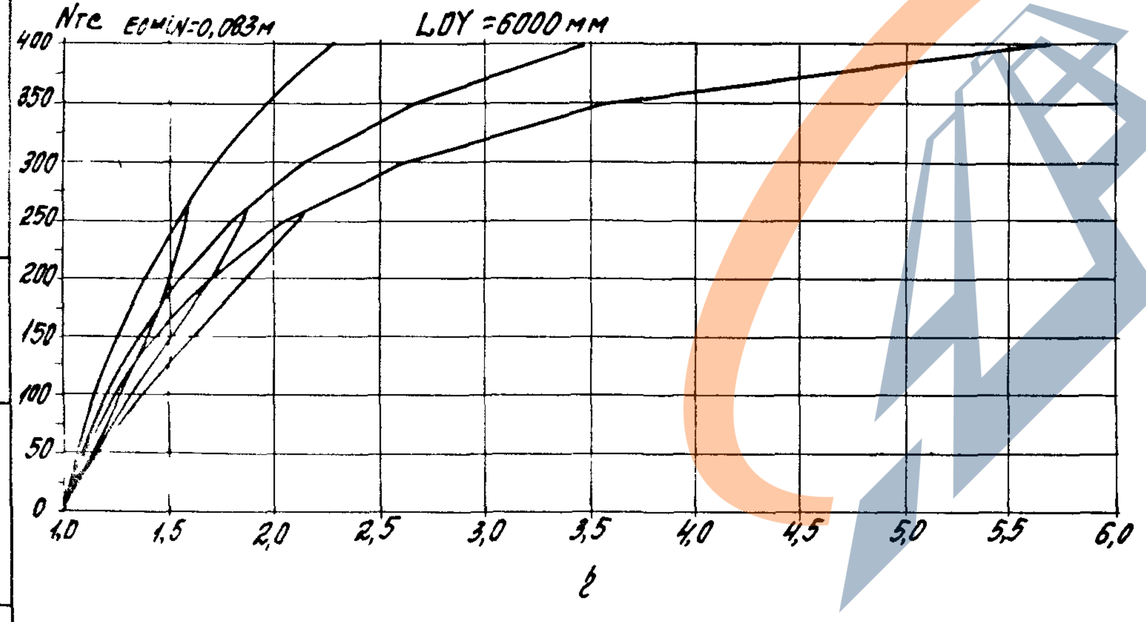

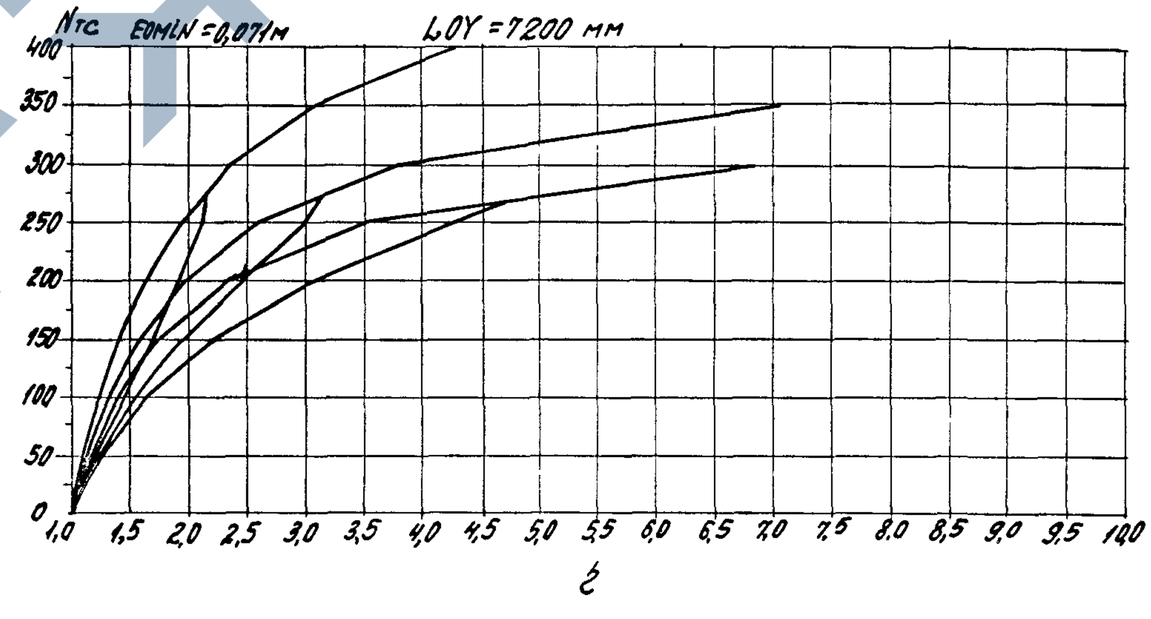

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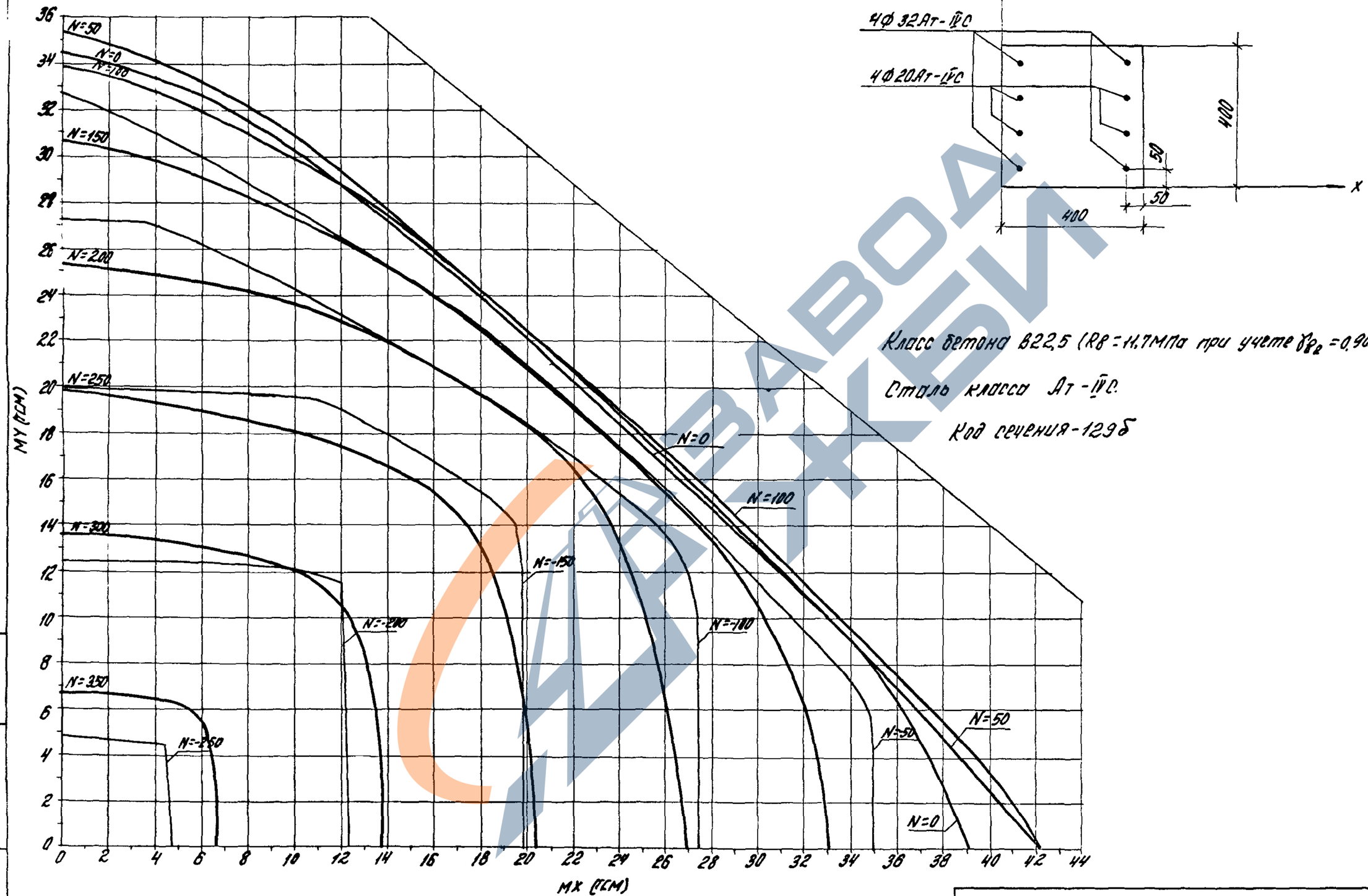

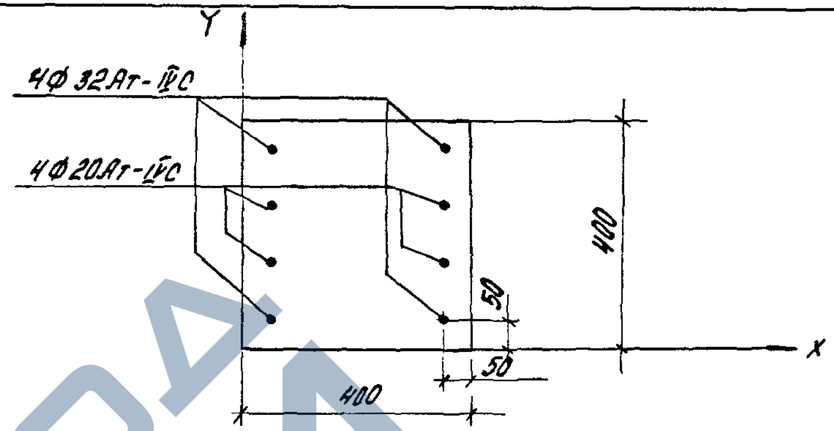

Класс бетона В22,5 (R_B = 11,7МПа при учете γ_{B2} = 0,90)

Сталь класса Ат-IVс.

Код сечения-1295

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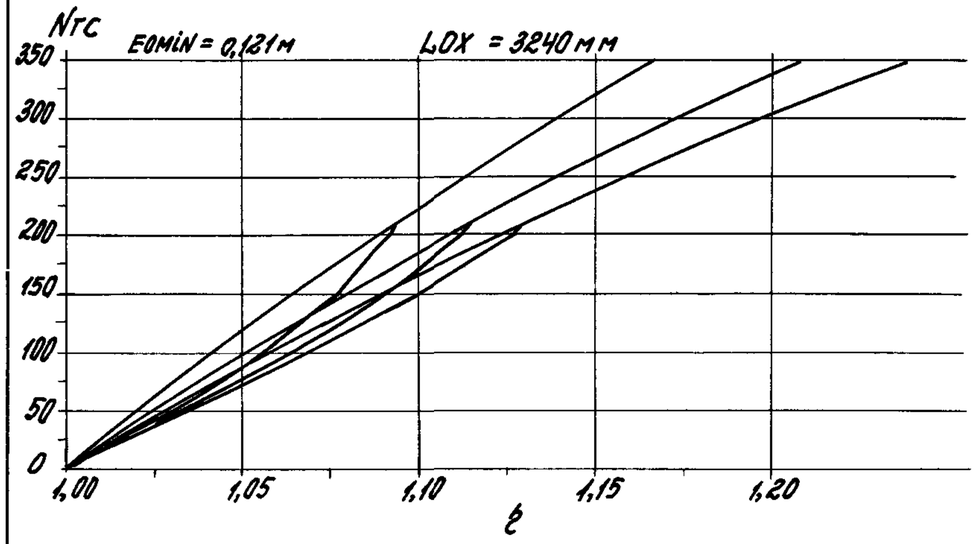

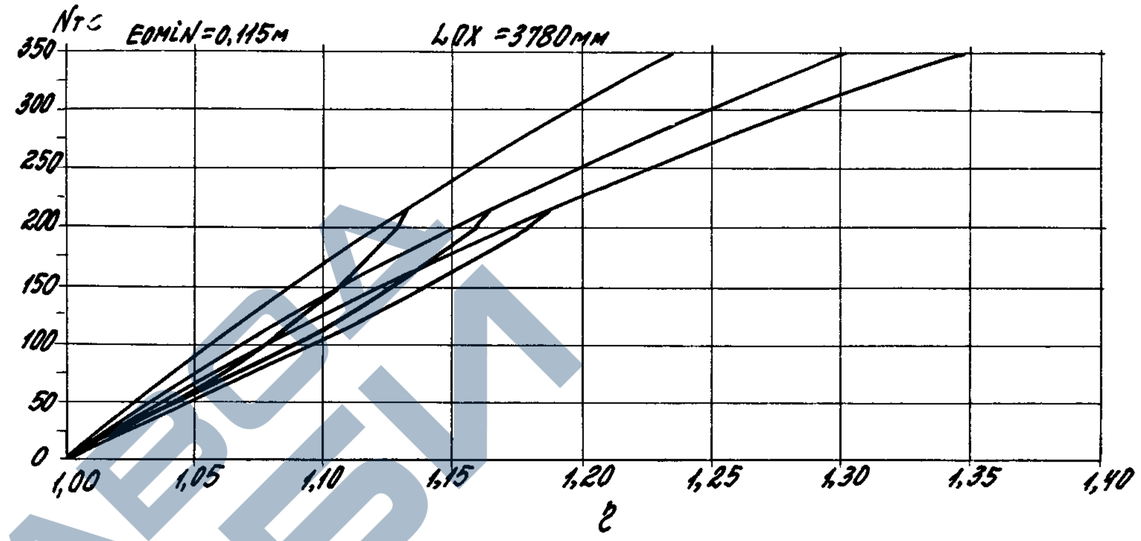

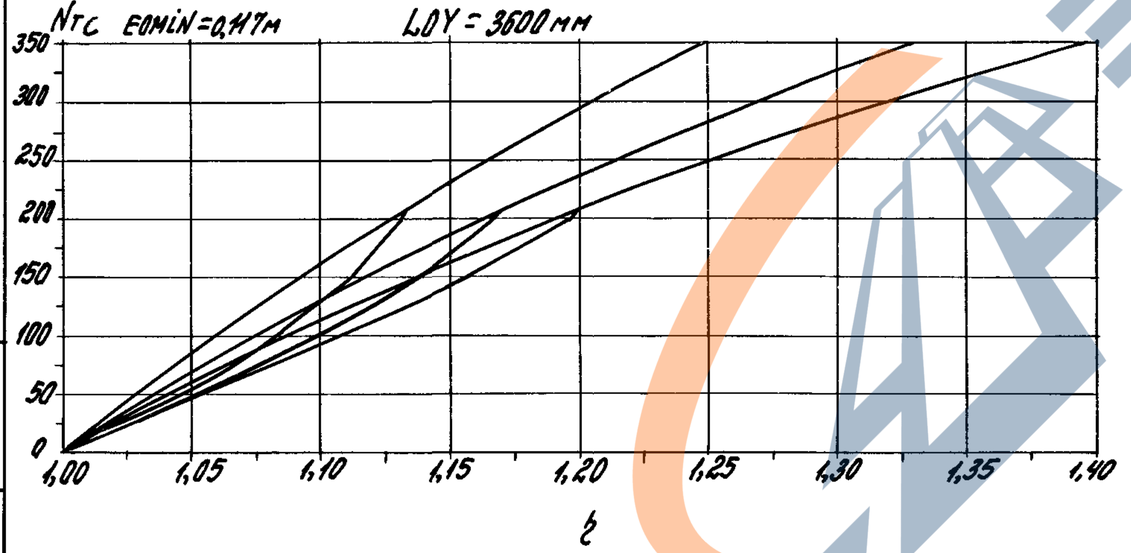

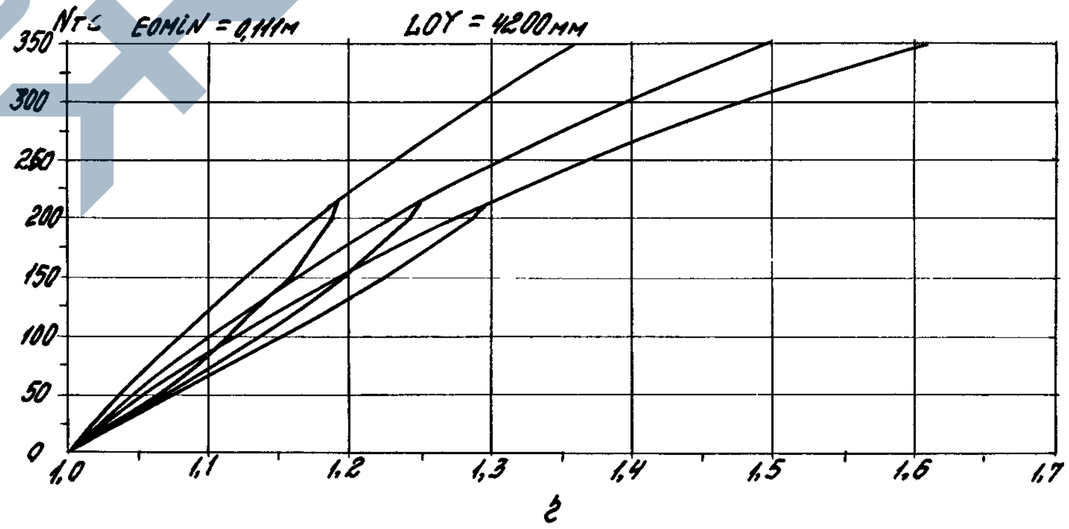

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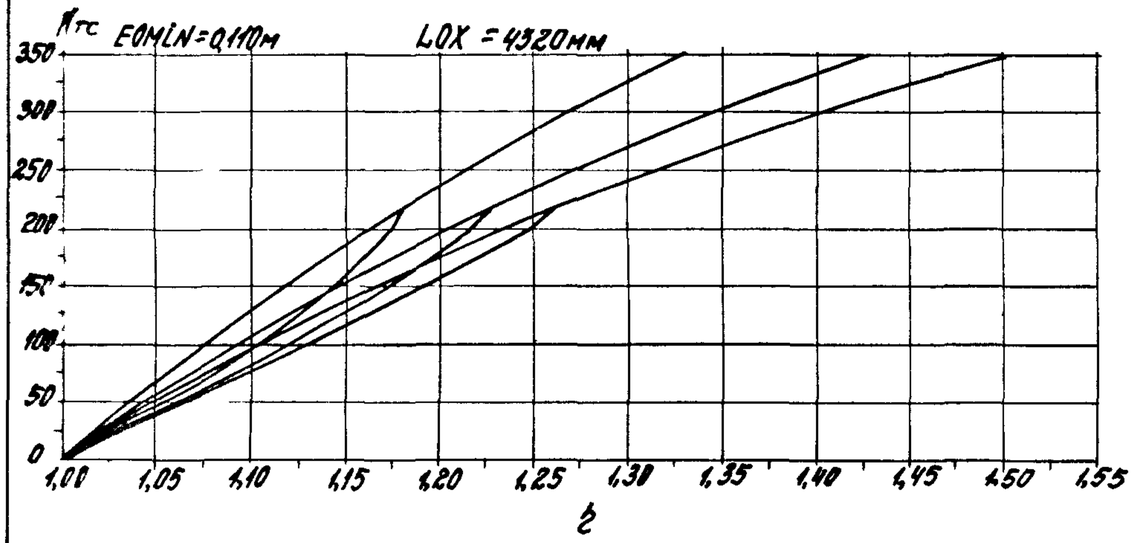

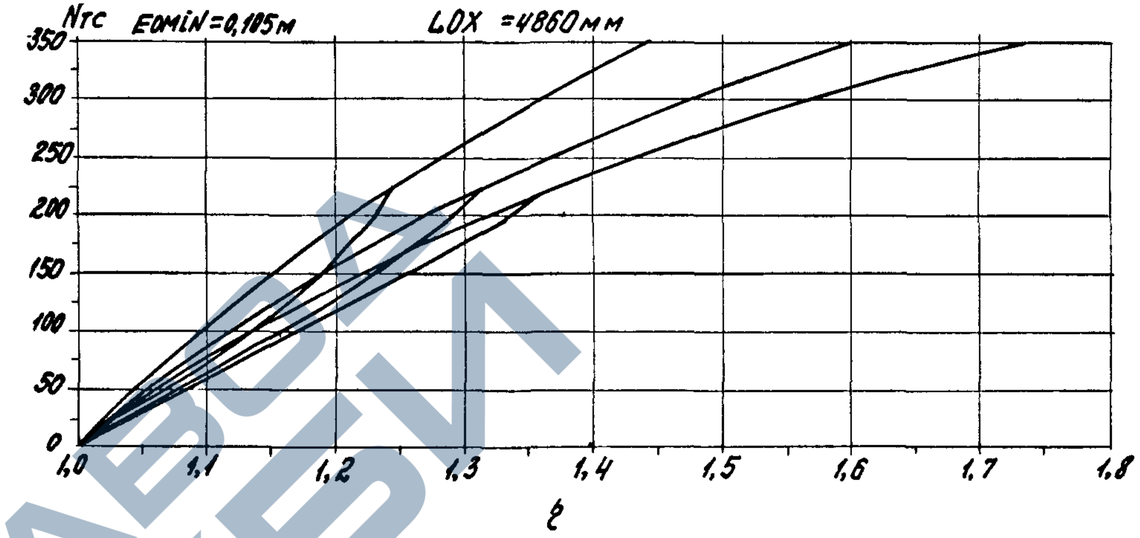

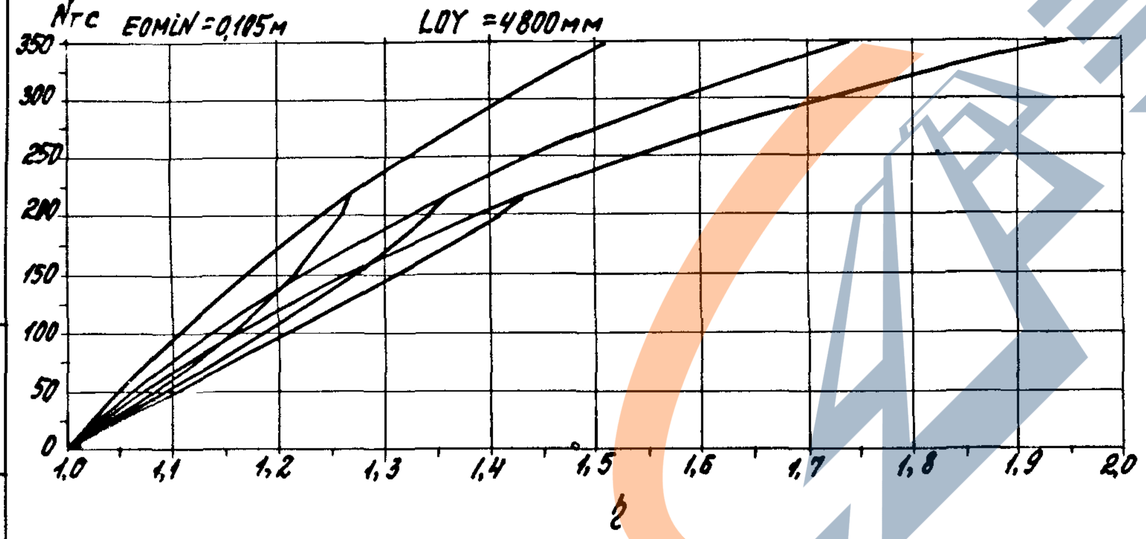

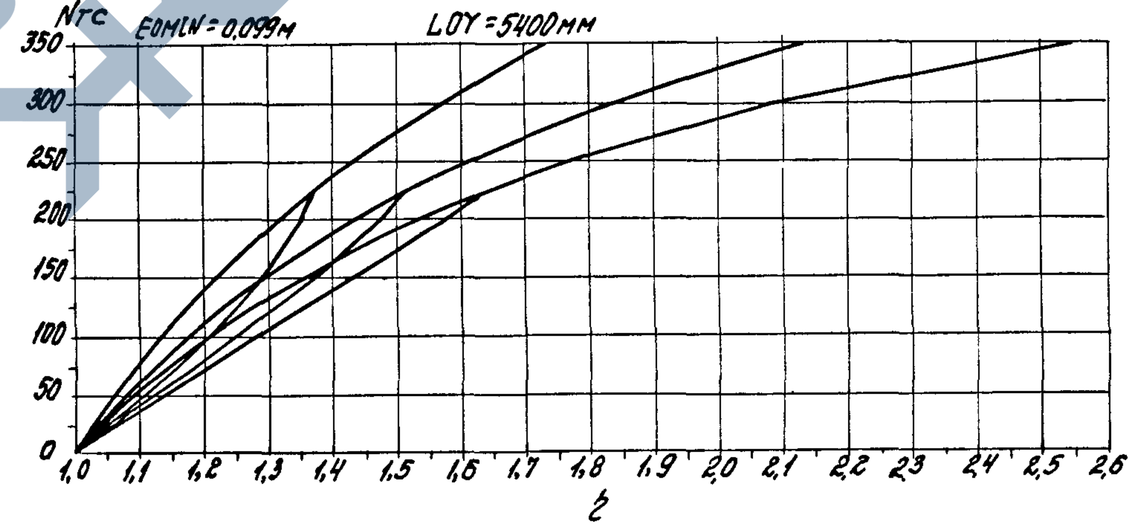

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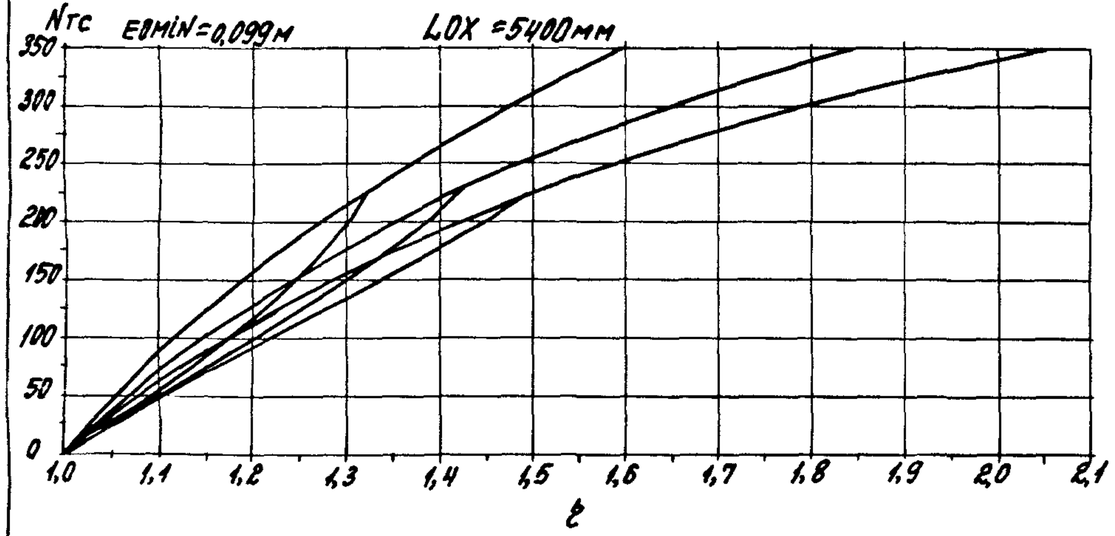

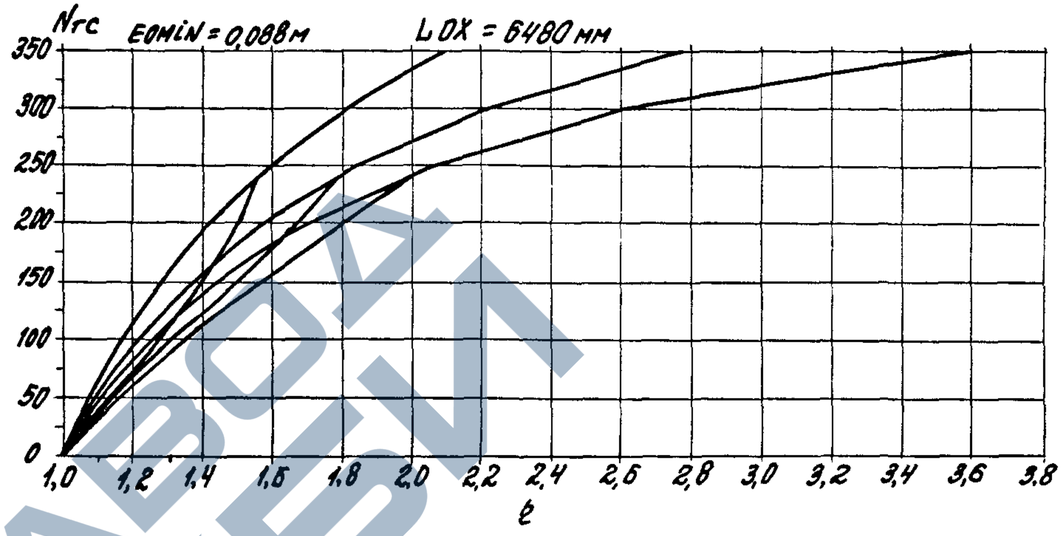

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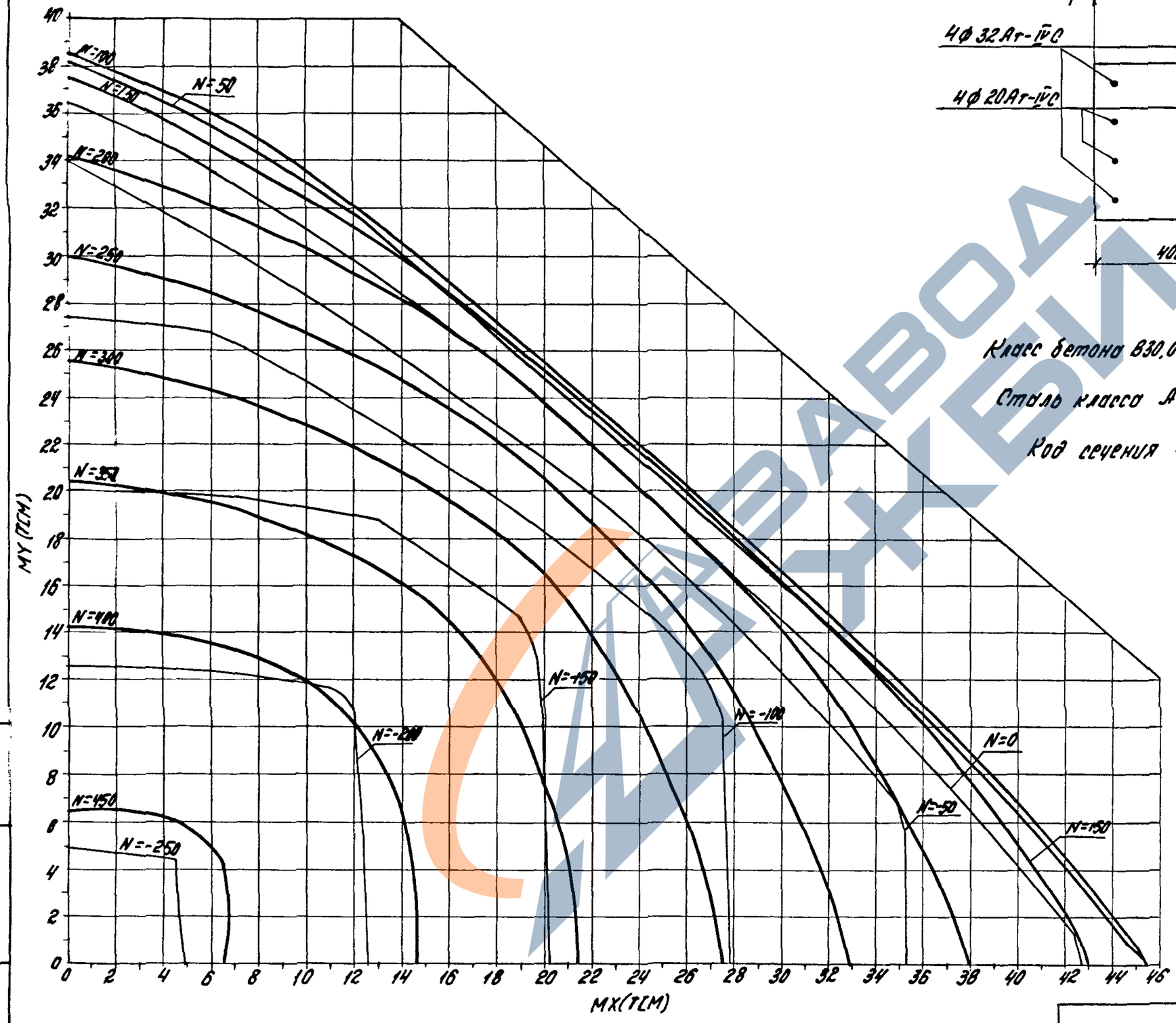

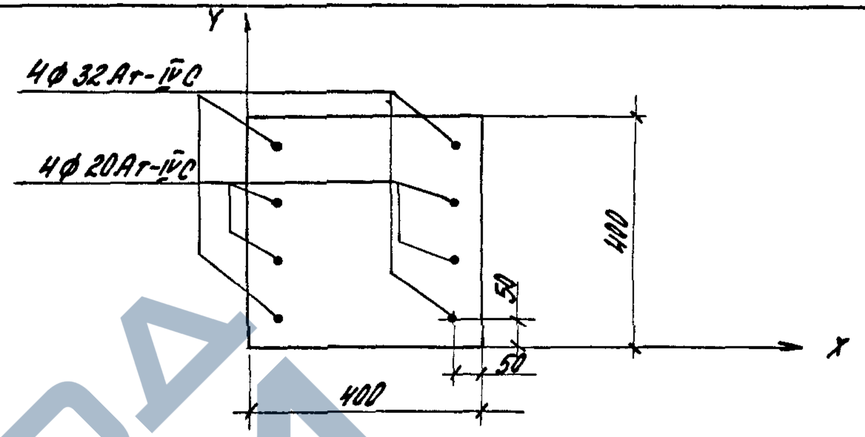

Класс бетона В30,0 (R_B =18,7МПа при учете γ_{B_2} = 1,10)

Сталь класса Ат-IVС.

Код сечения - 130а.

Инв.№подл.	Подпись и дата	Взам.инв.№	
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			ЛИСТ 238

24166-03 10

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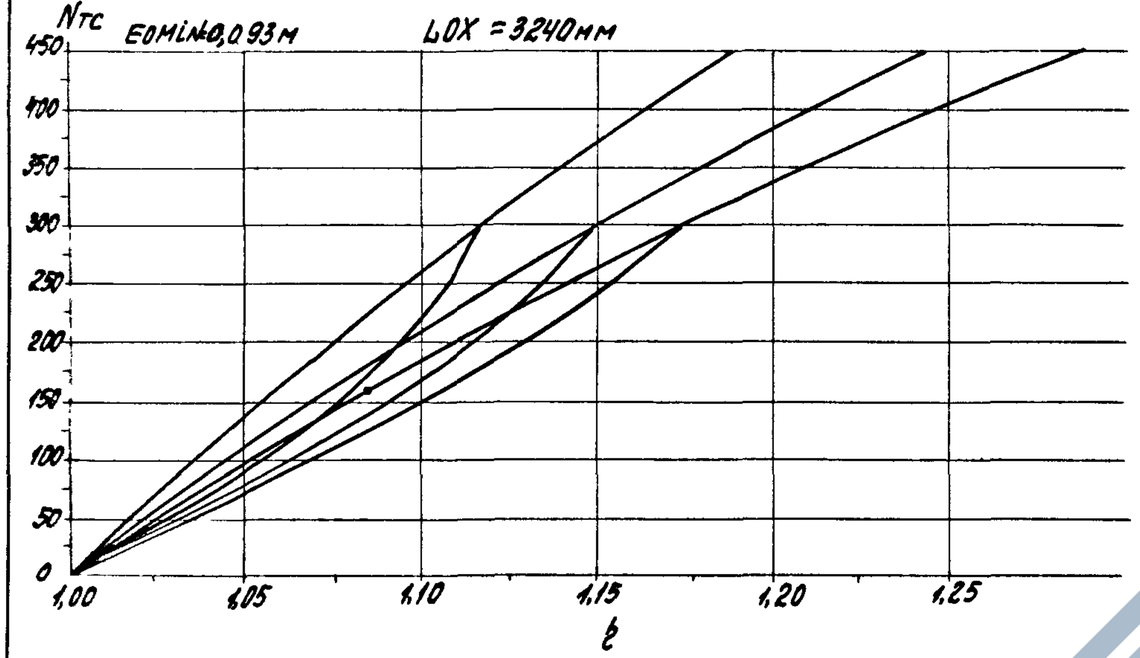

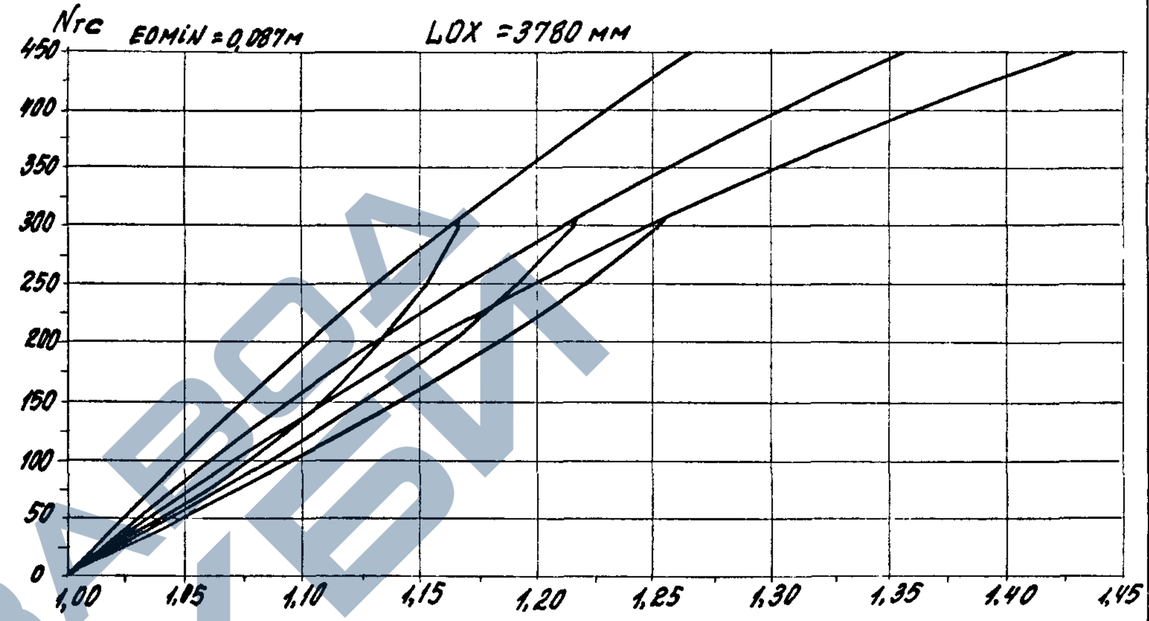

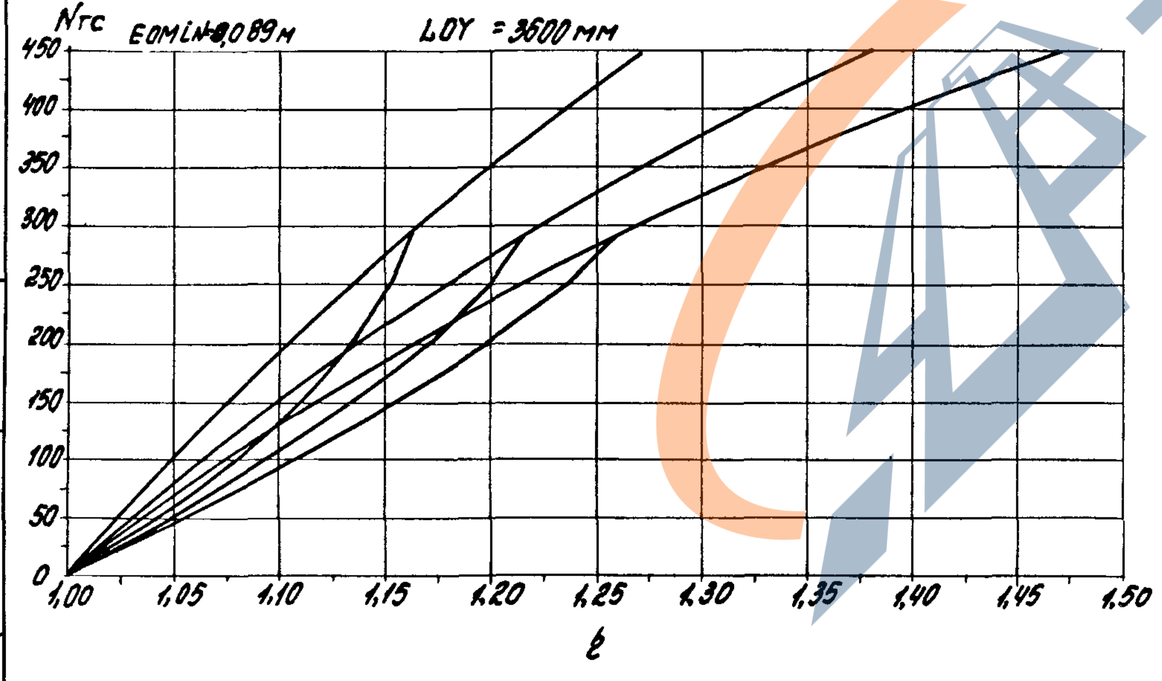

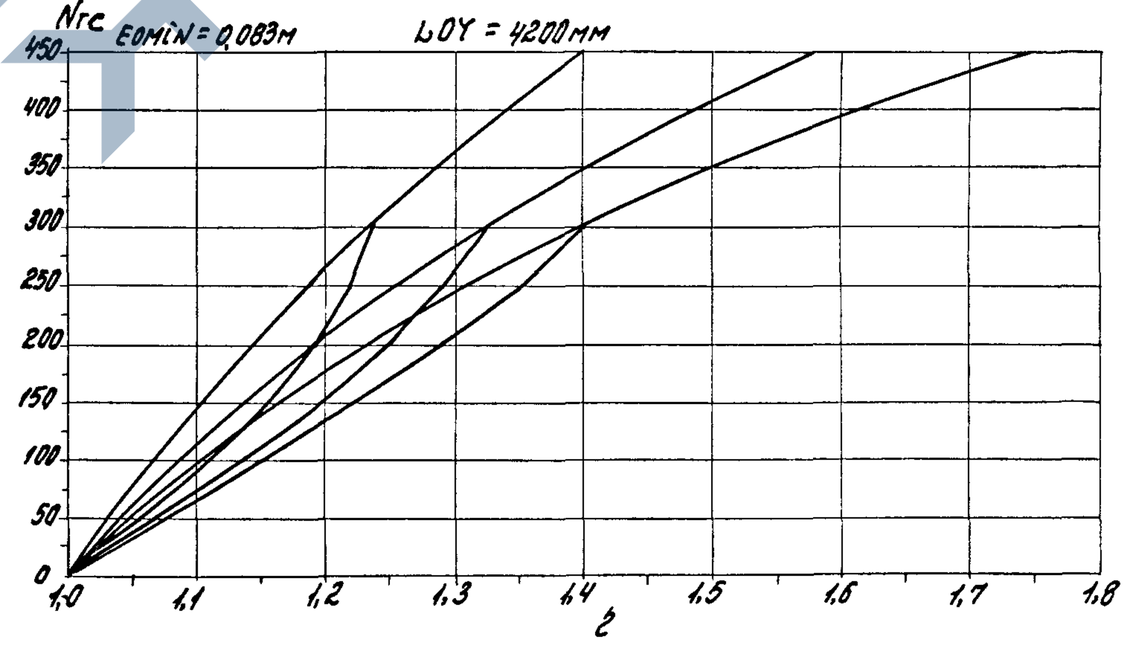

Инв.№подл. | Подп. и дата | Взам.инв.№

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Лист 234

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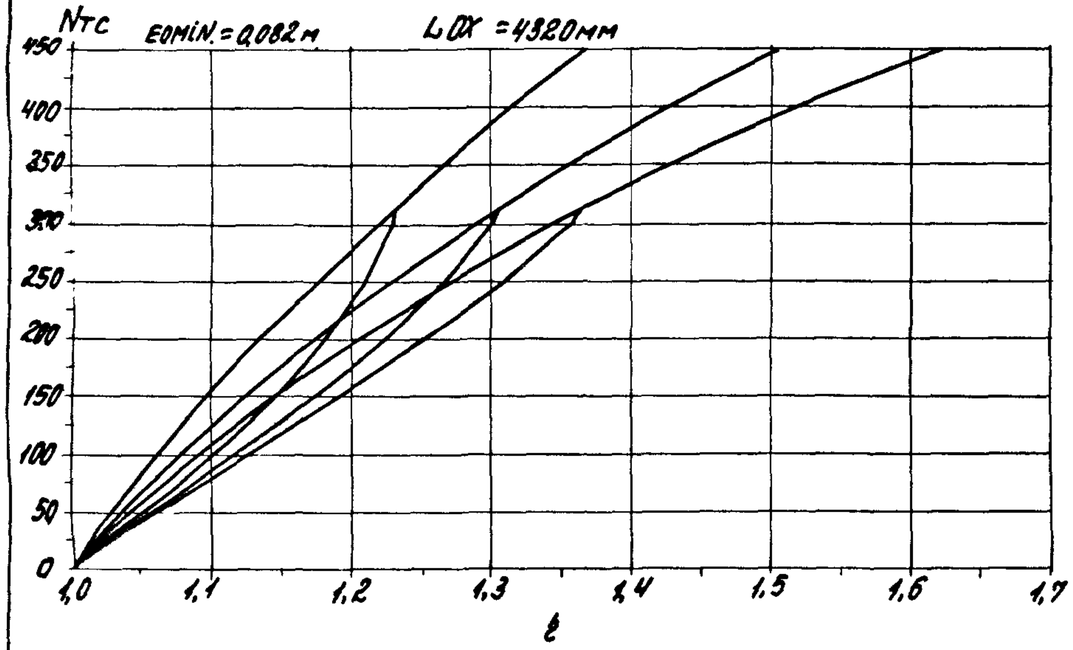

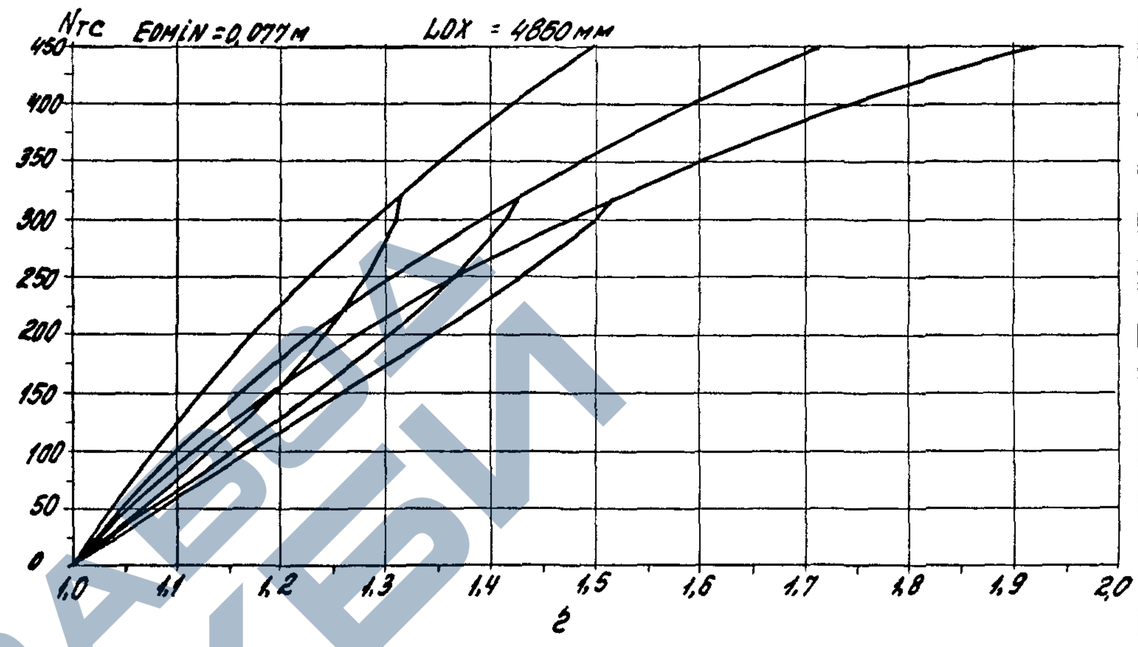

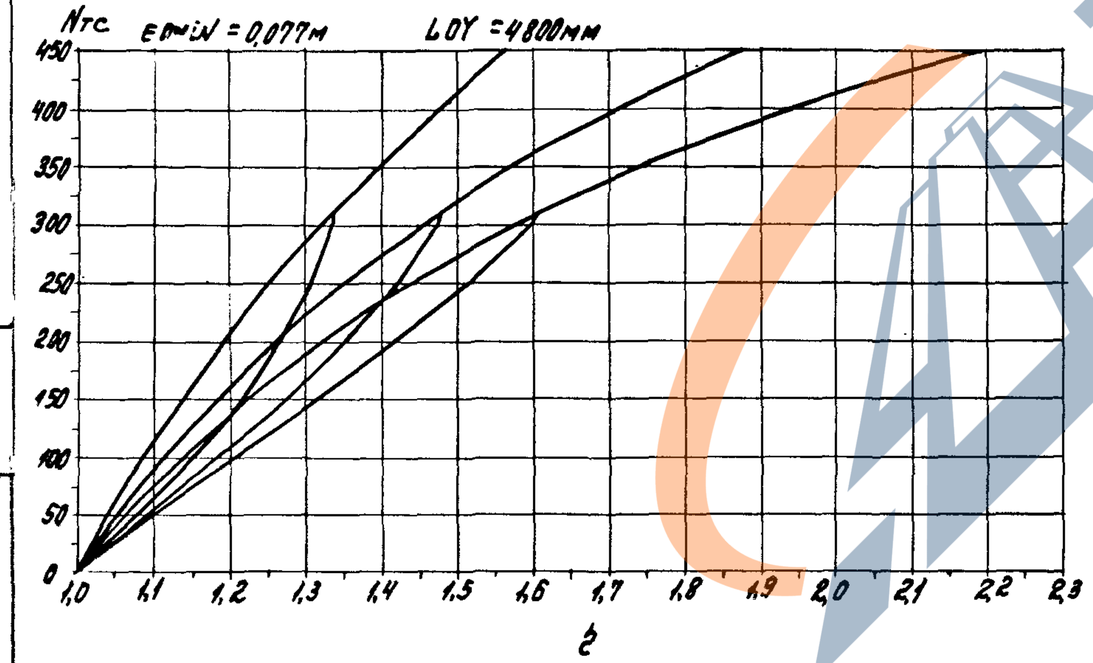

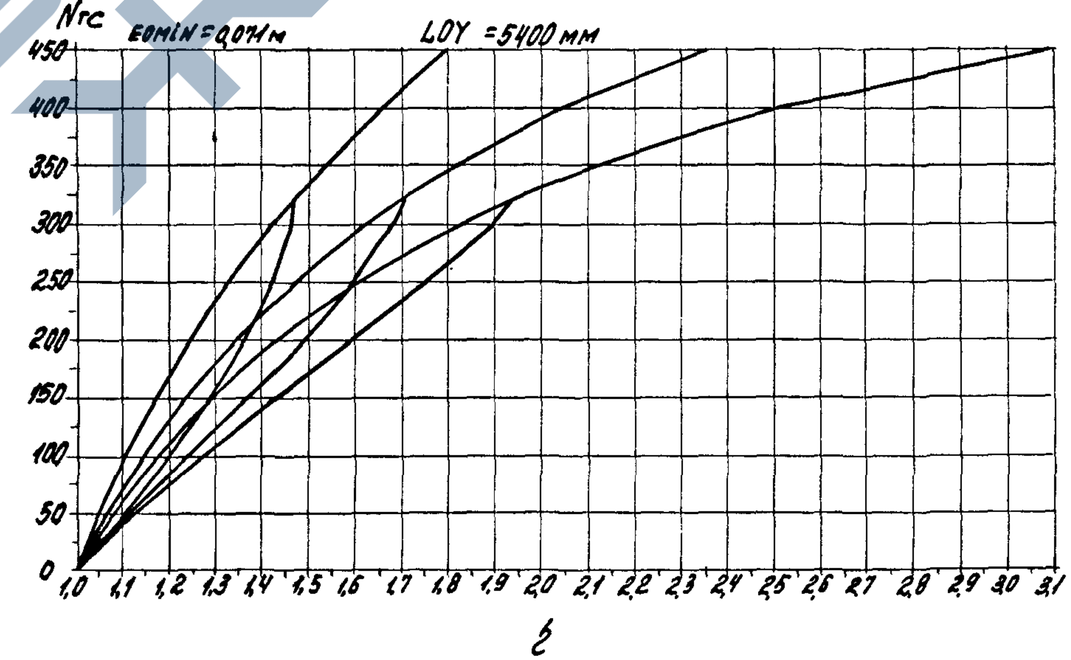

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Лист 235

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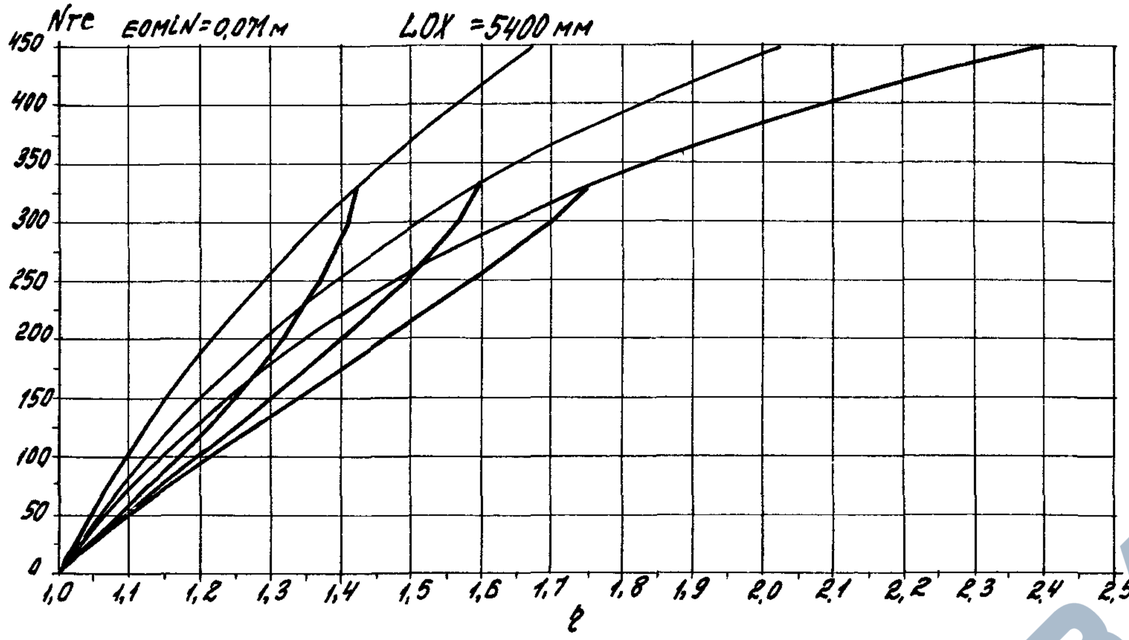

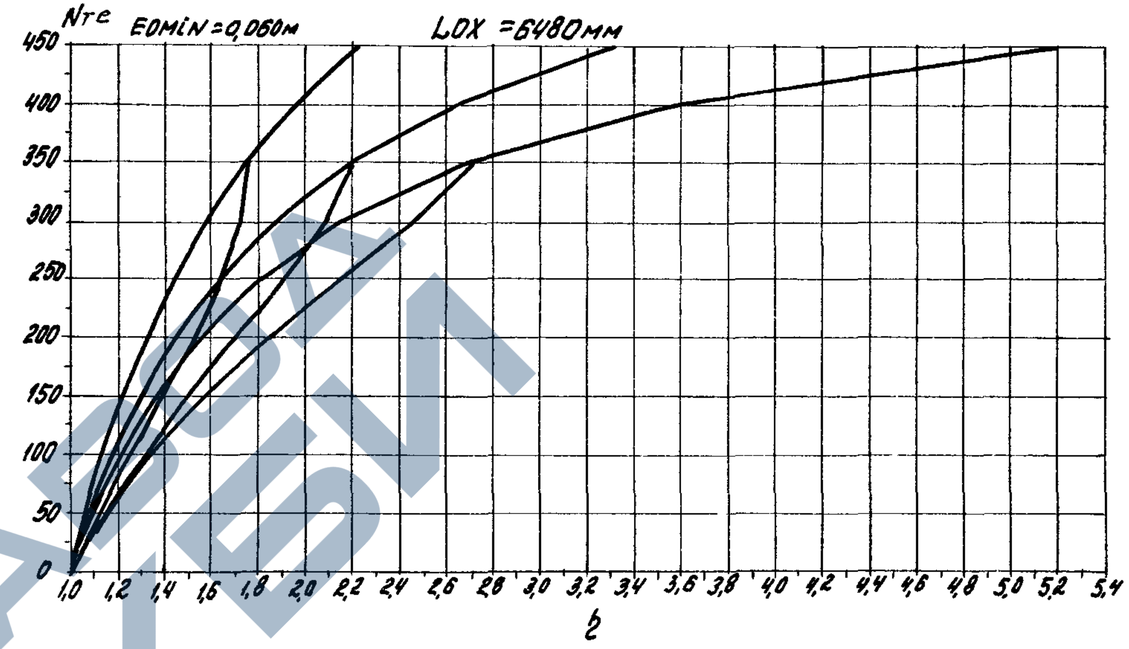

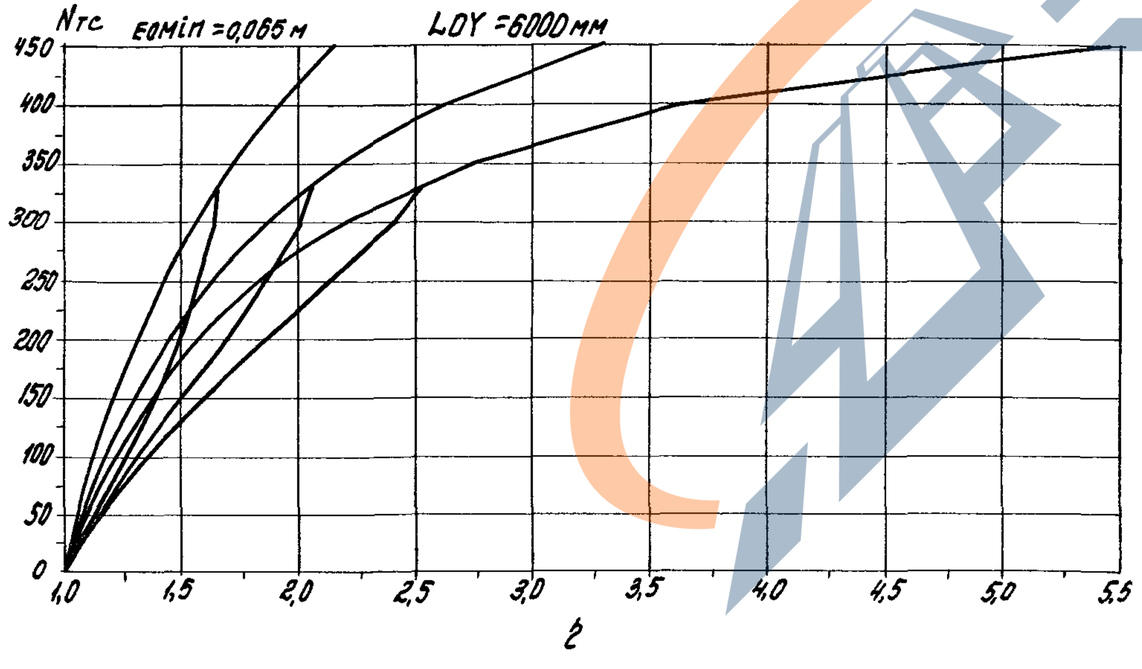

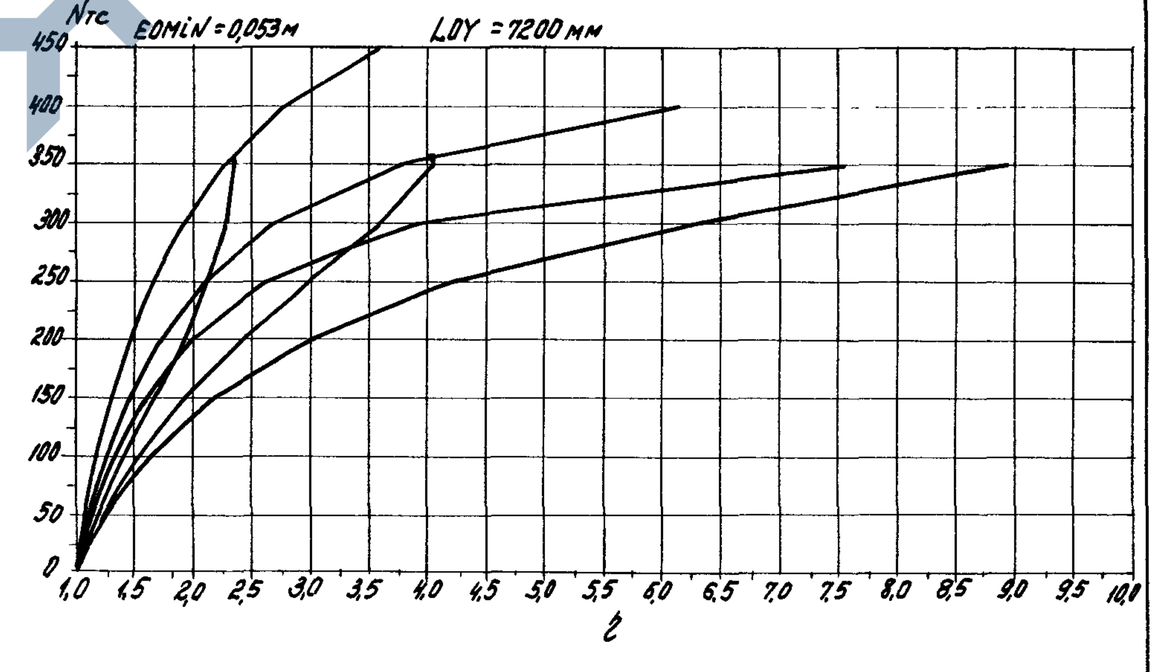

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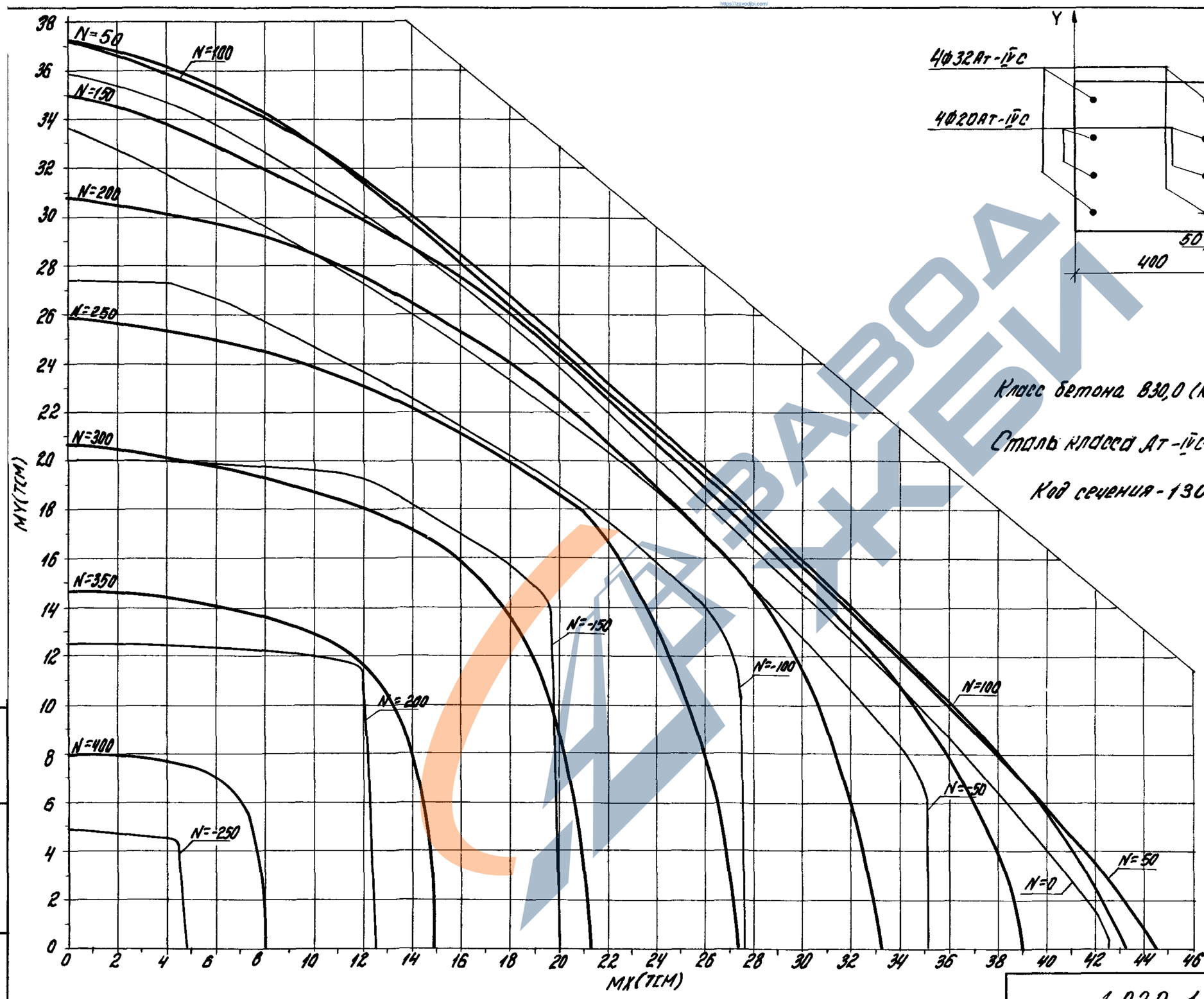

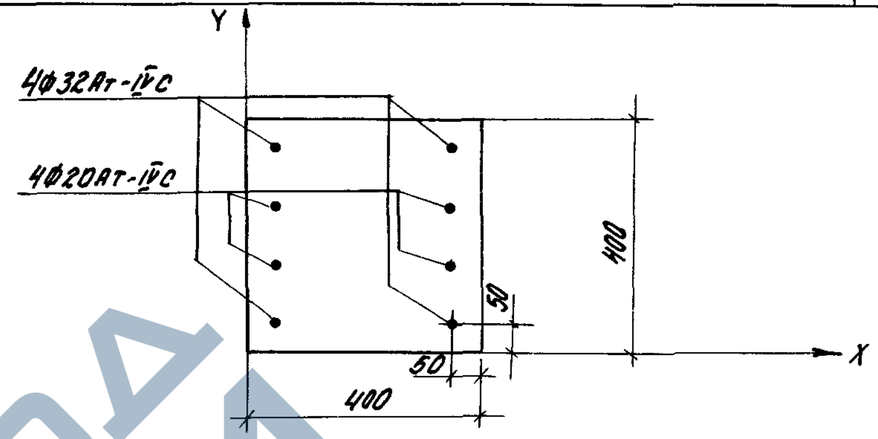

Класс бетона В30,0 (R_B = 15,3МПа при учете γ_{B_2} = 0,90)

Сталь класса Ат-IVС

Код сечения - 1306

Инв.№подл.	Подпись и дата	Взам.инв.№

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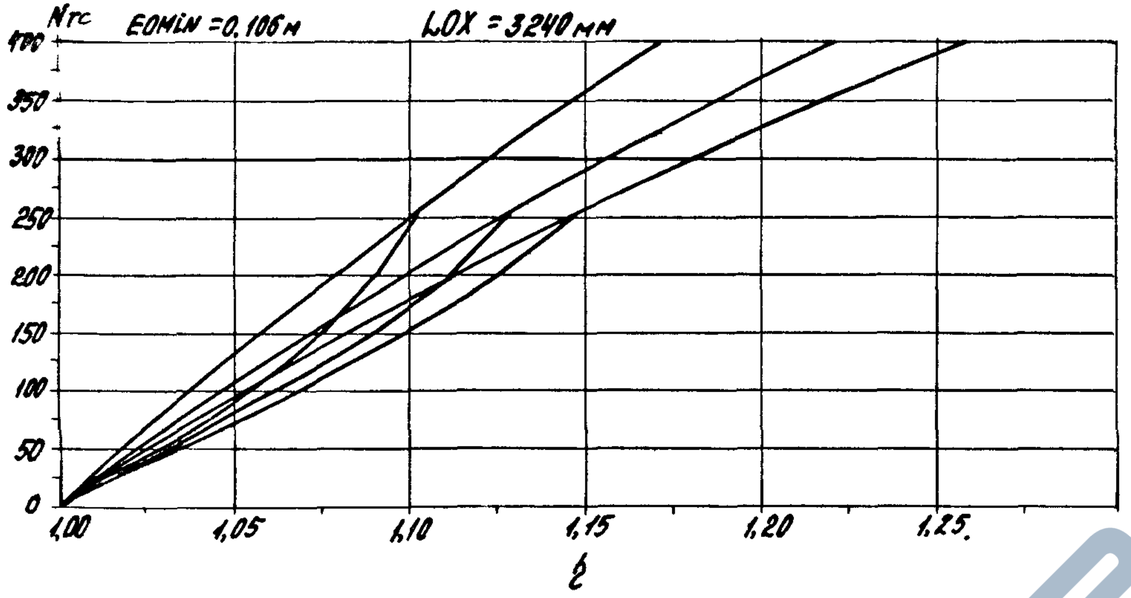

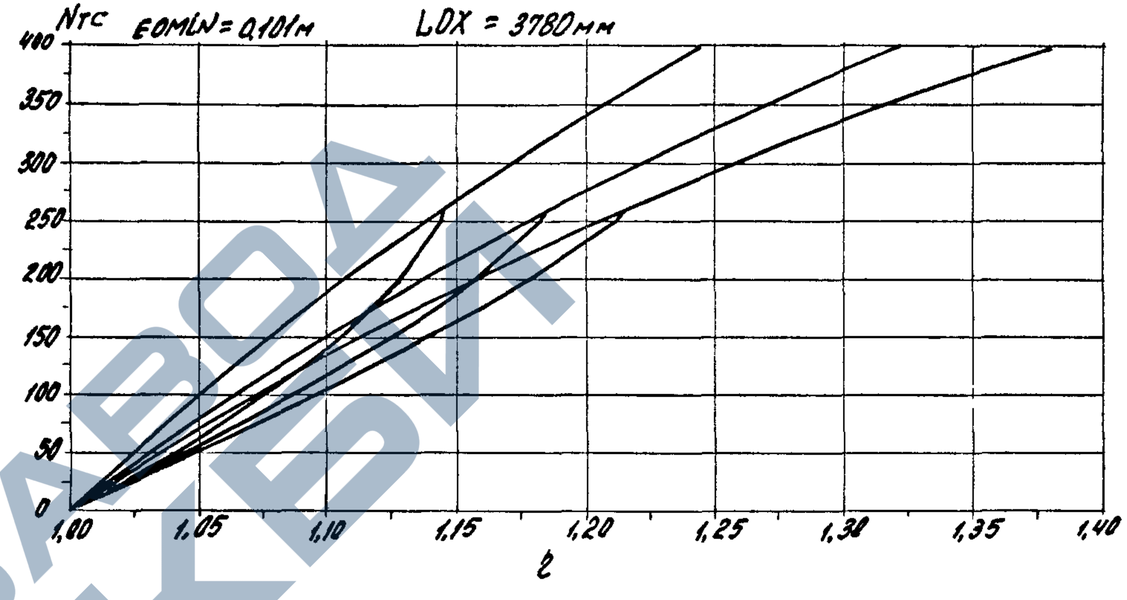

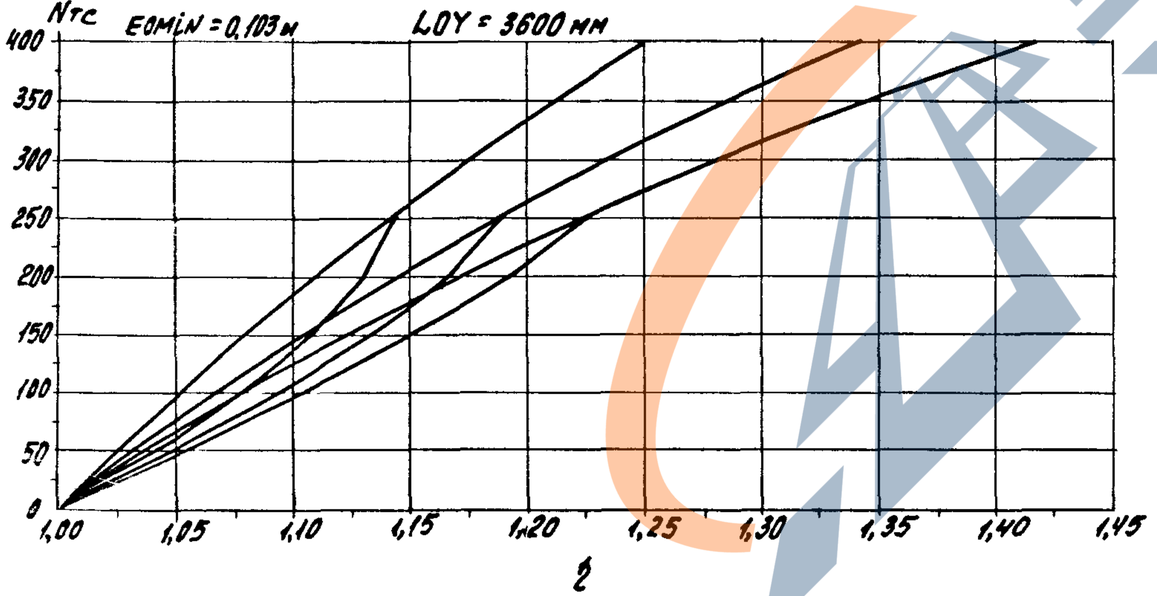

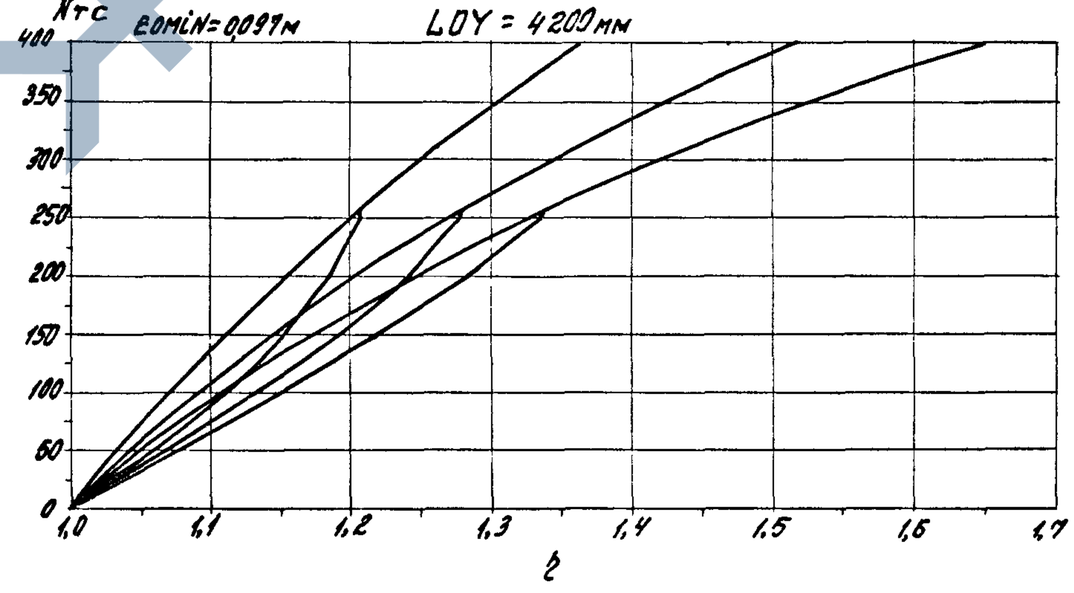

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Лист 238

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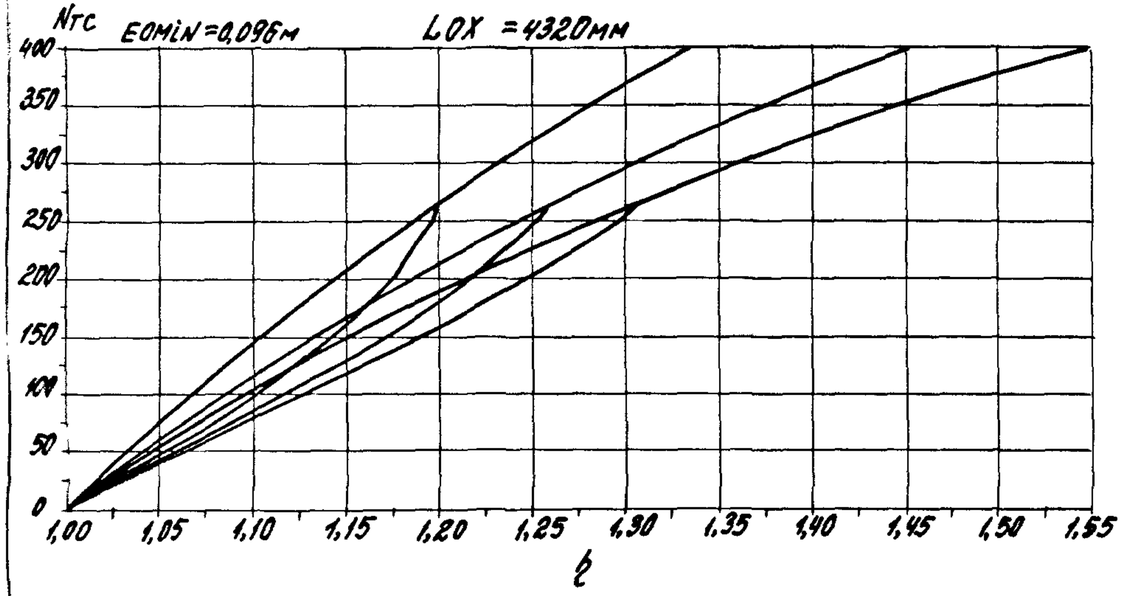
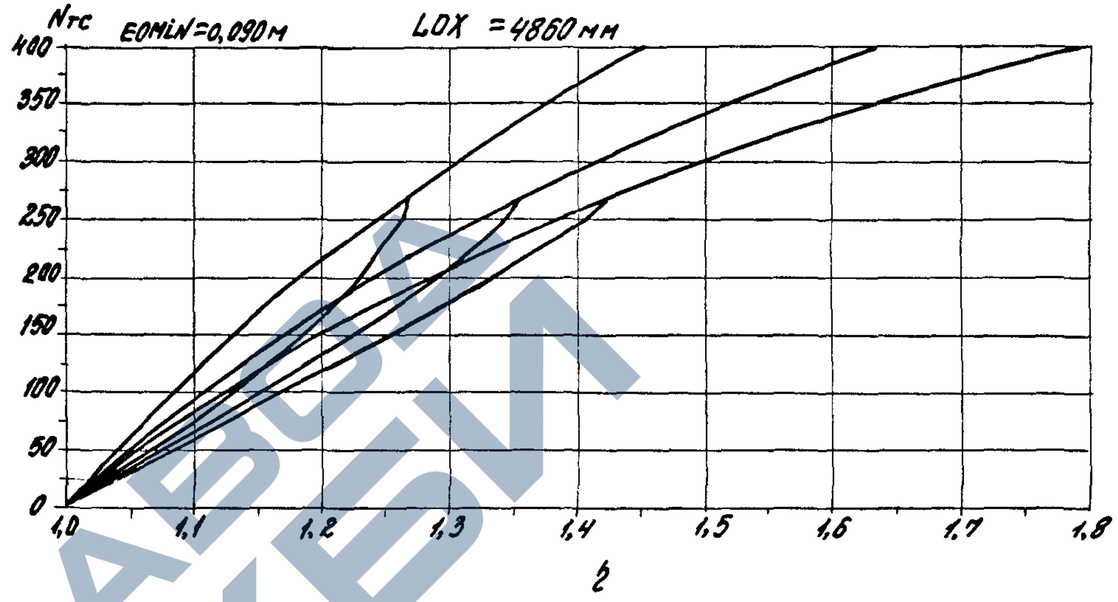




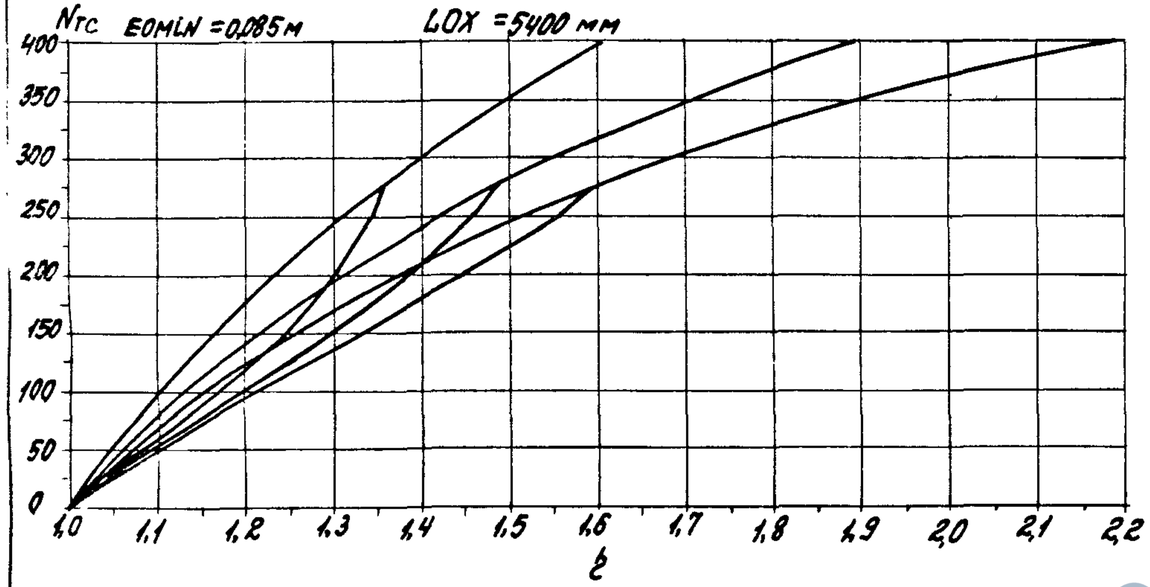
Инв.№ подл. | Подпись и дата | Взам.инв.№

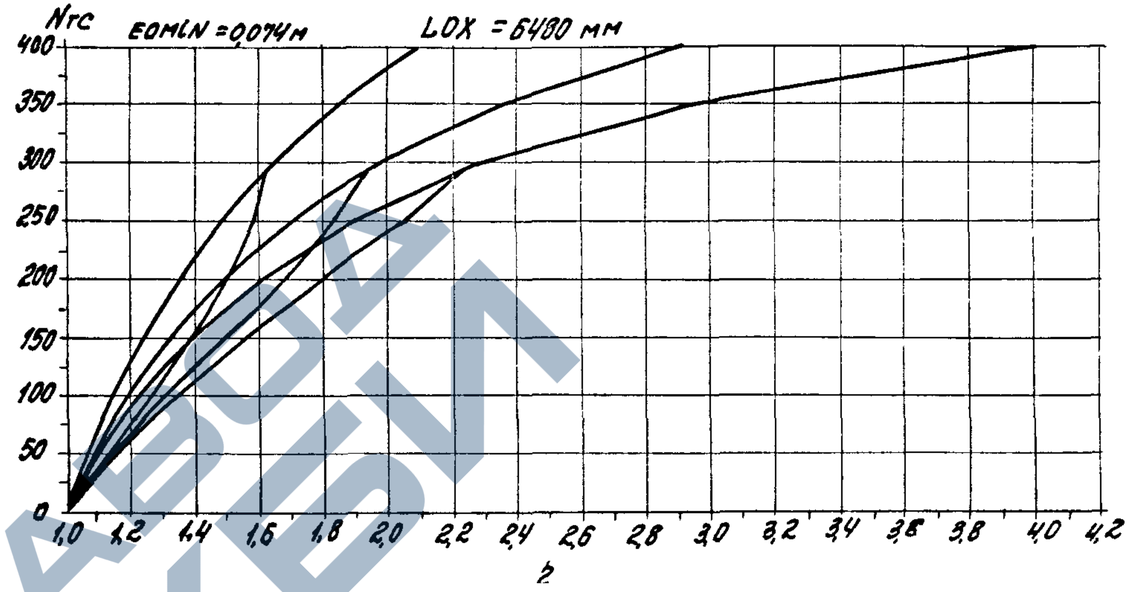
1.020.1-4. 0-9 - 002

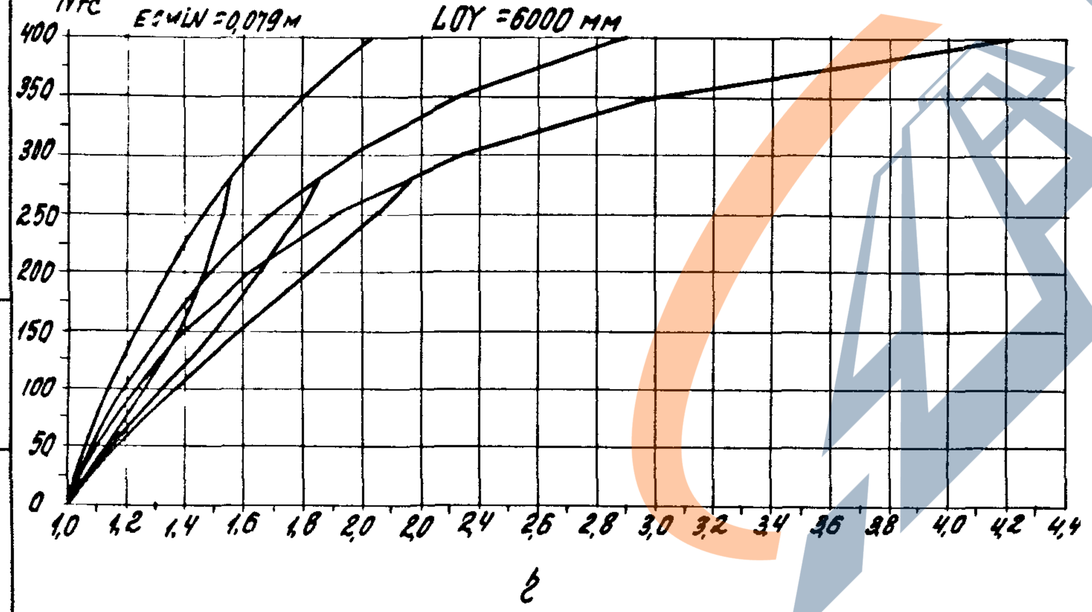
Лист 239

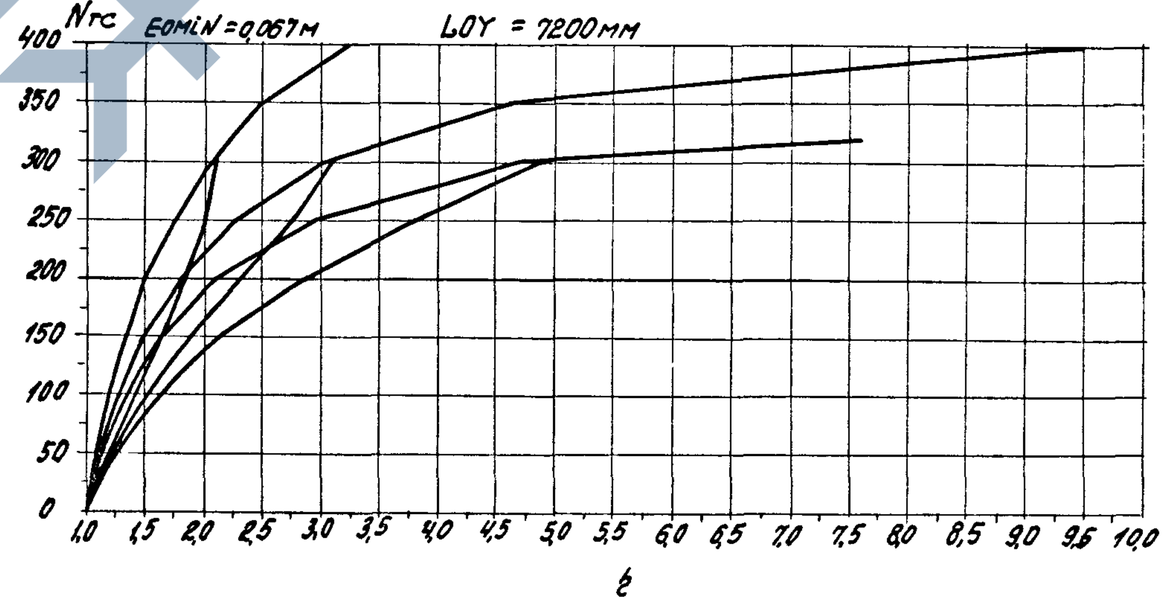
24166-03 16

https://zavodjbi.com/









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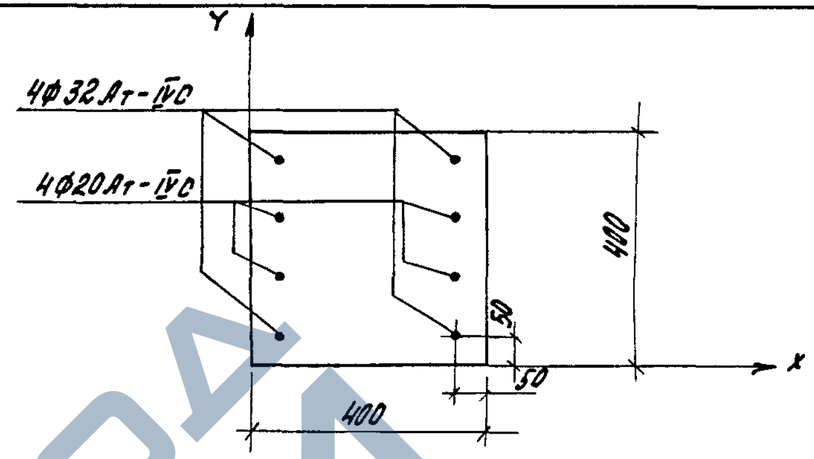
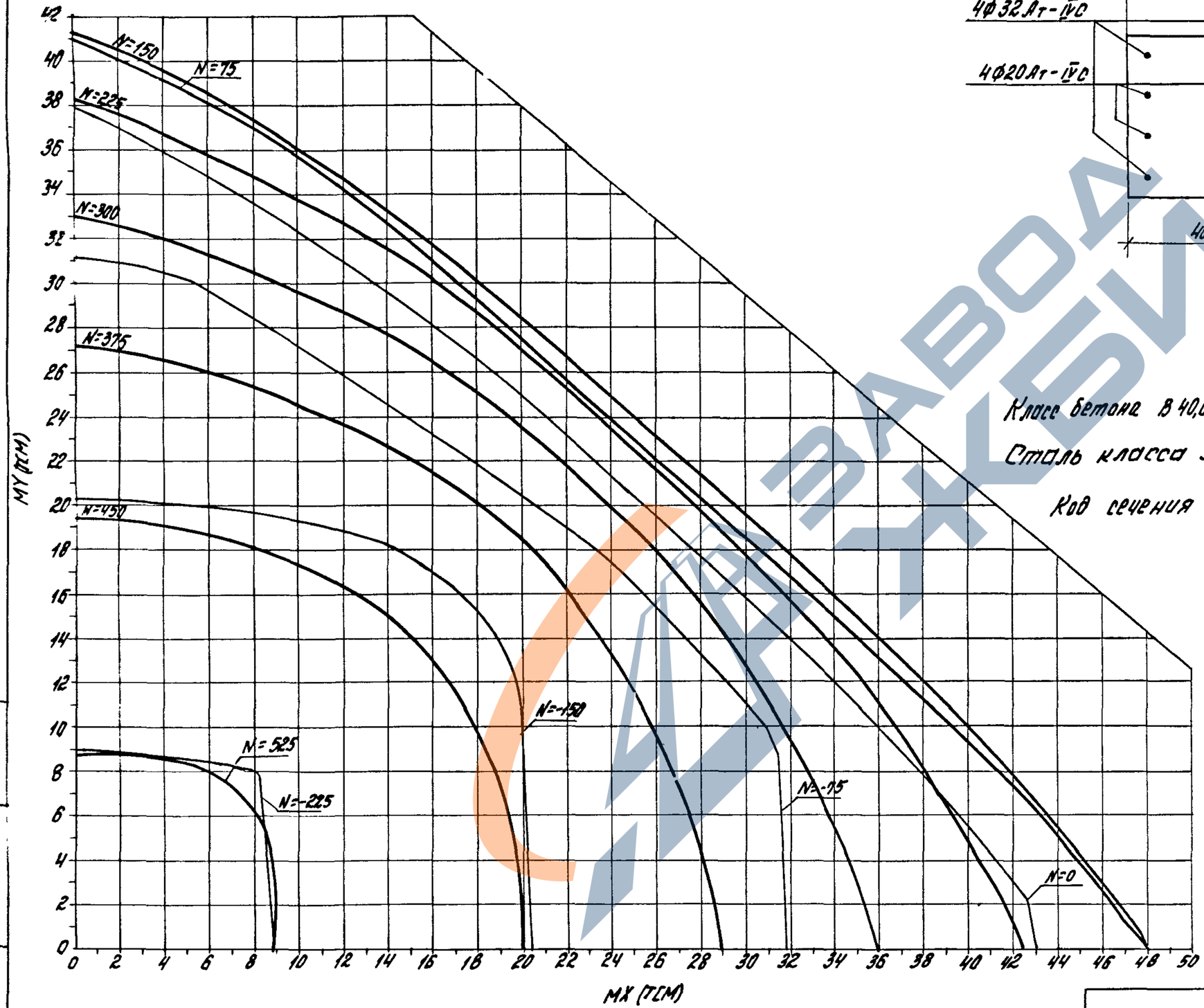




Класс бетона В 40,0 (R_B = 24,2МПа при учете γ_{B_2} = 1,10)

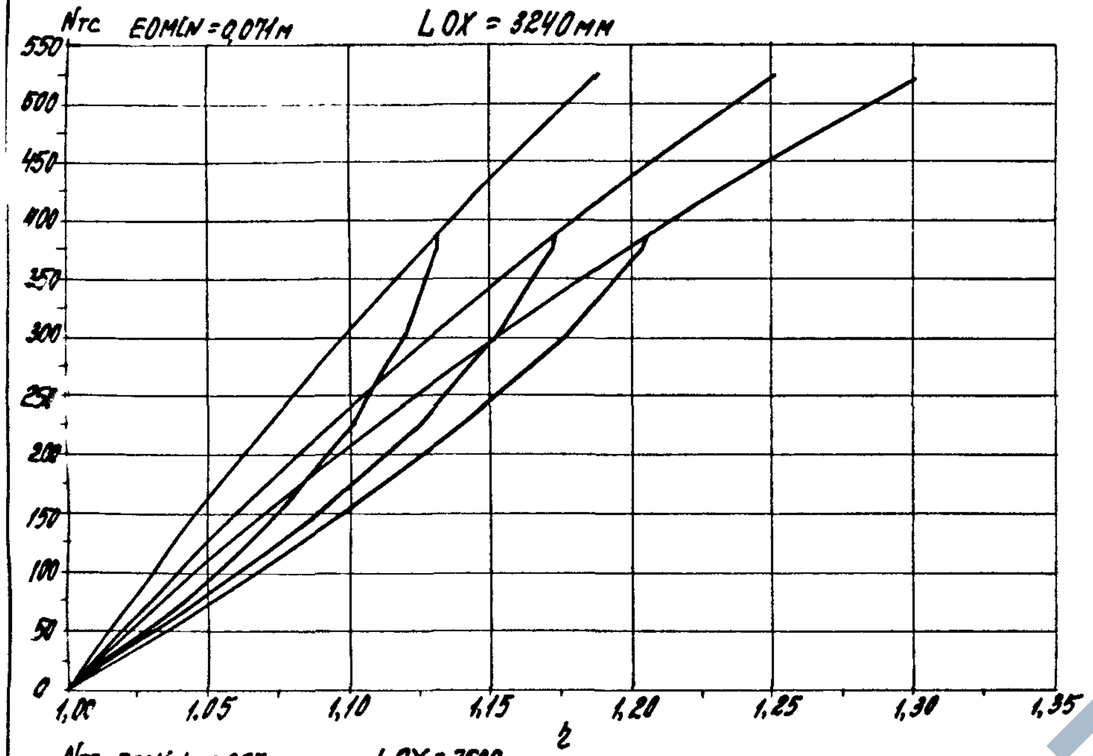
Сталь класса Ат-IVС.

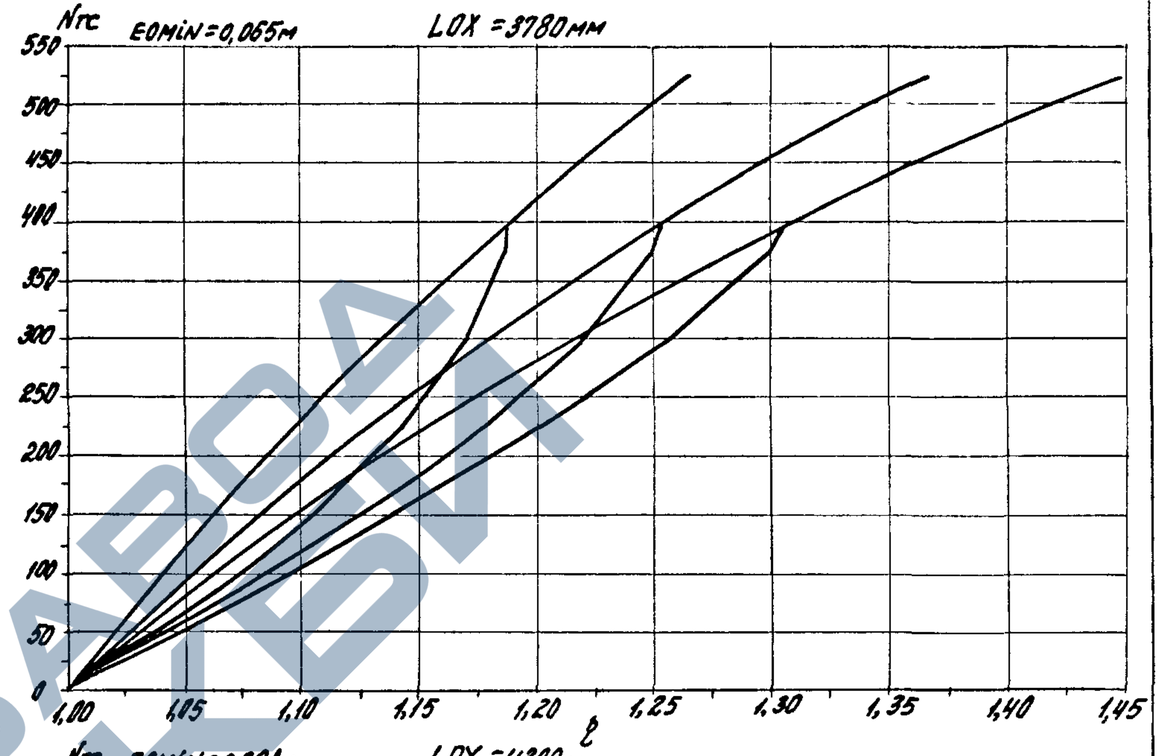
Ков сечения - 131а

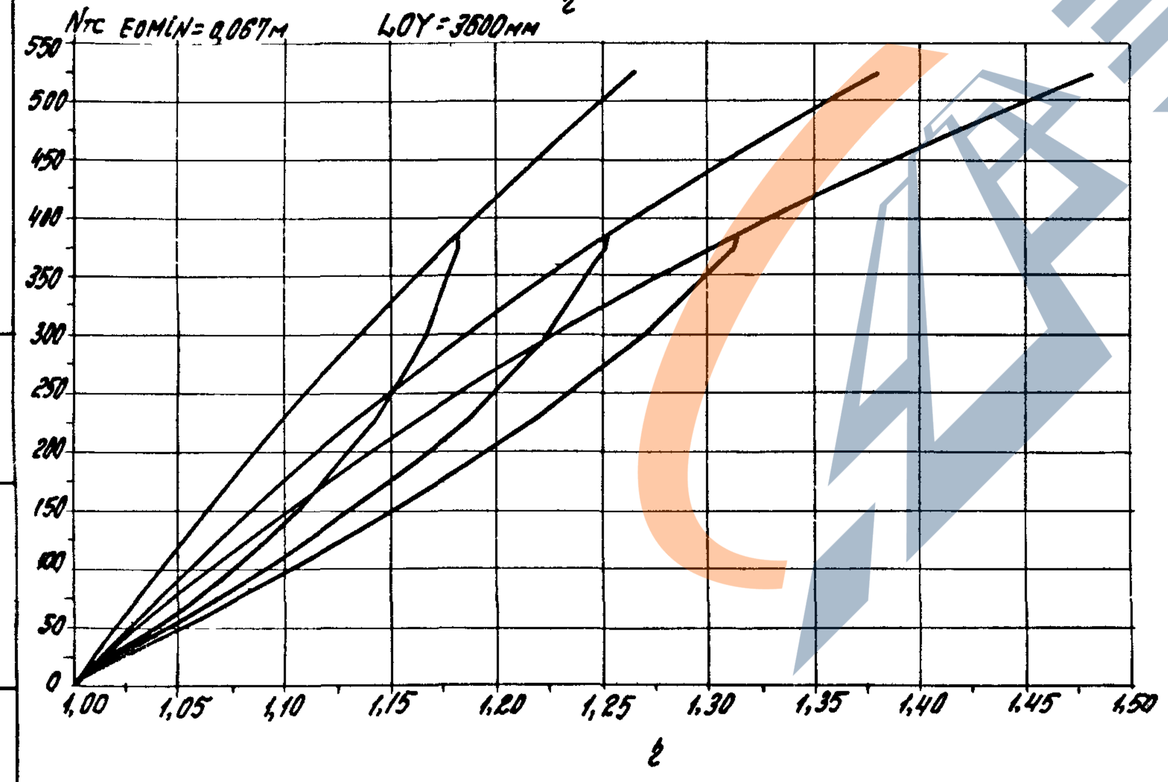
Инв.№подл. | Подпись и дата | Взам.инв.№

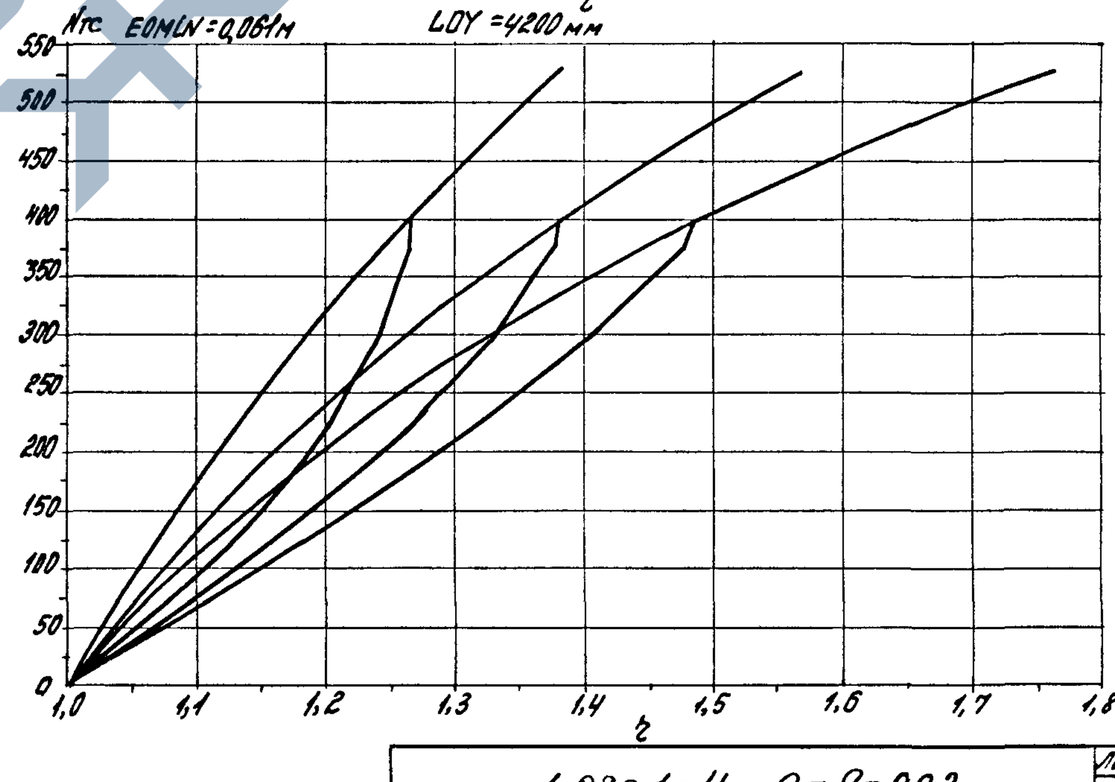
https://zavodjbi.com/

https://zavodjbi.com/









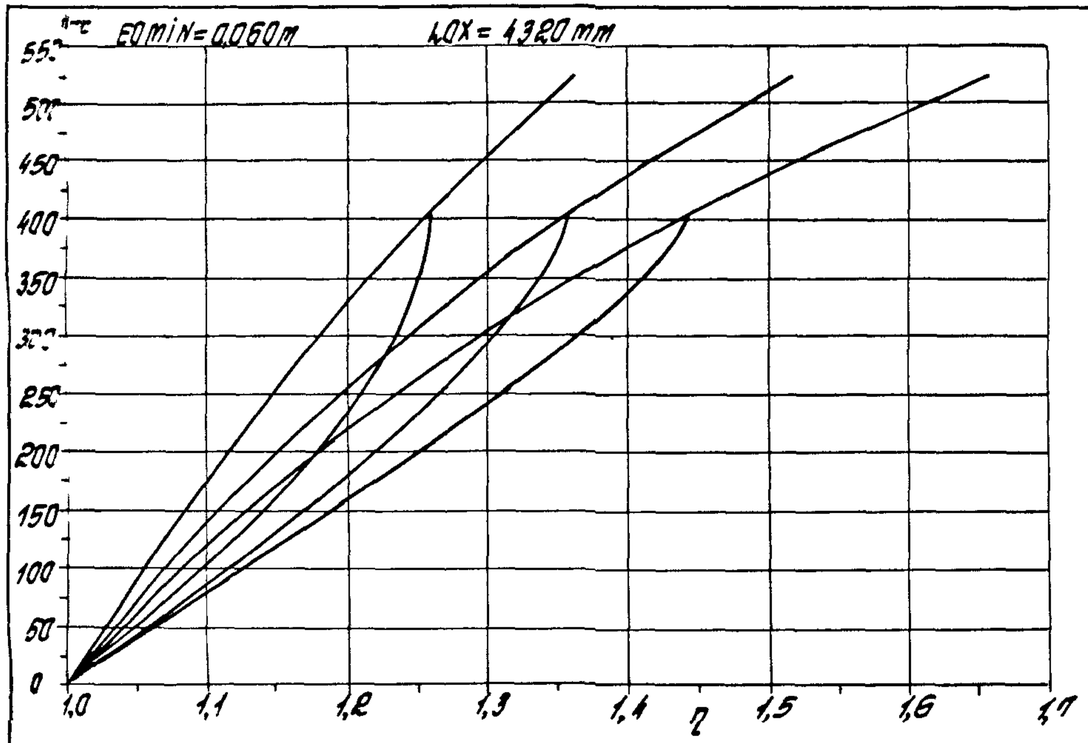
Инв.№подл. | Подпись и дата | Взам.инв.№

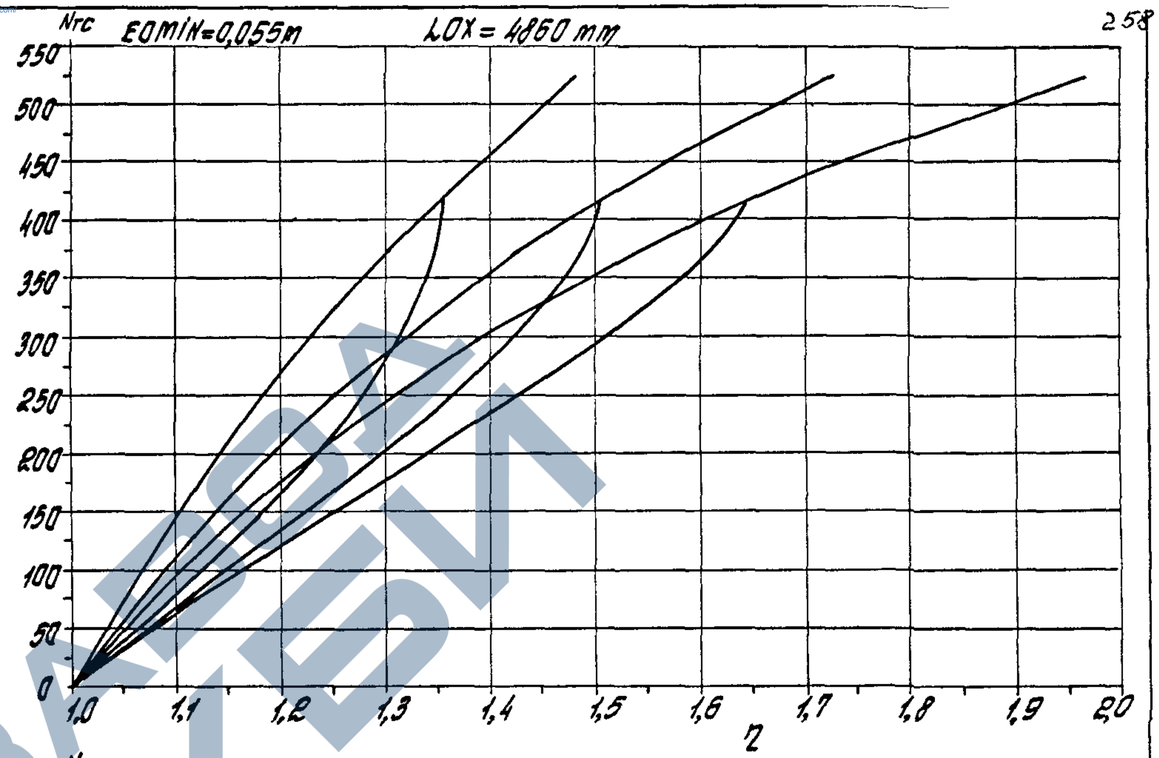
1.020.1-4. 0-9-002

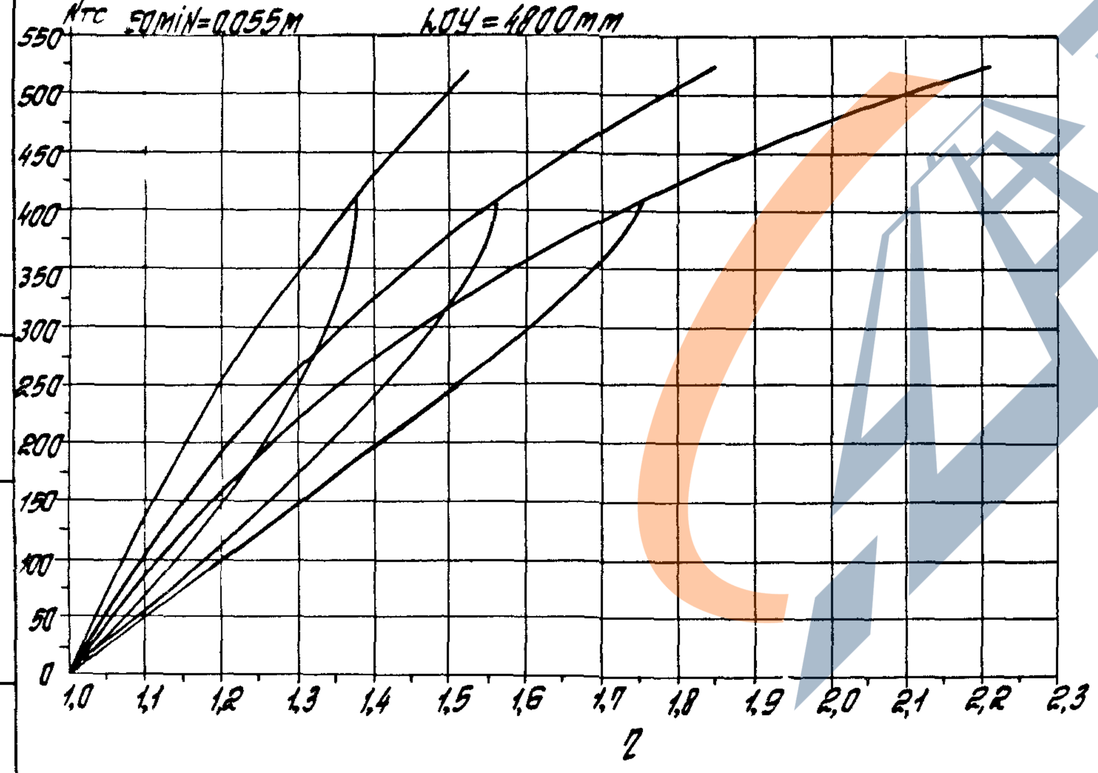
Лист 242

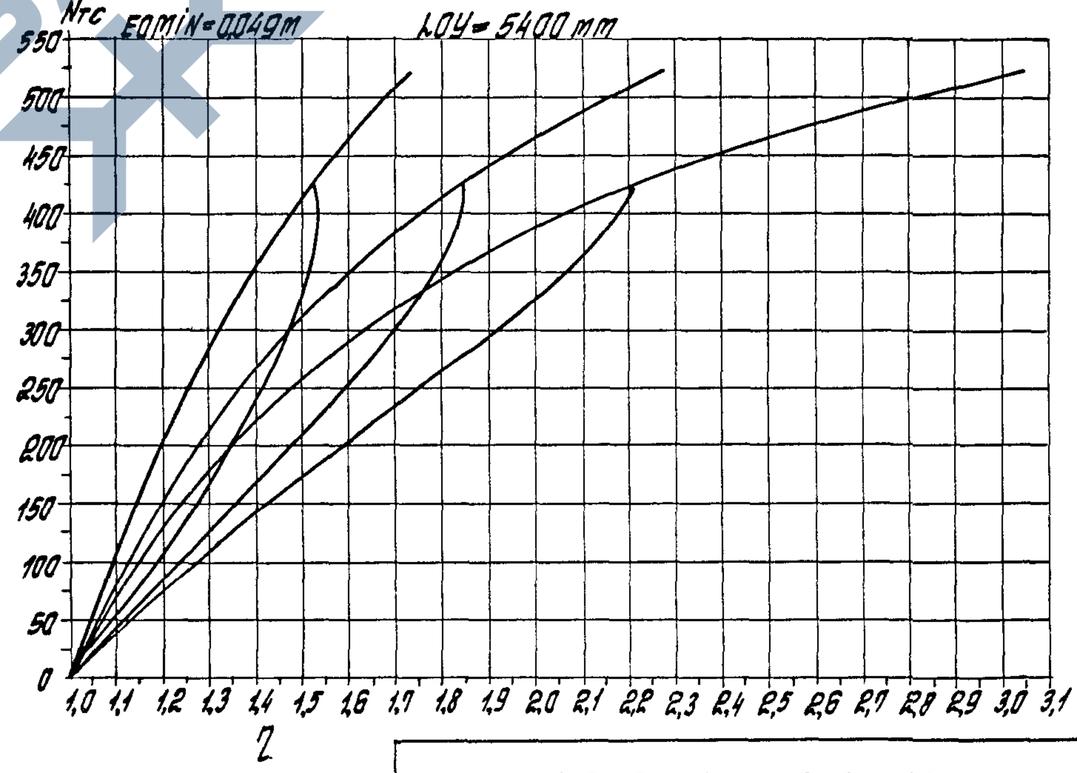
24166-03 19

https://zavodjbi.com/









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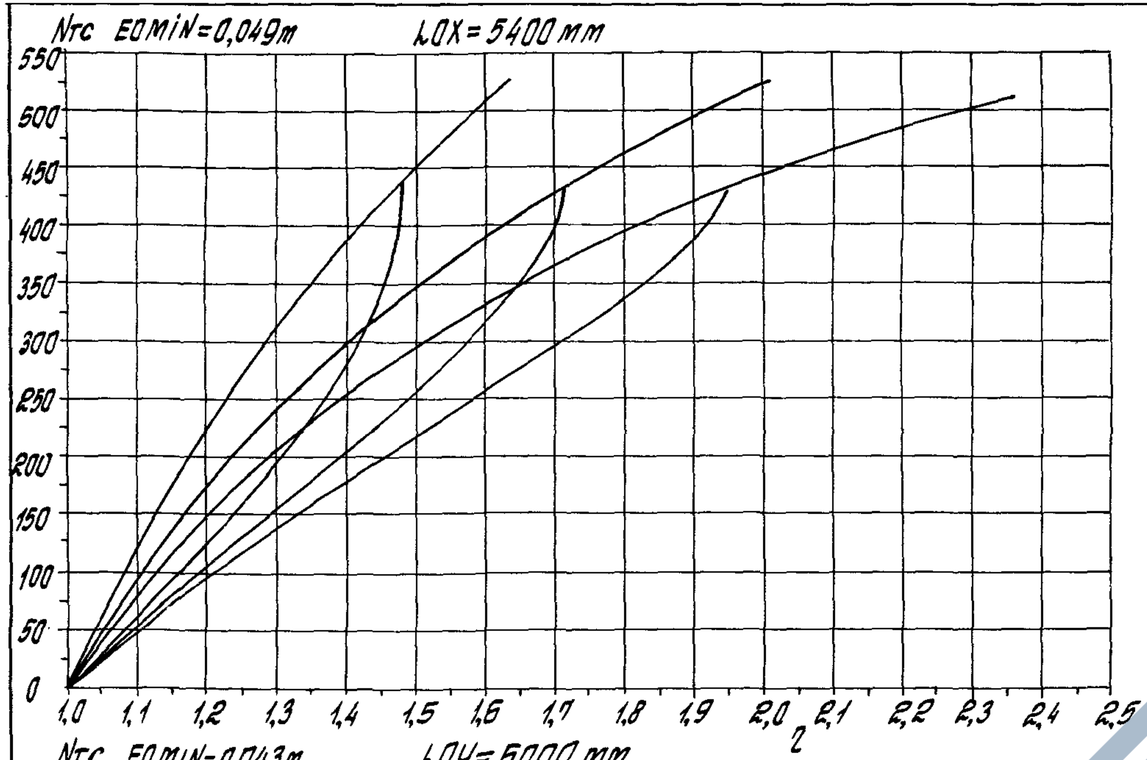
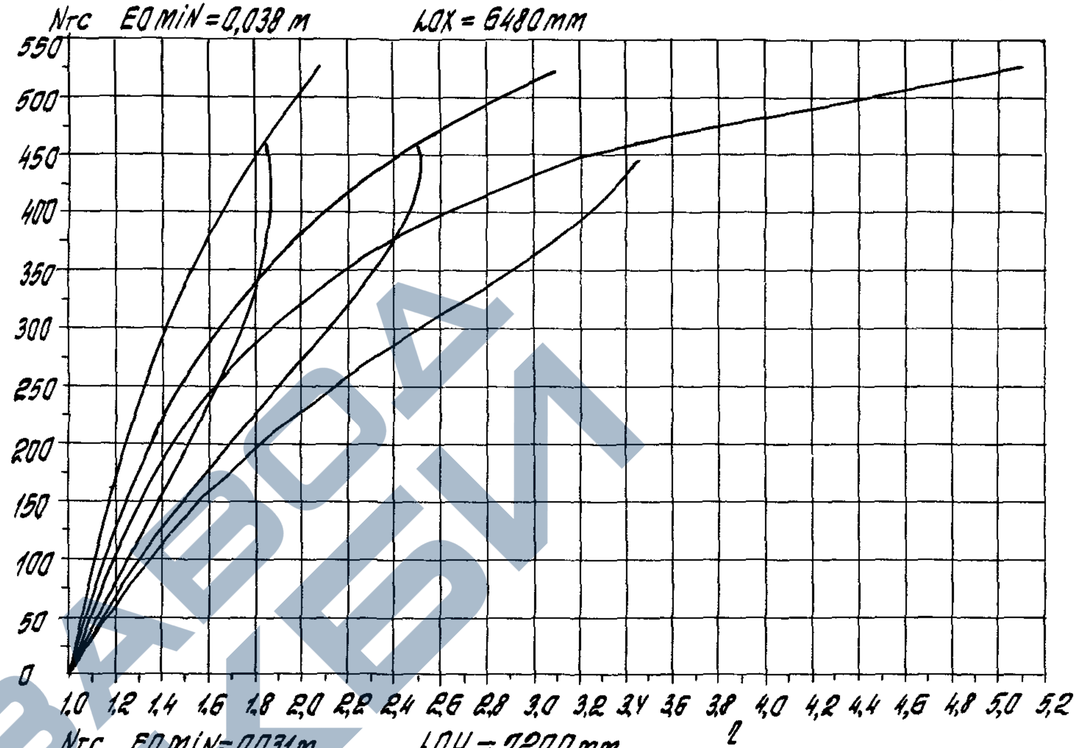
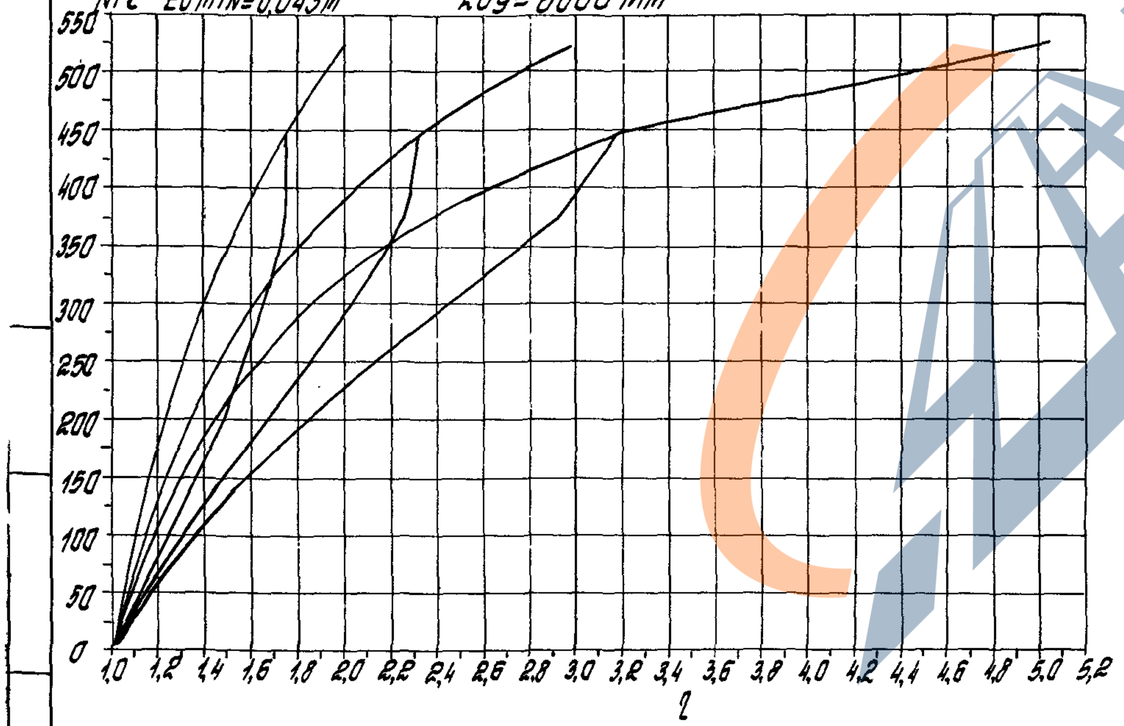
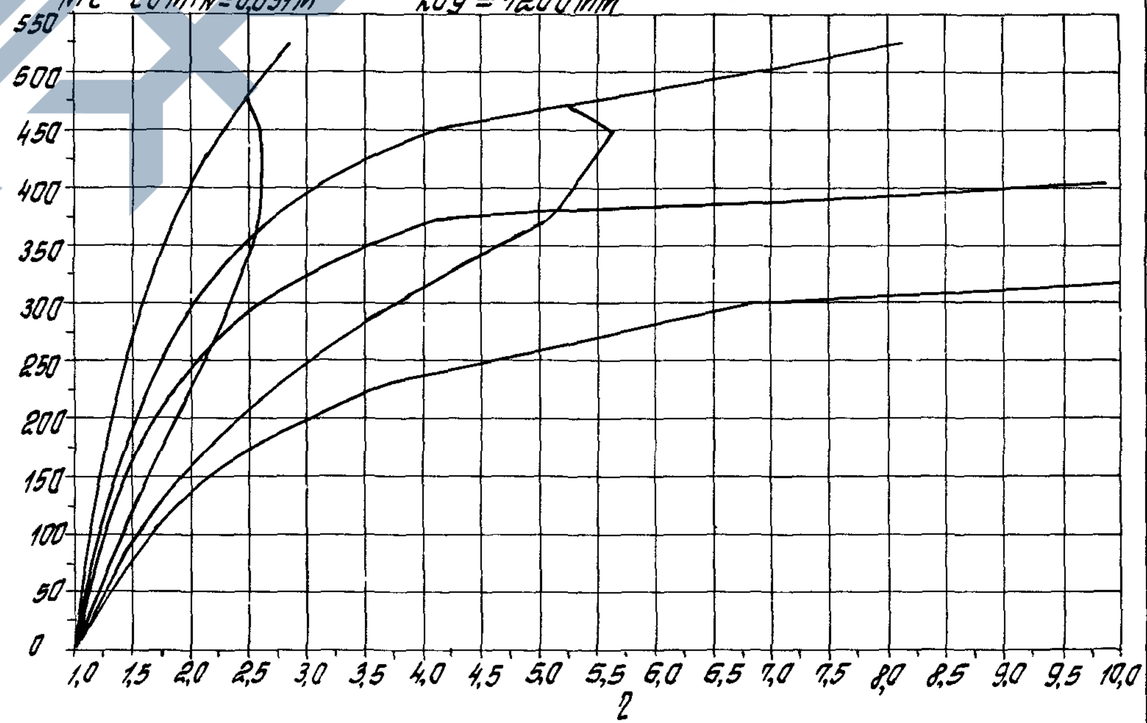
https://zavodjbi.com/

https://zavodjbi.com/









1.020 1-4 0-9 002	Лист 244

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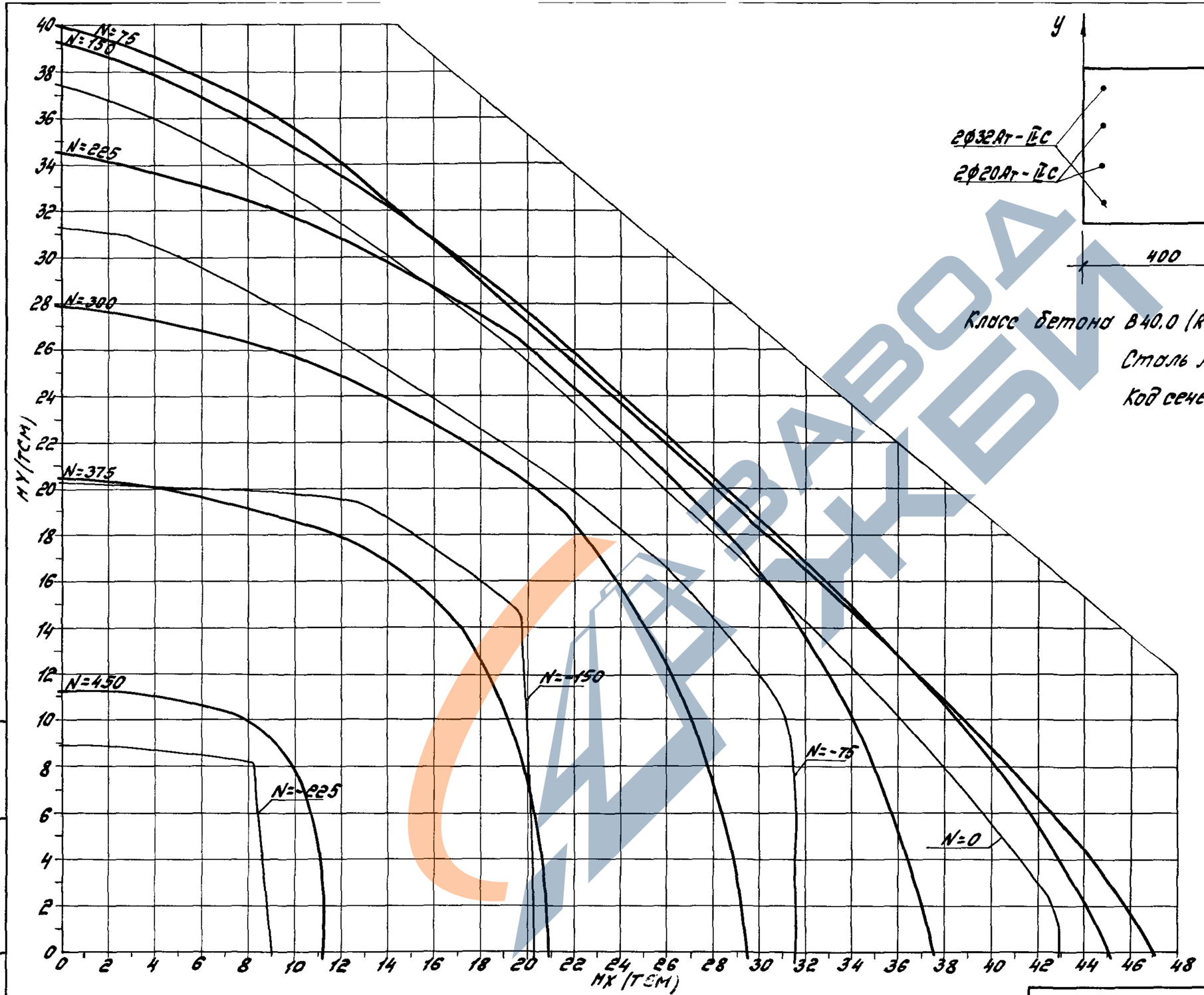
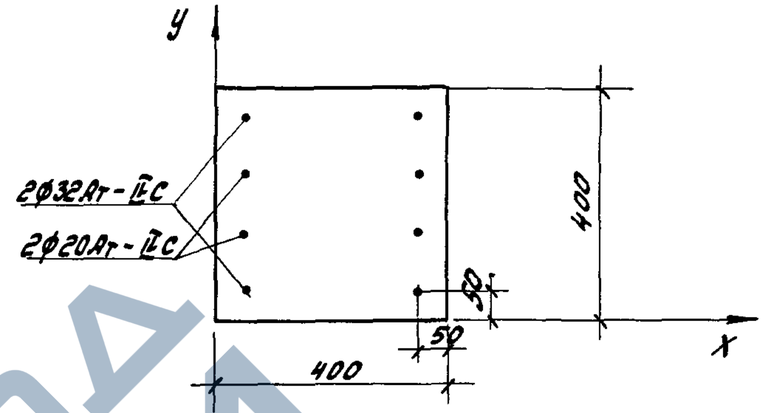
https://zavodjbi.com/





Класс бетона В40.0 ($R_в$ = 19,8 МПа при учёте $\gamma_{в2}$ = 0.90)

Сталь Ат-IIC

Код сечения - 131б

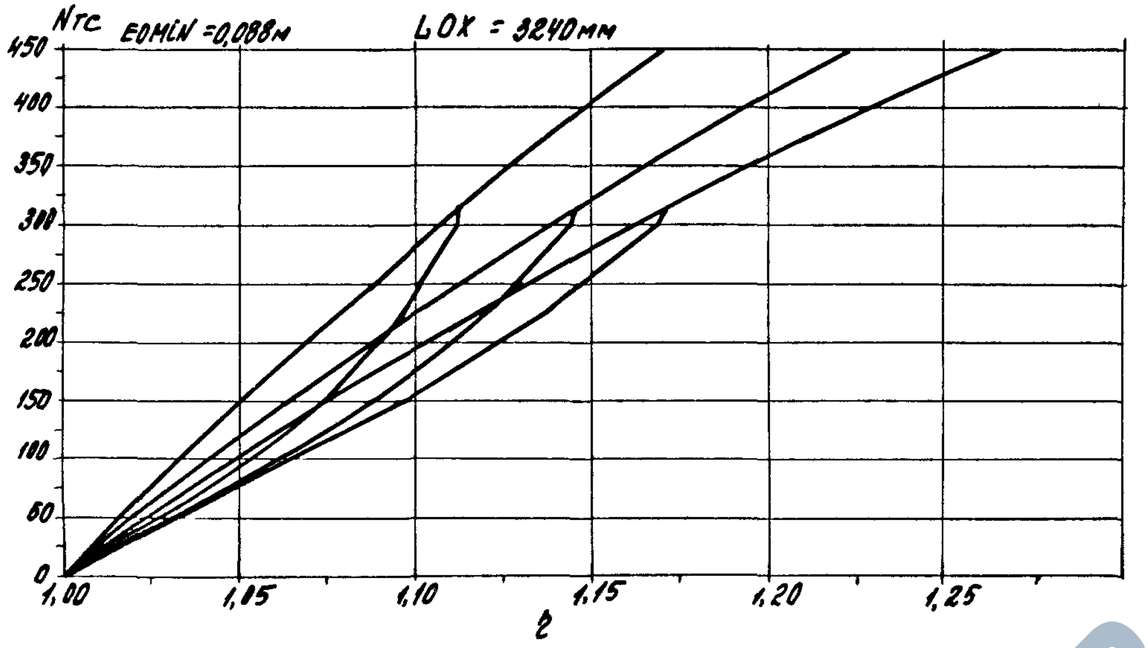
Инв. N подл.	Подпись и дата	Взам. инв. N

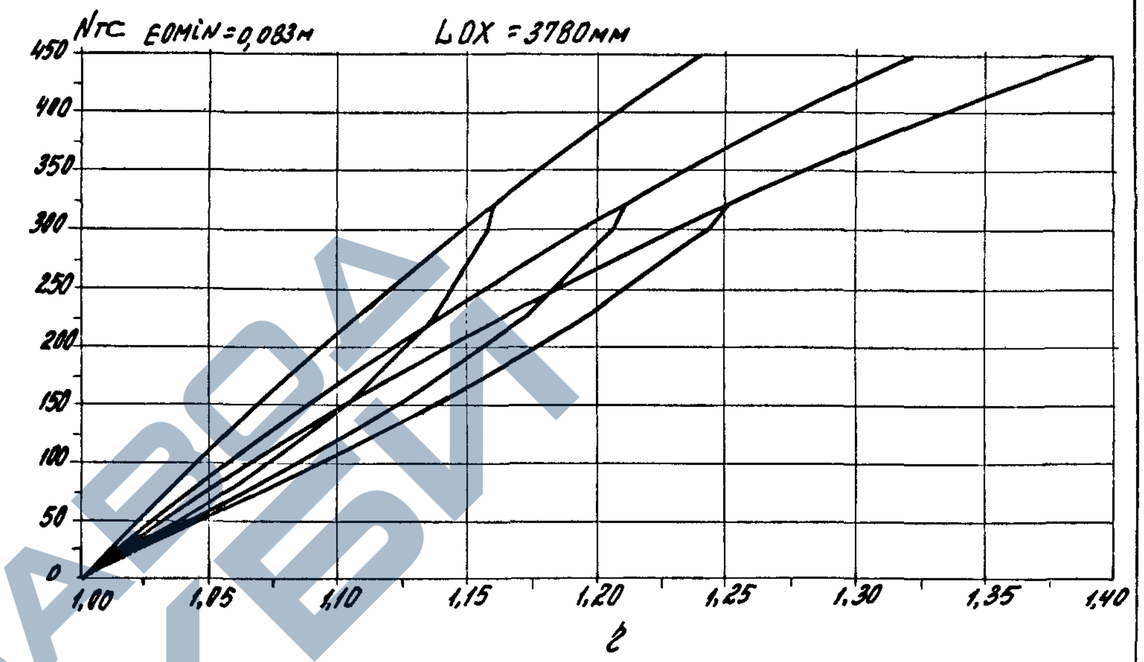
1.020. 1-4 0-9 002

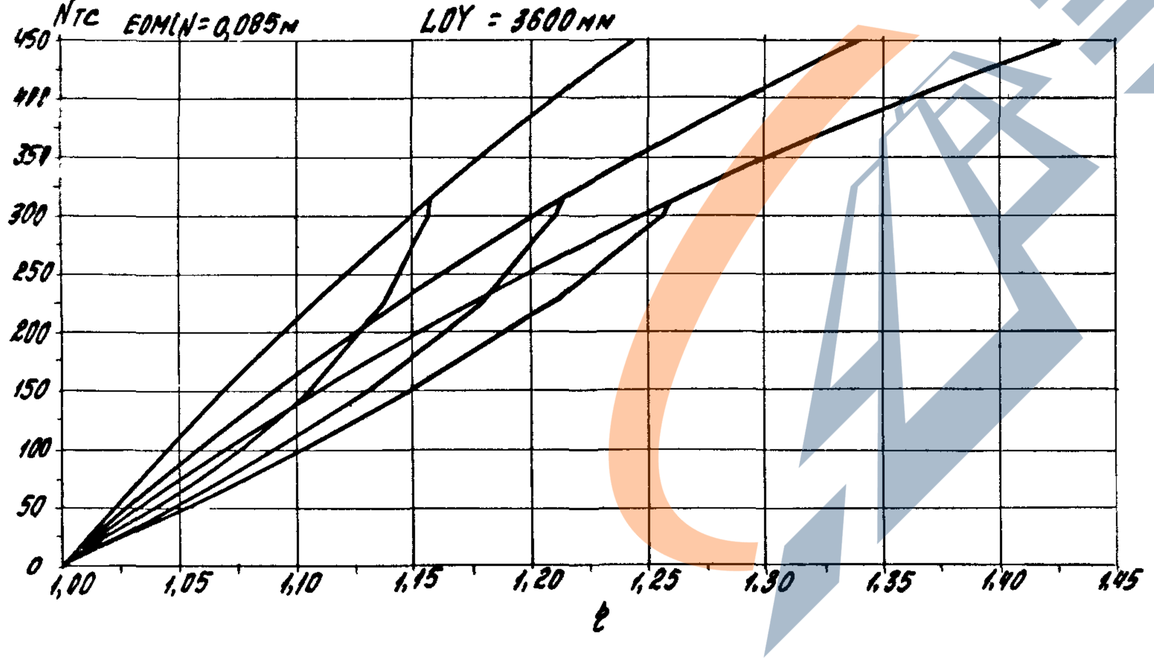
Лист 245

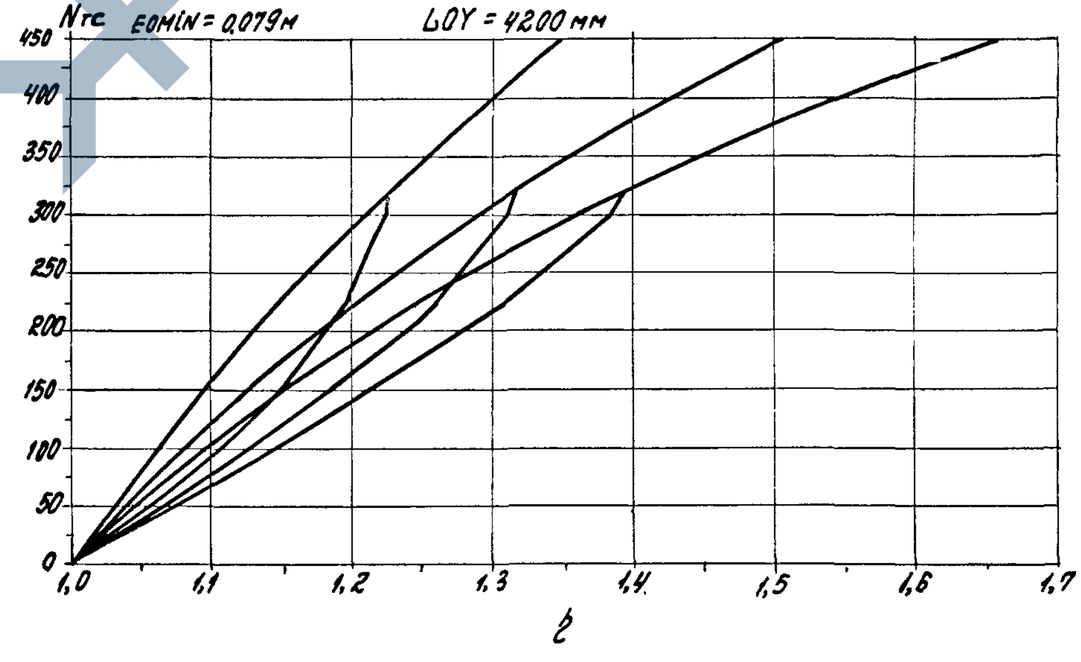
24166-08 22

https://zavodjbi.com/









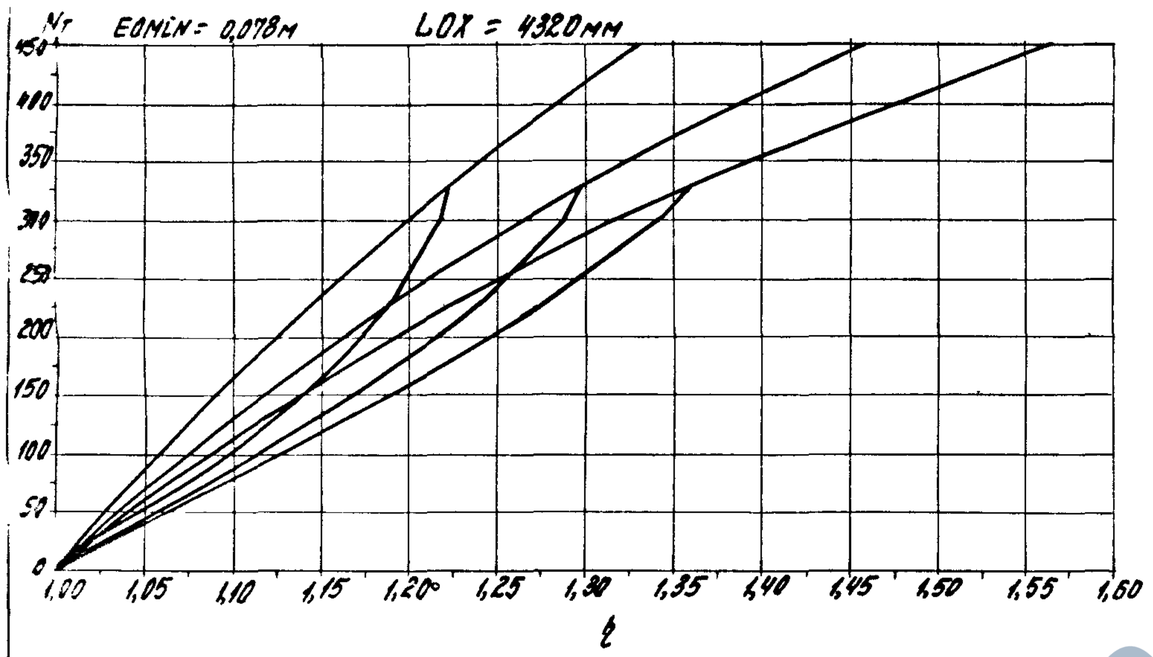
Инв.№ подл. | Подпись и дата | Взам.инв.№

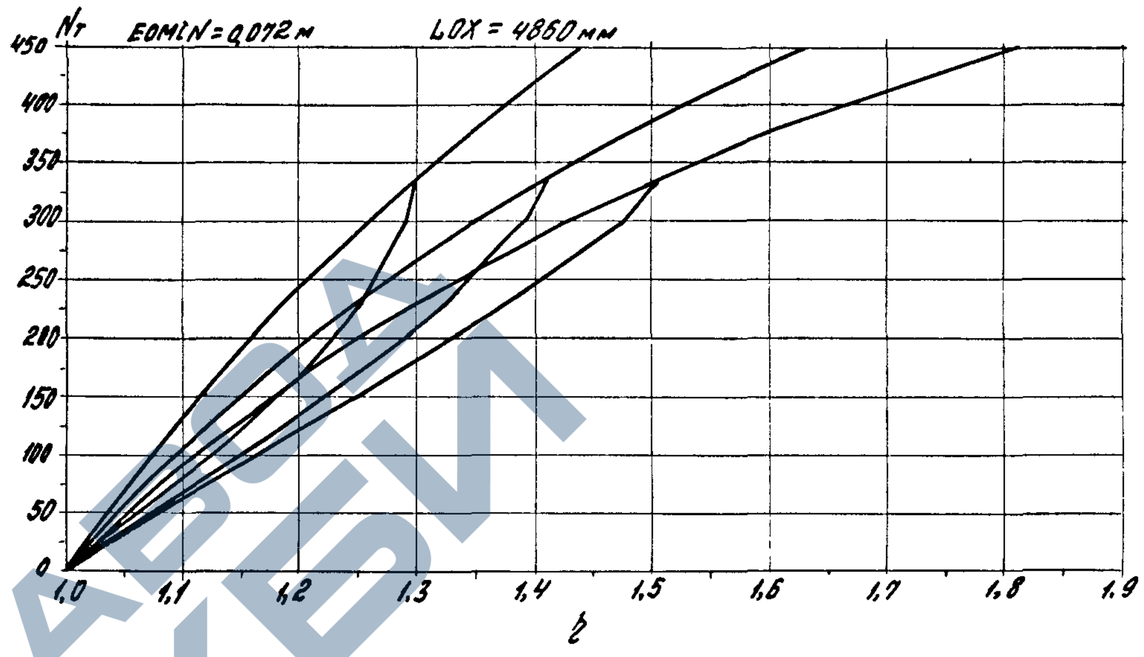
1.020.1-4. 0-9-002

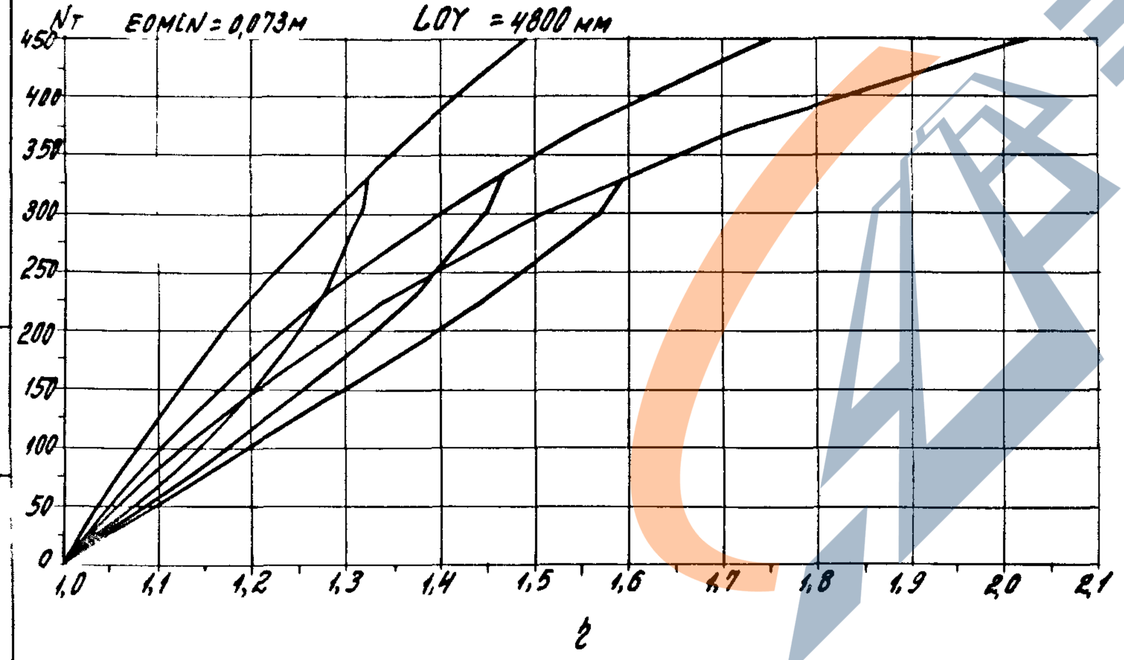
Лист 246

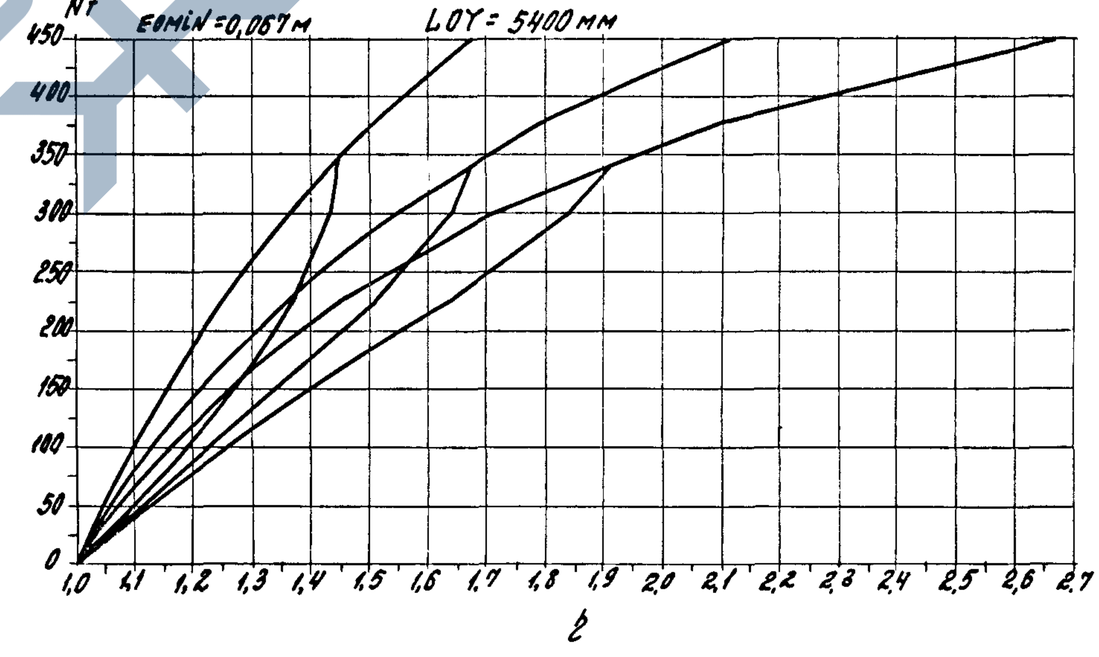
24166-03 23

https://zavodjbi.com/









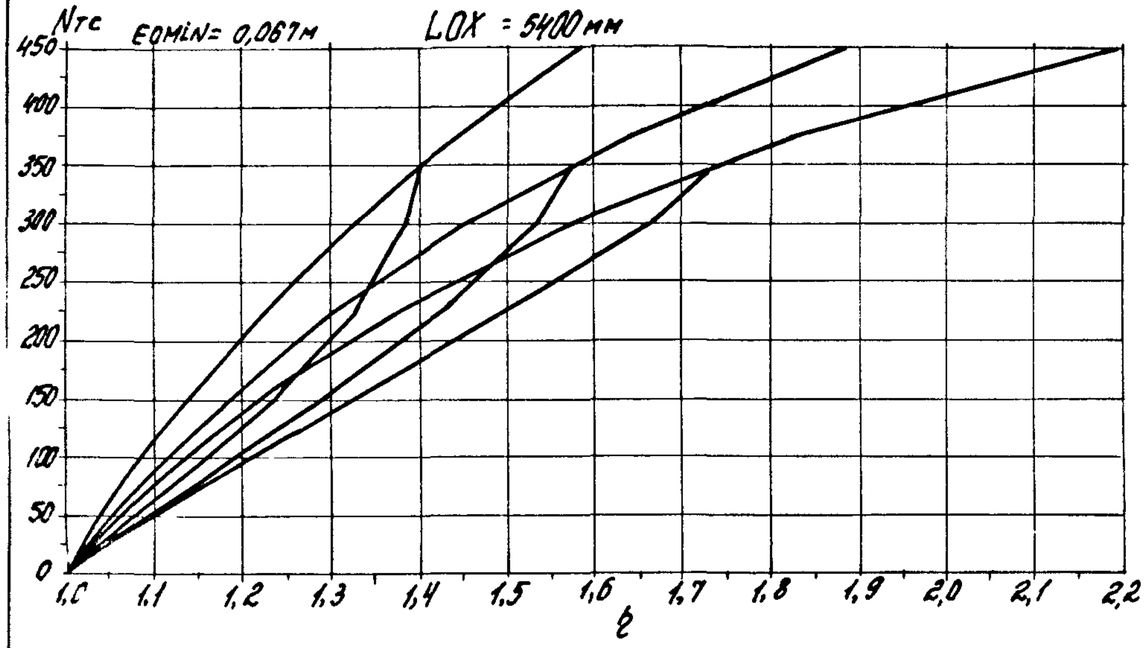
Инв.№ подл. | Подпись и дата | Взам.инв.№

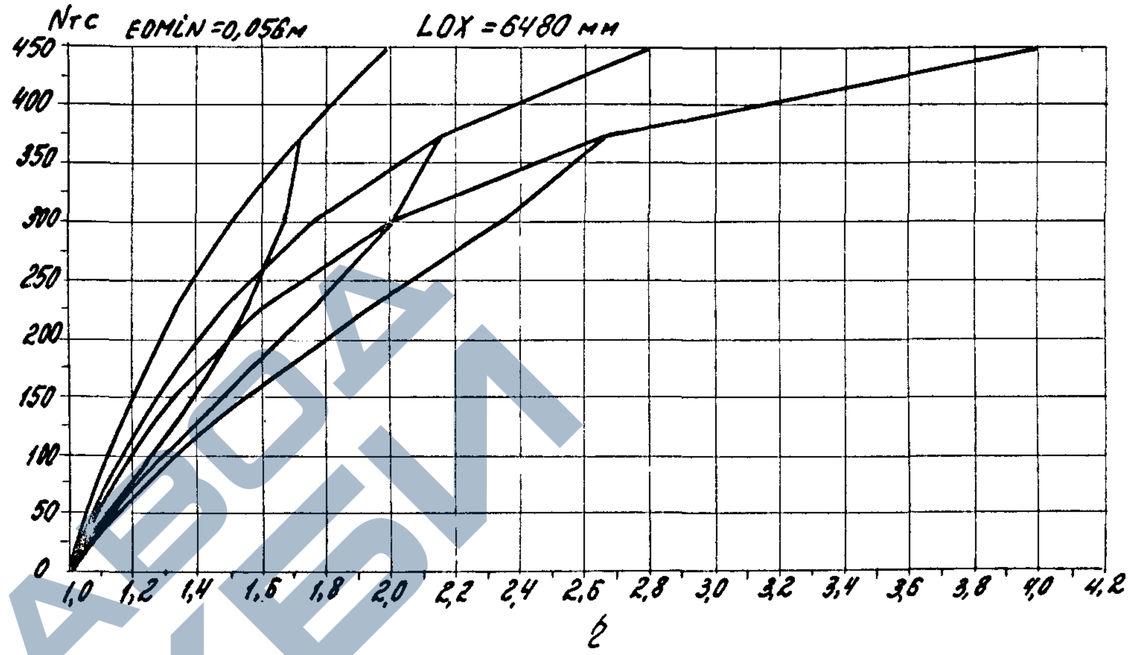
1.020.1-4. 0-9-002	Лист 247

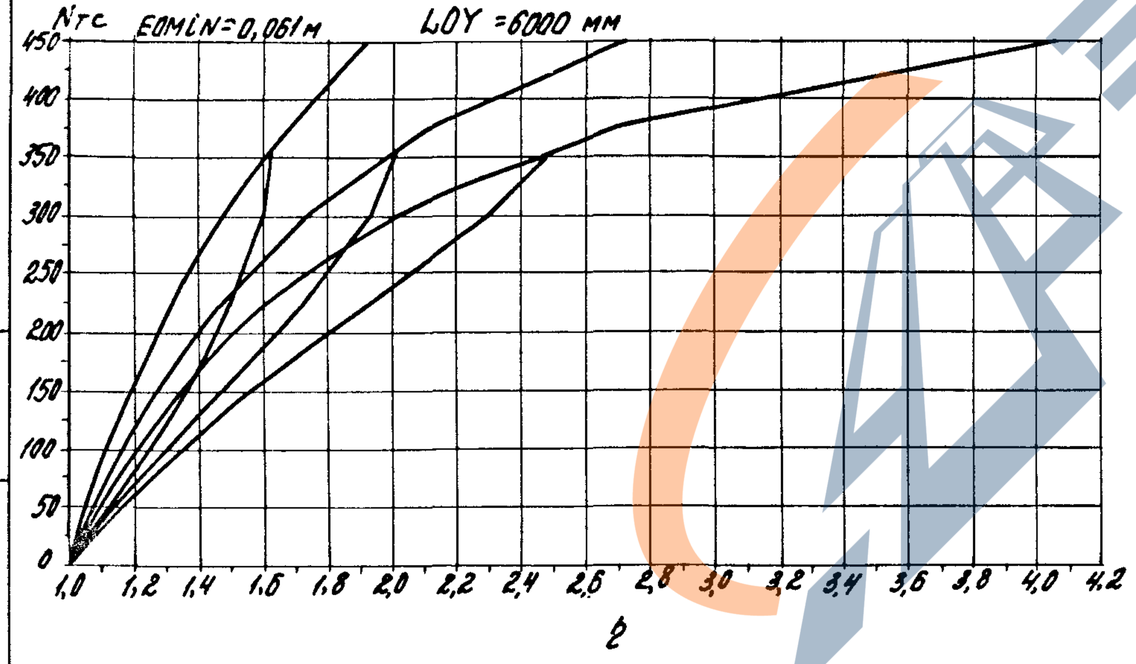
24166-03 24

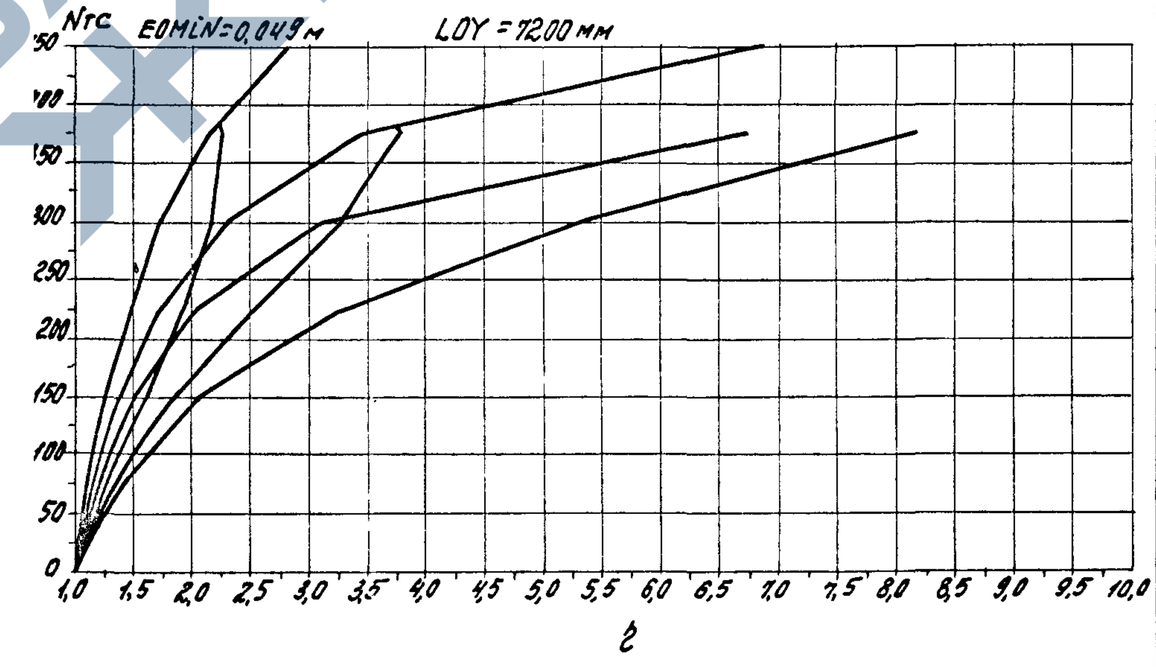
https://zavodjbi.com/

https://zavodjbi.com/









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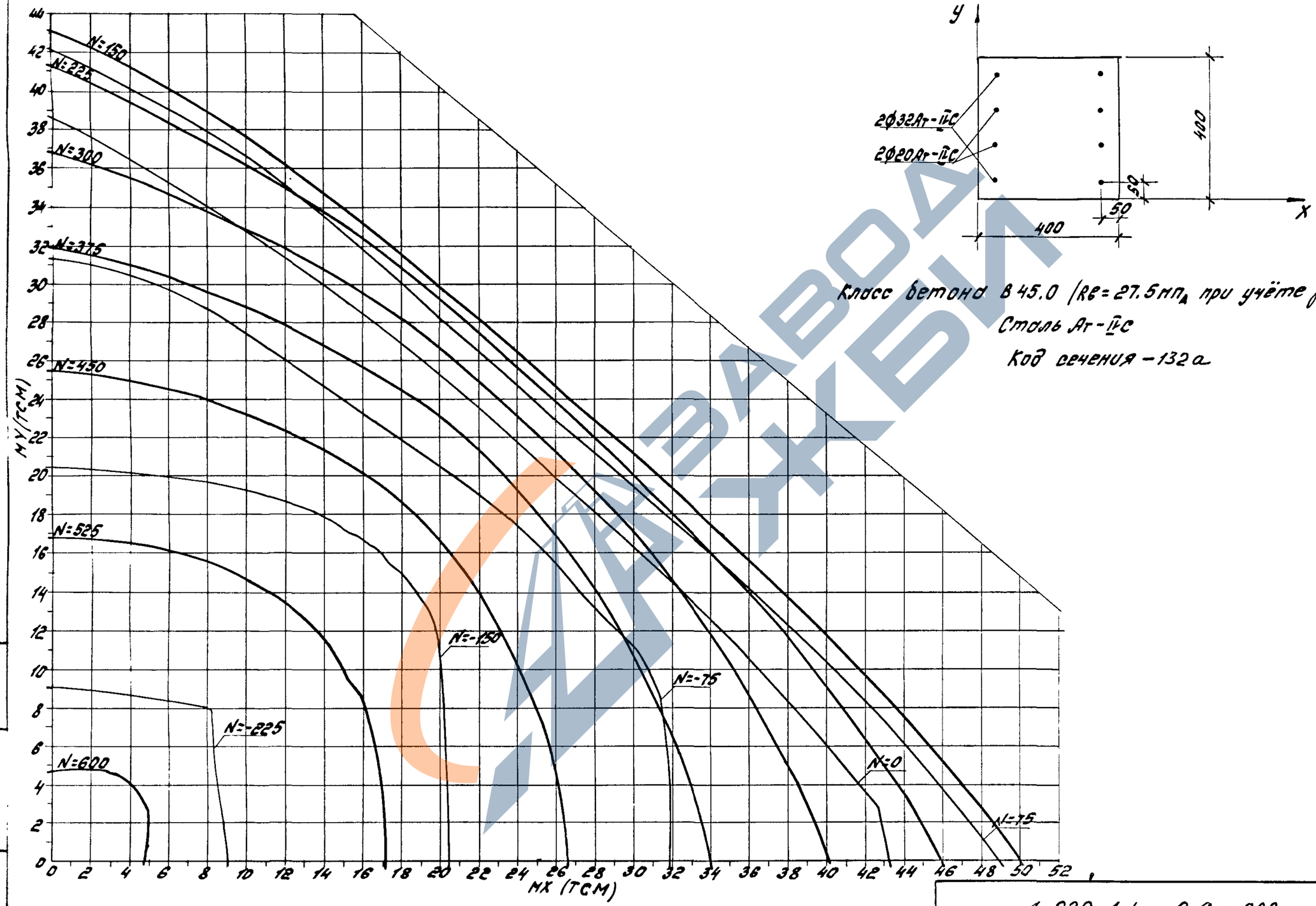
https://zavodjbi.com/



Класс бетона В 45.0 ($R_в$ = 27.5 мпа при учёте $\gamma_{в2}$ = 1.10)

Сталь Ат-IIIС

Код сечения – 132а

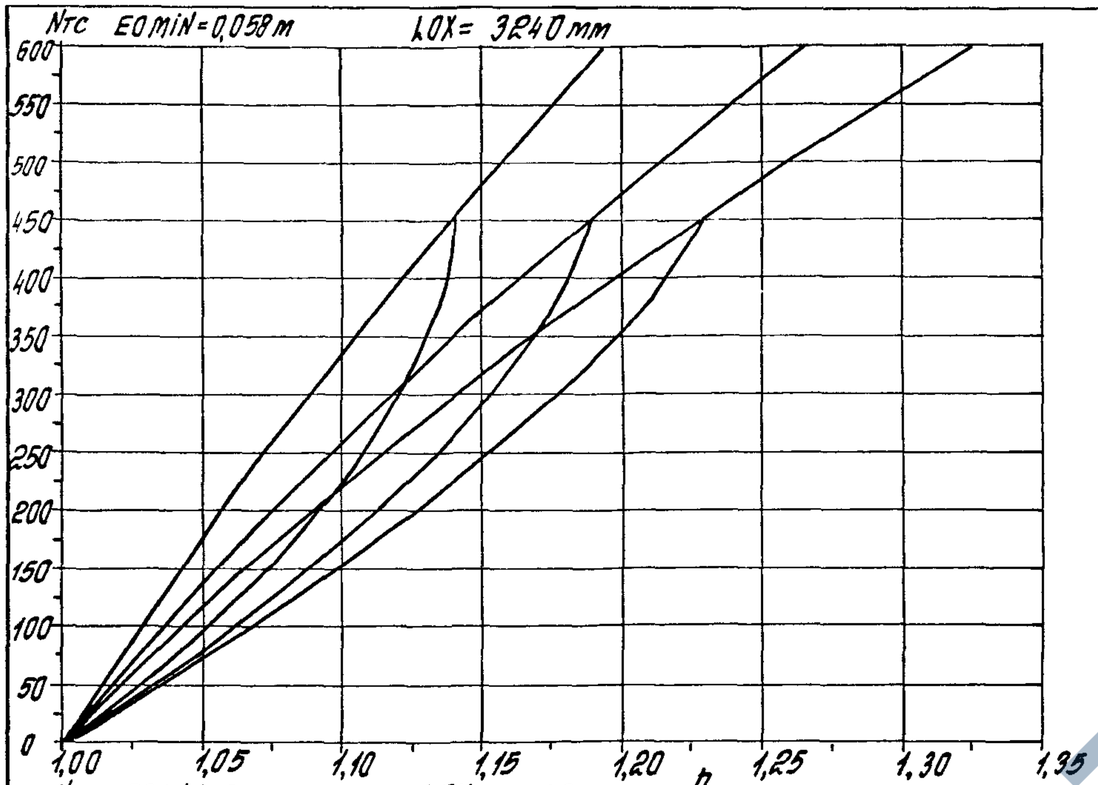
Инв.№ подл. | Подпись и дата | Взам. инв.№

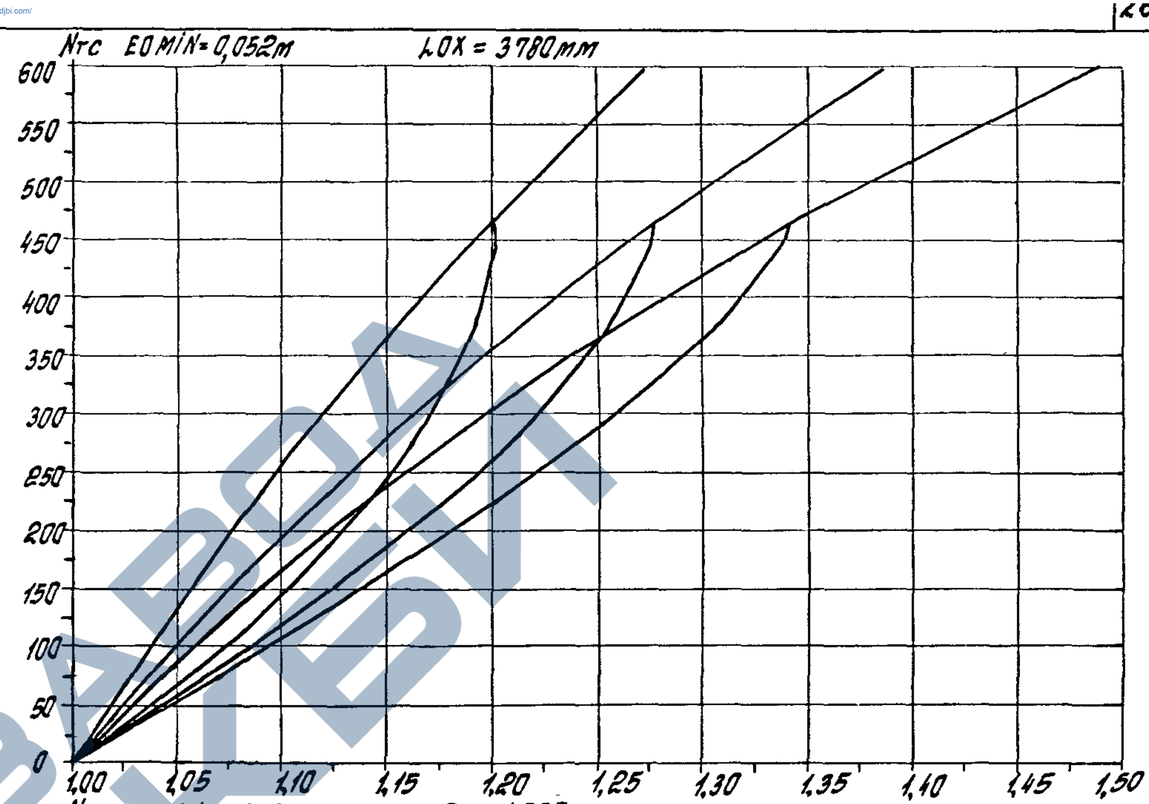
1. 020. 1-4. 0-9 - 002

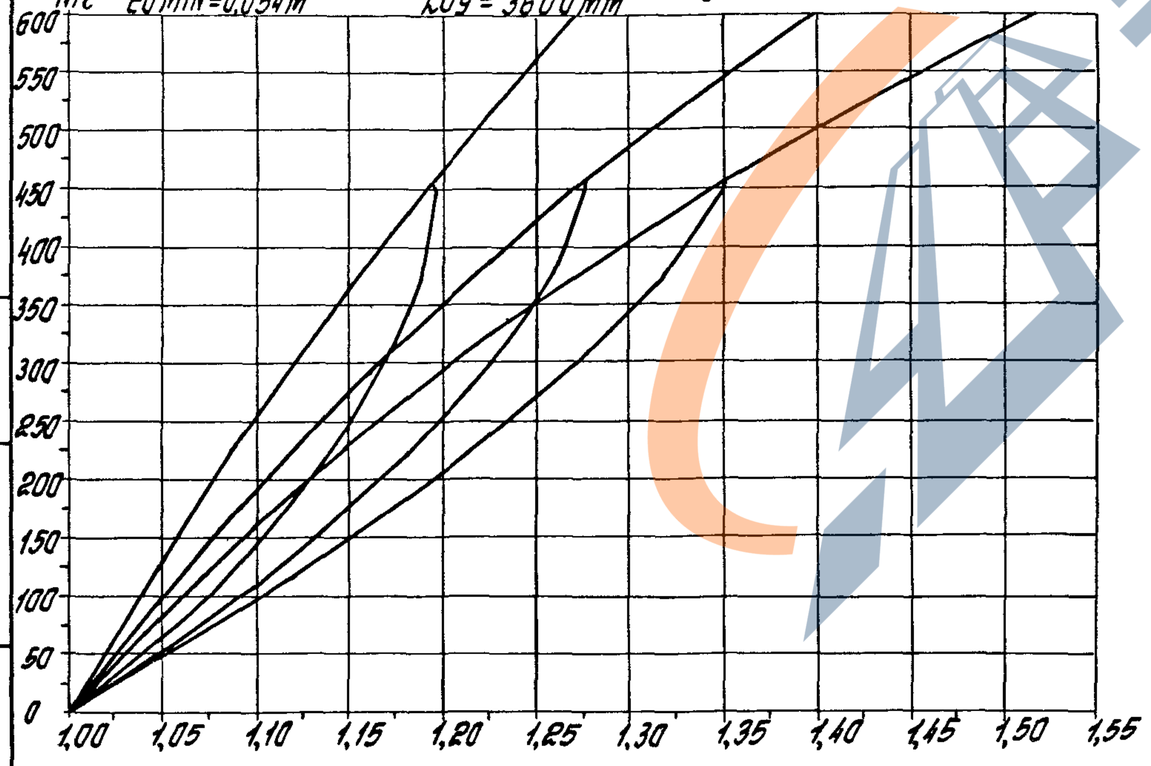
Лист 249

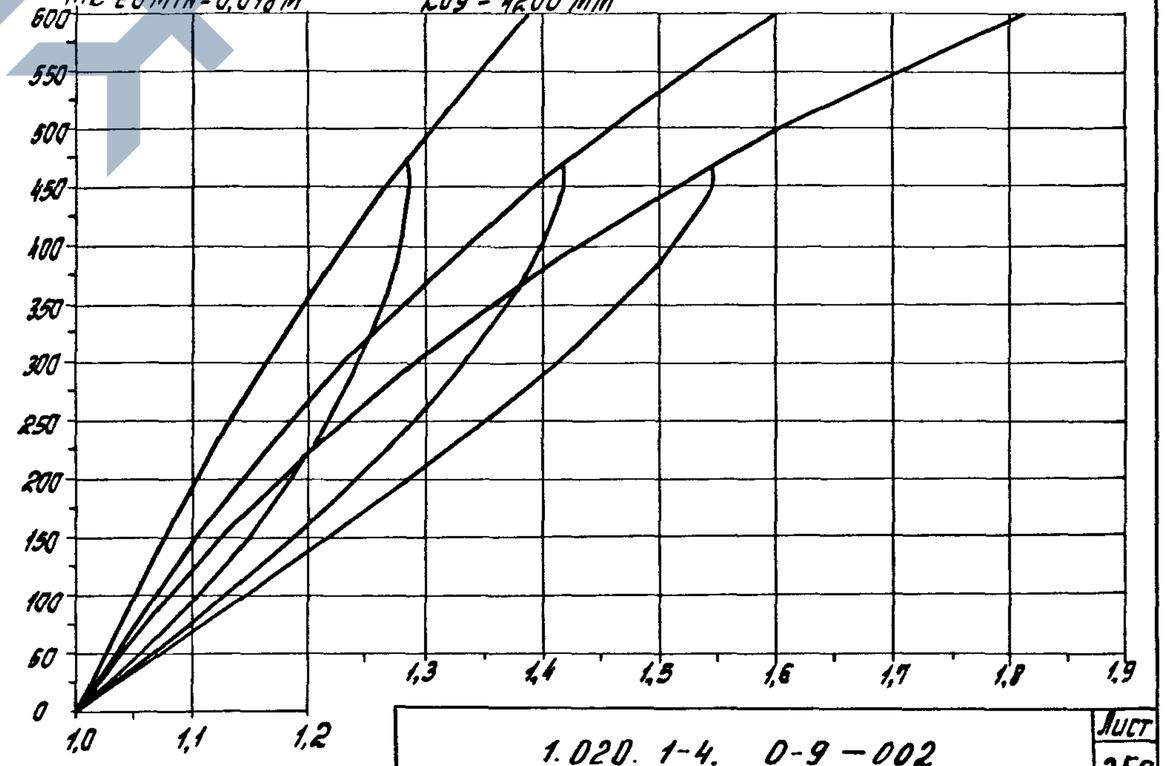
https://zavodjbi.com/

https://zavodjbi.com/









Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020. 1-4. 0-9 – 002

Лист 250

24166-03 27

https://zavodjbi.com/

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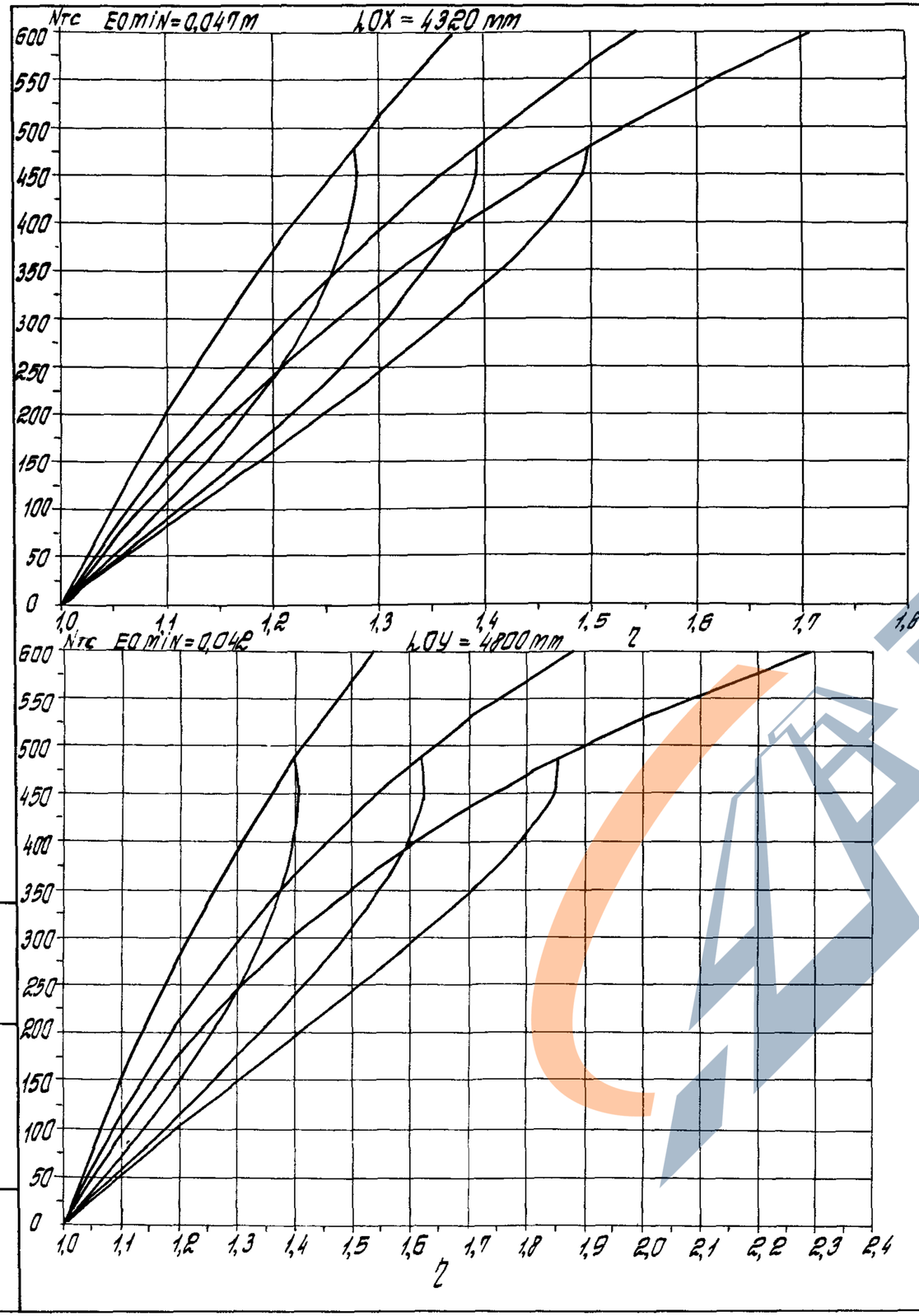

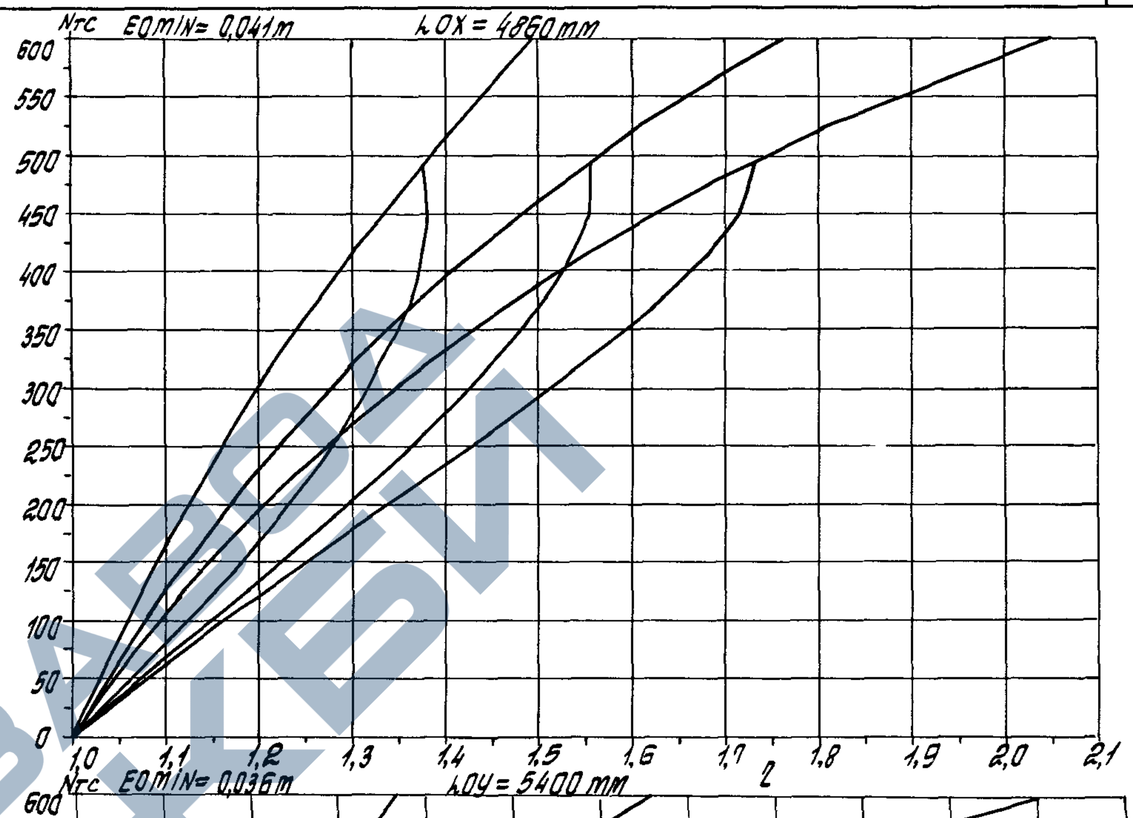

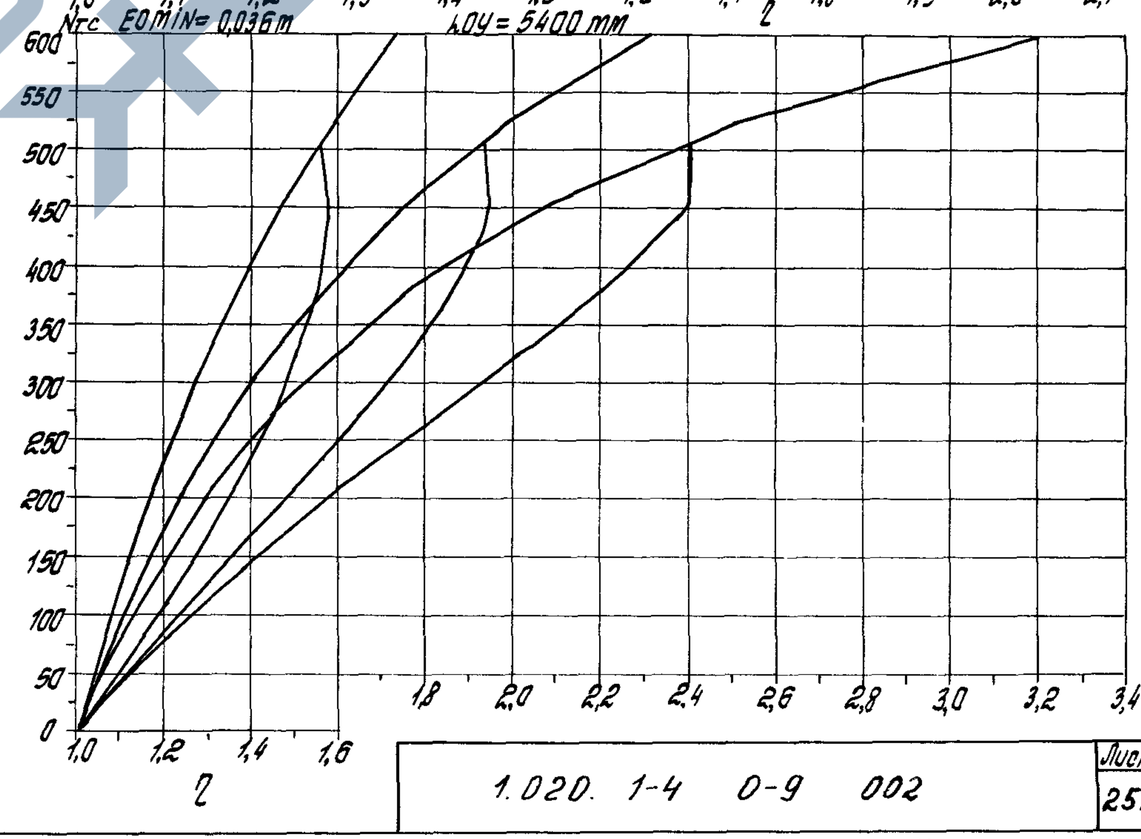

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020. 1-4 0-9 002

Лист 251

24166-08 28

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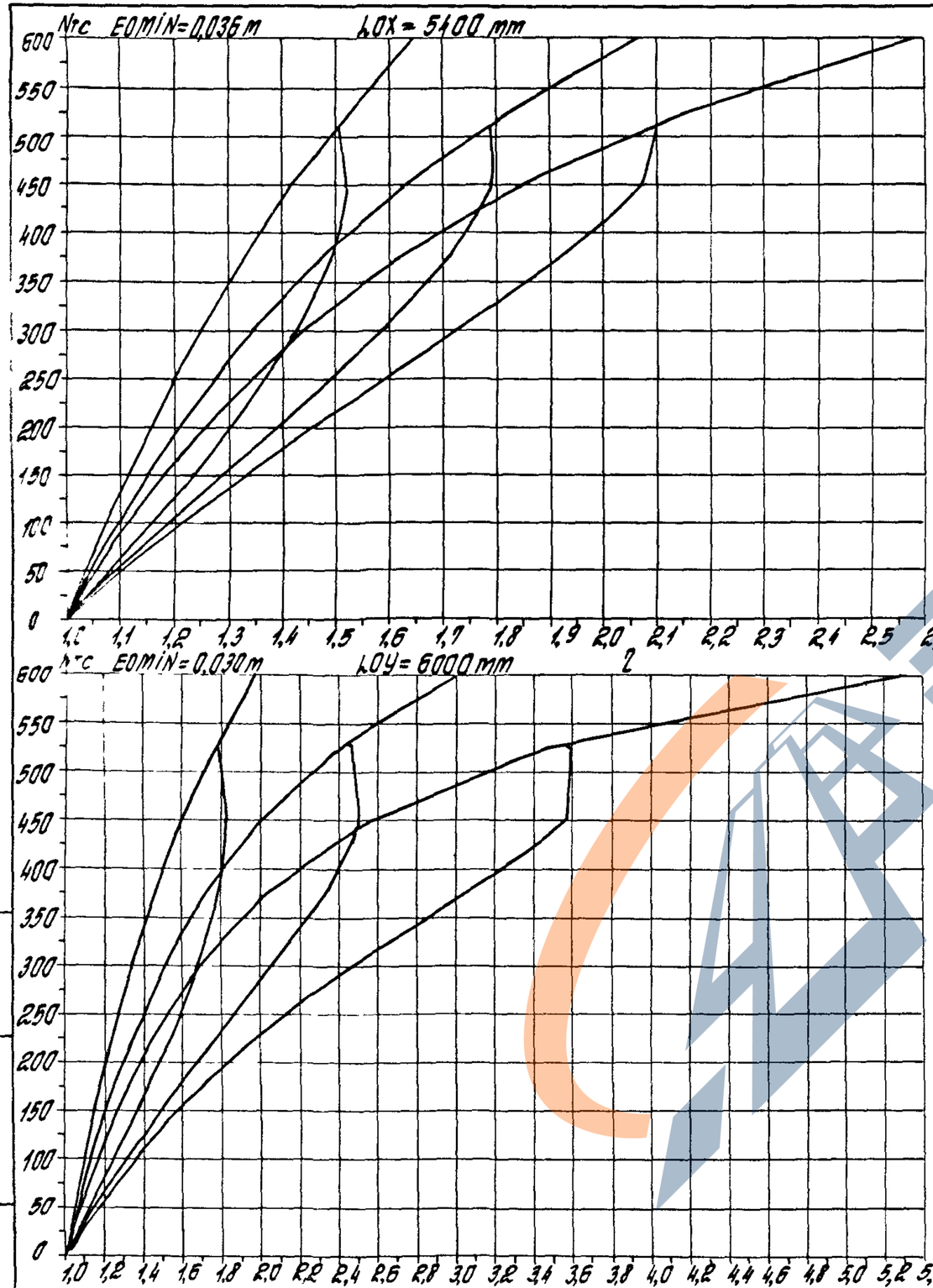
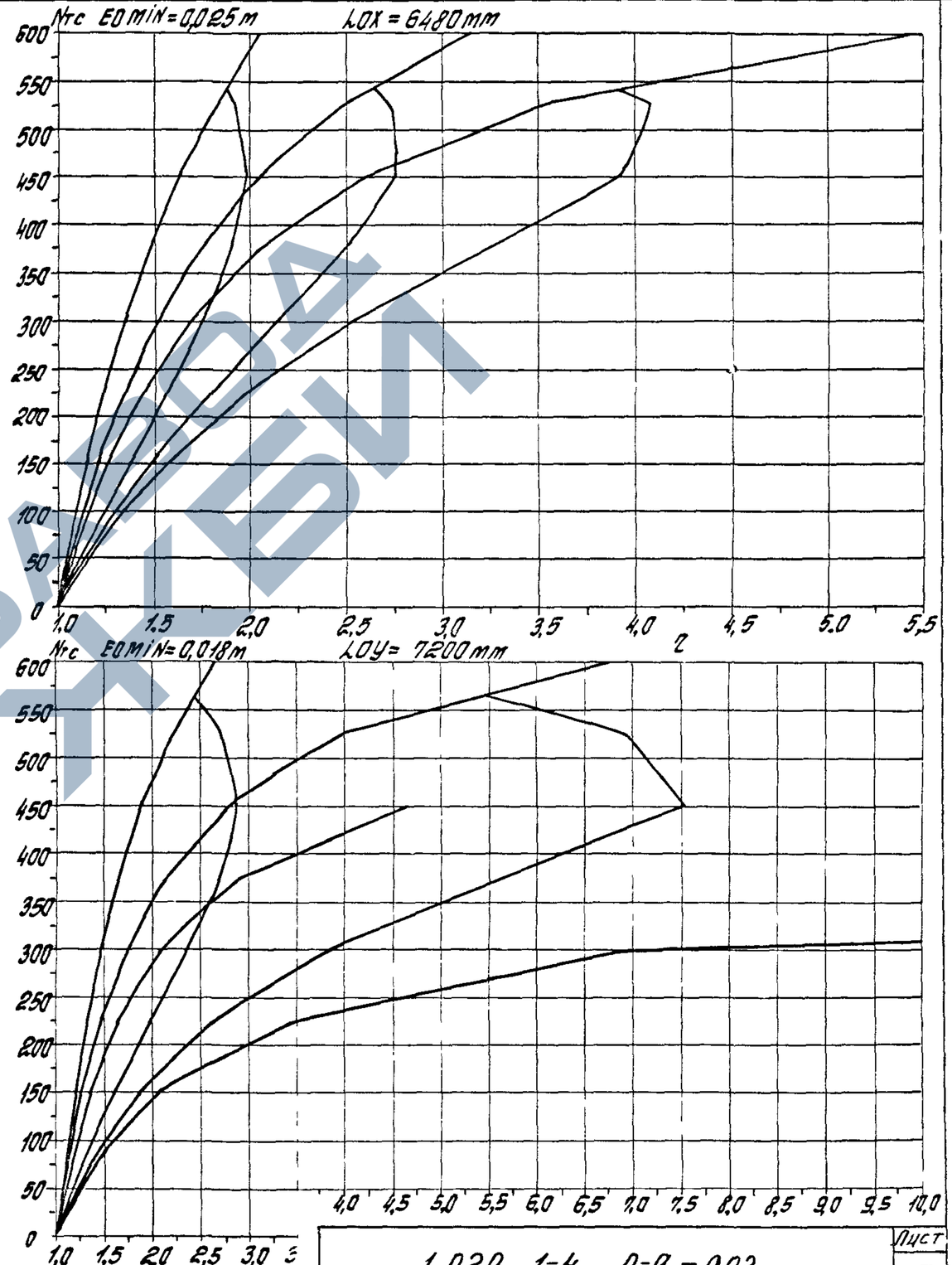




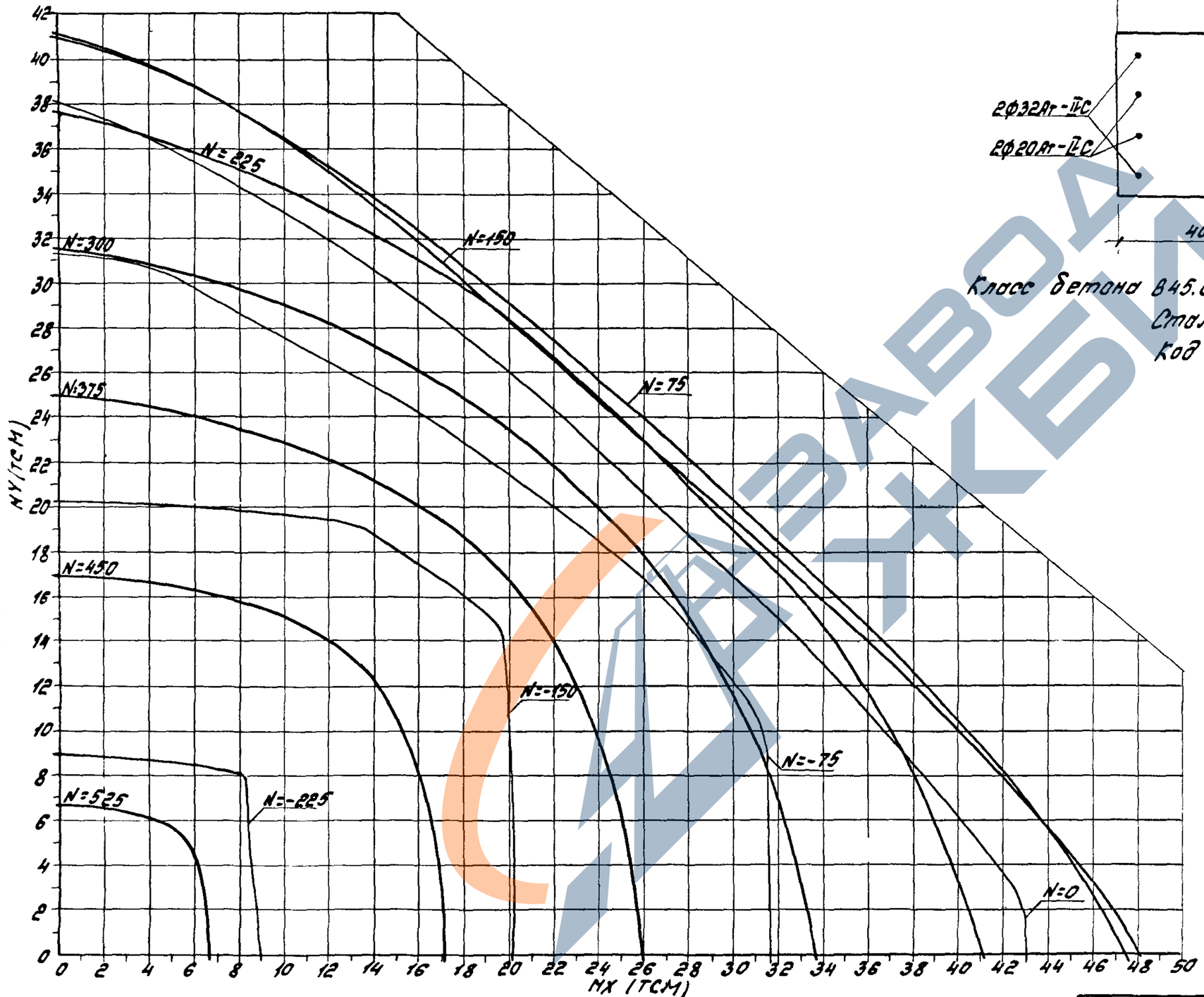
Инв.№ подл. | Подпись и дата | Взам.инв.№

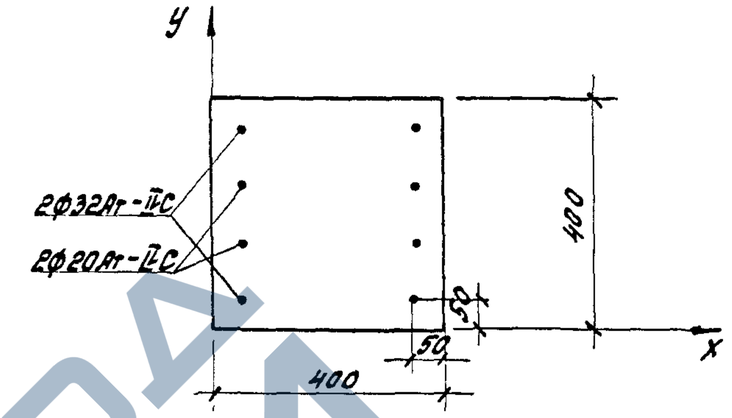
1.020. 1-4. 0-9 – 002

Лист 252

https://zavodjbi.com/

https://zavodjbi.com/





Класс бетона В45.0 ($R_в$= 22.5 мпа при учёте $\gamma_{в2}$=0.90)

Сталь Ат-IIC

Код сечения – 132 б

1.020. 1-4. 0-9-002	Лист 253

24166-03 30

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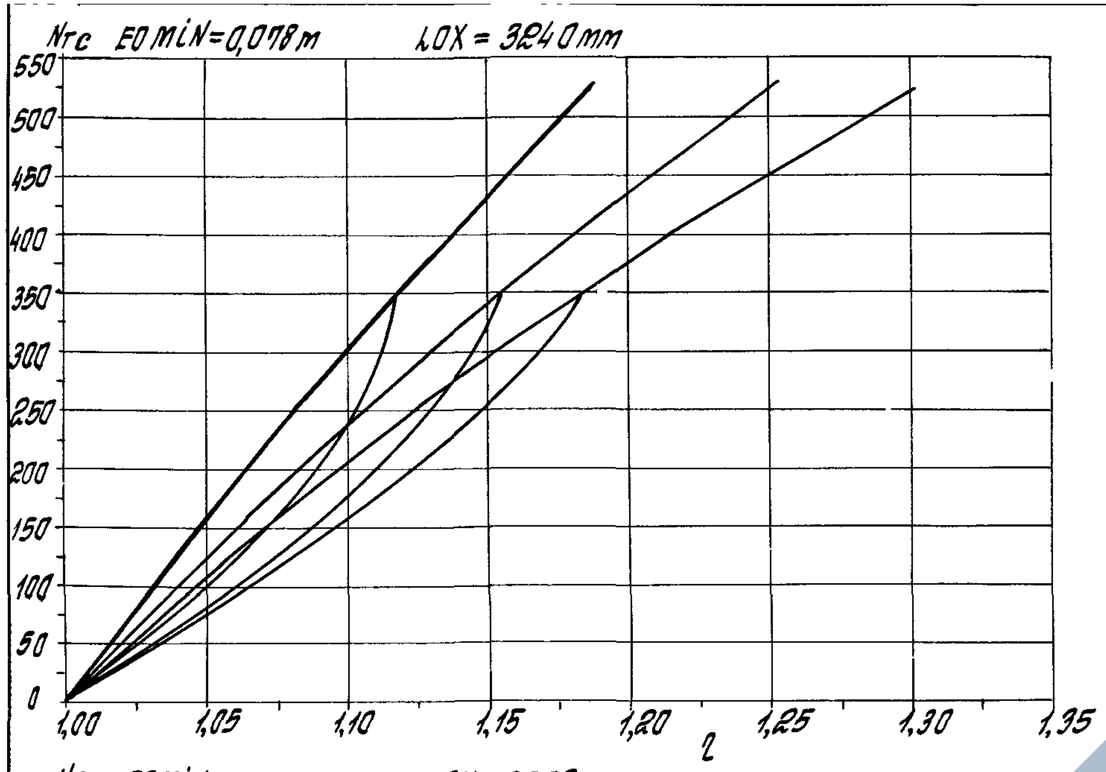
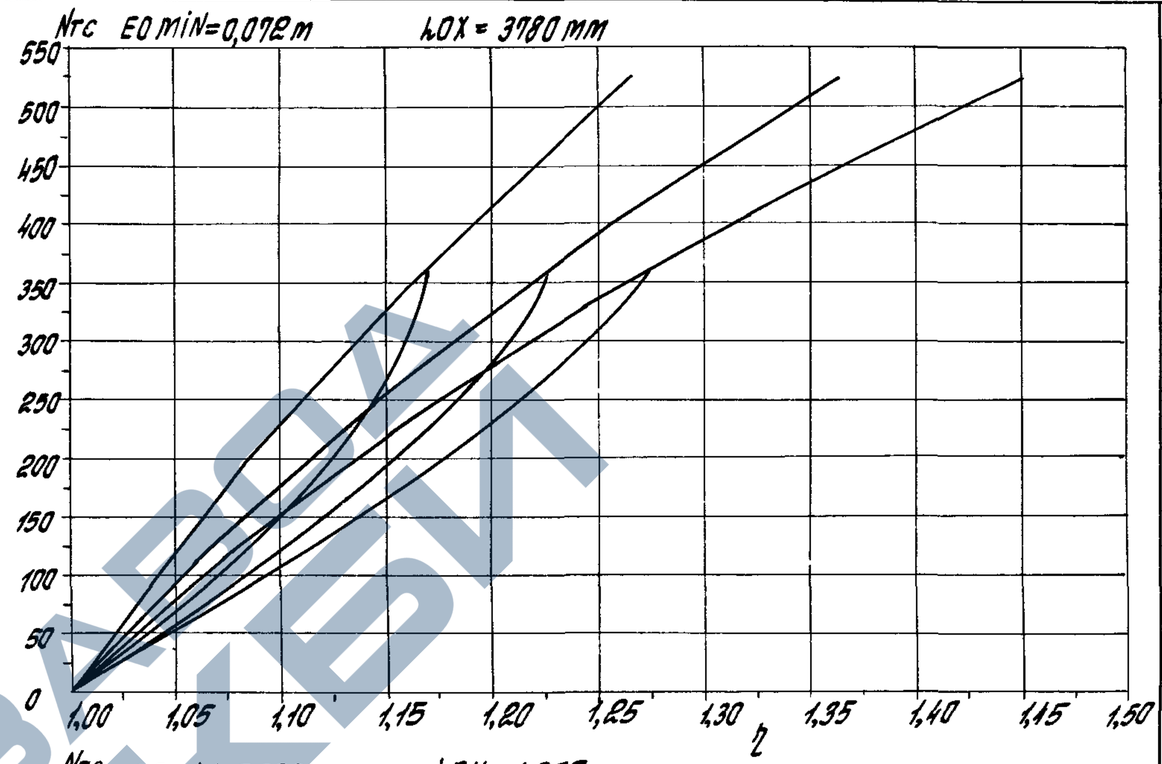
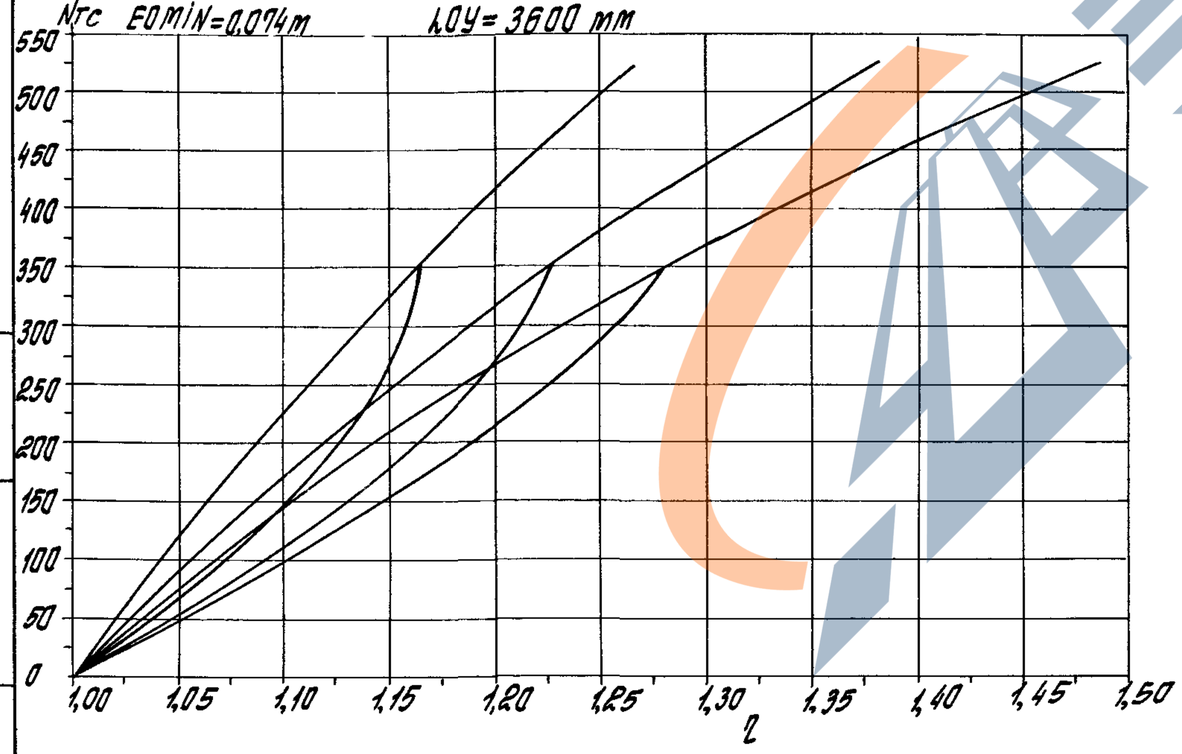
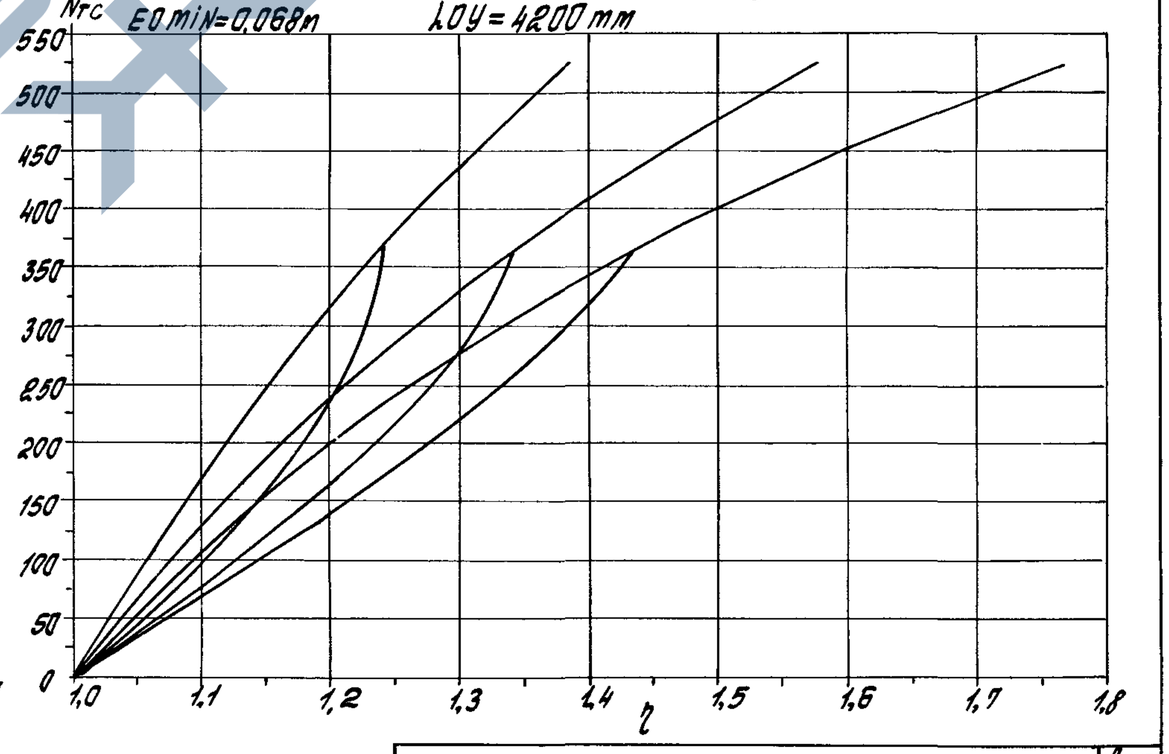






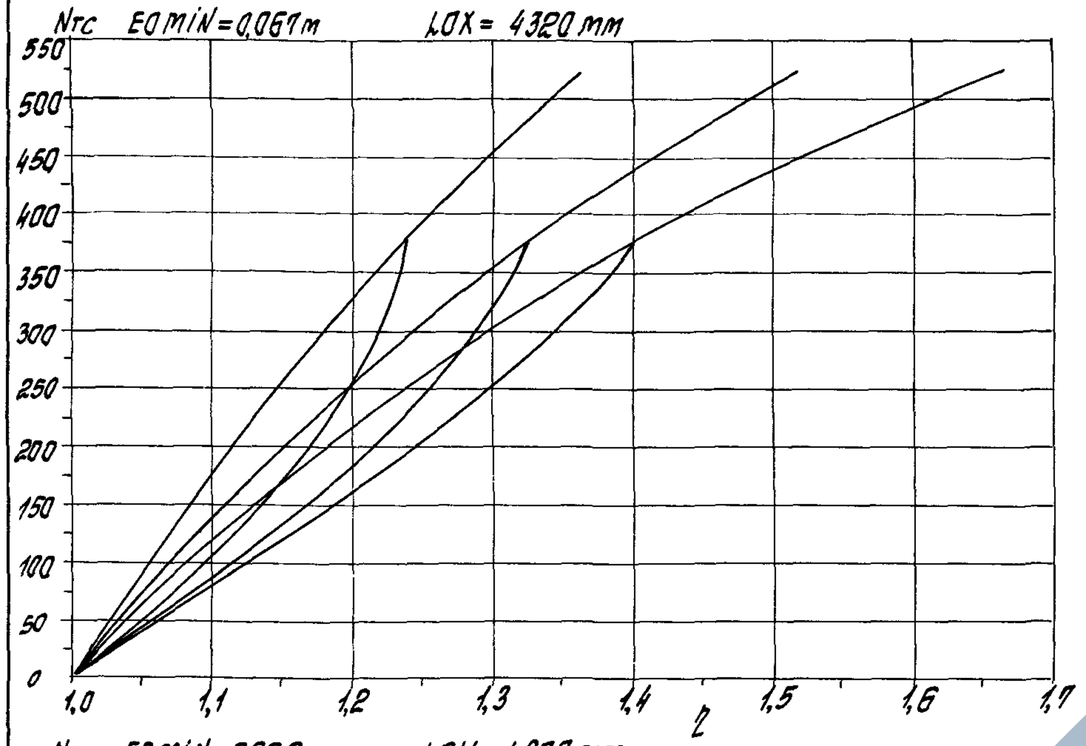


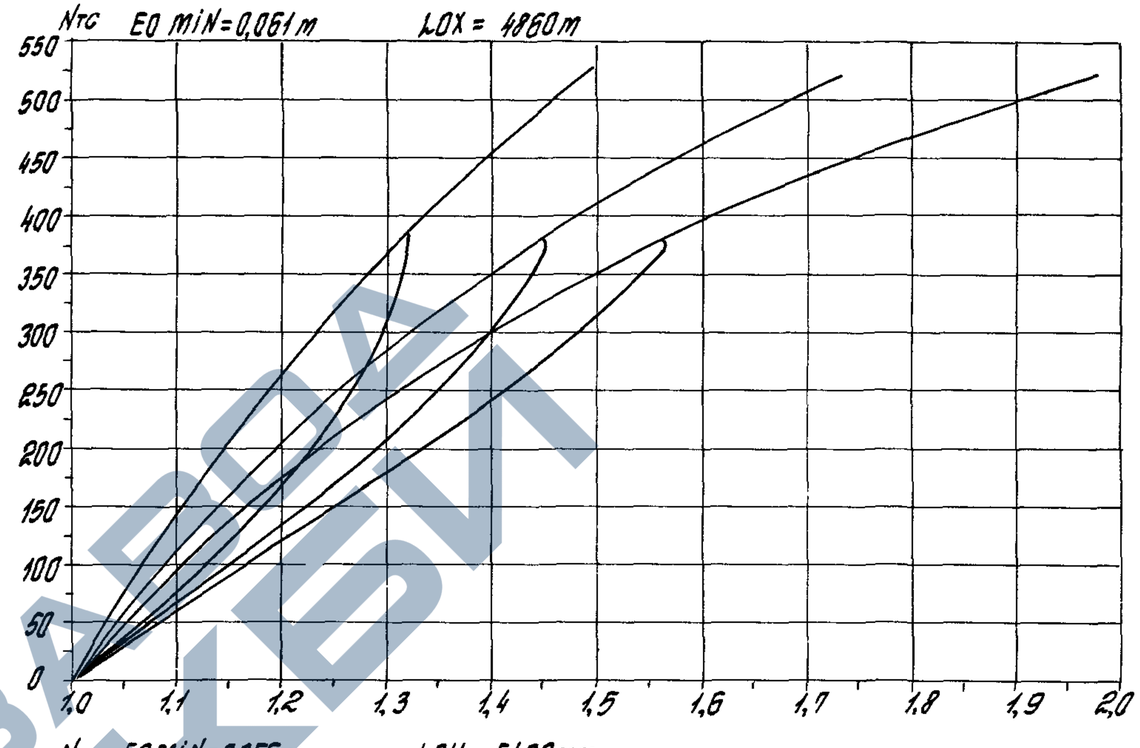
Инв. № подл. | Подпись и дата | Взам. инв. №

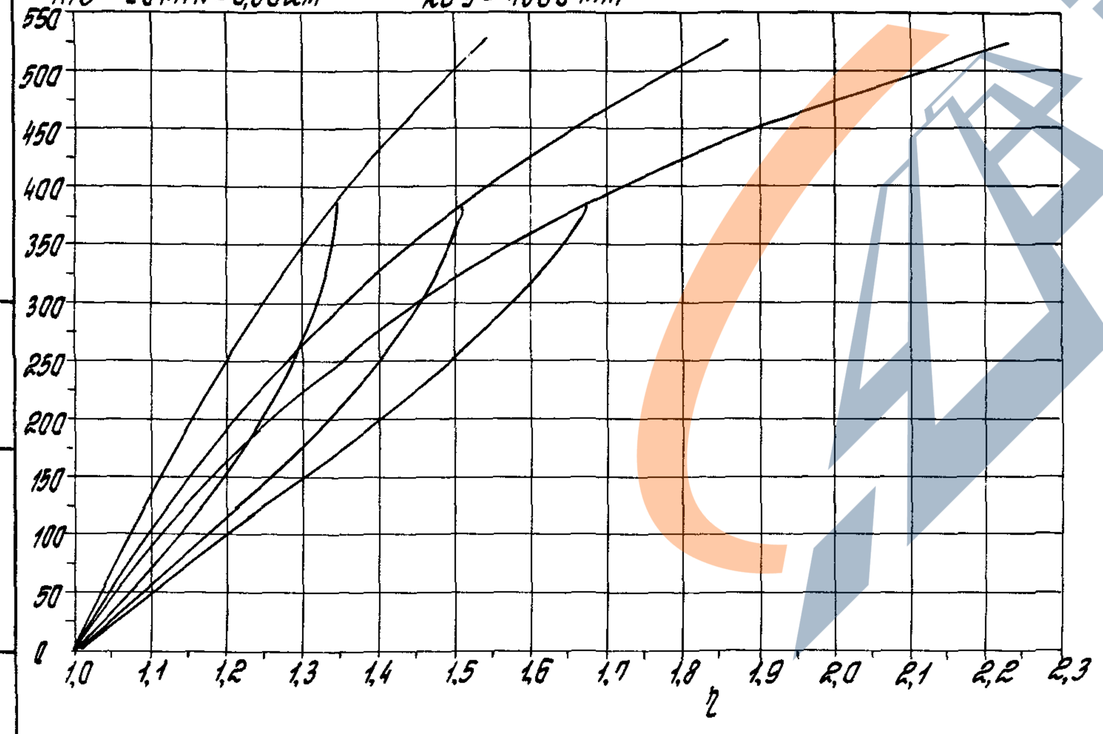
	1.020.1-4 0-9 002	Лист 254

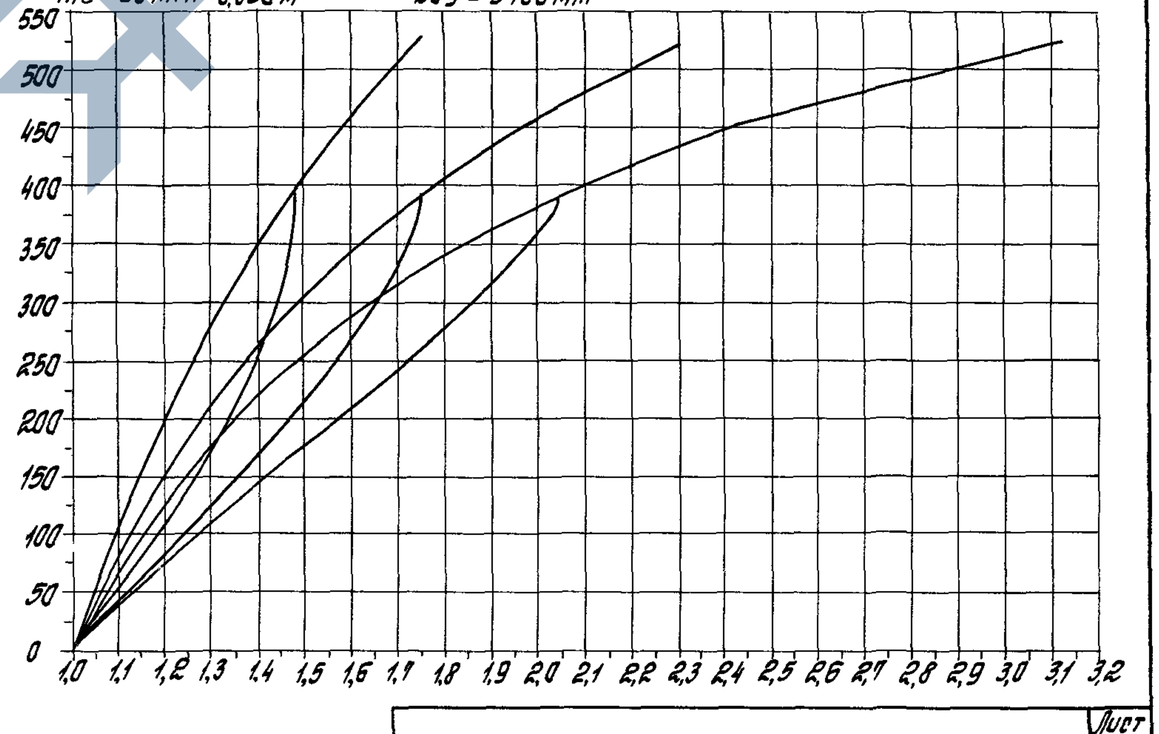
https://zavodjbi.com/

https://zavodjbi.com/









Инв.№ подл. | Подпись и дата | Взам. инв.№

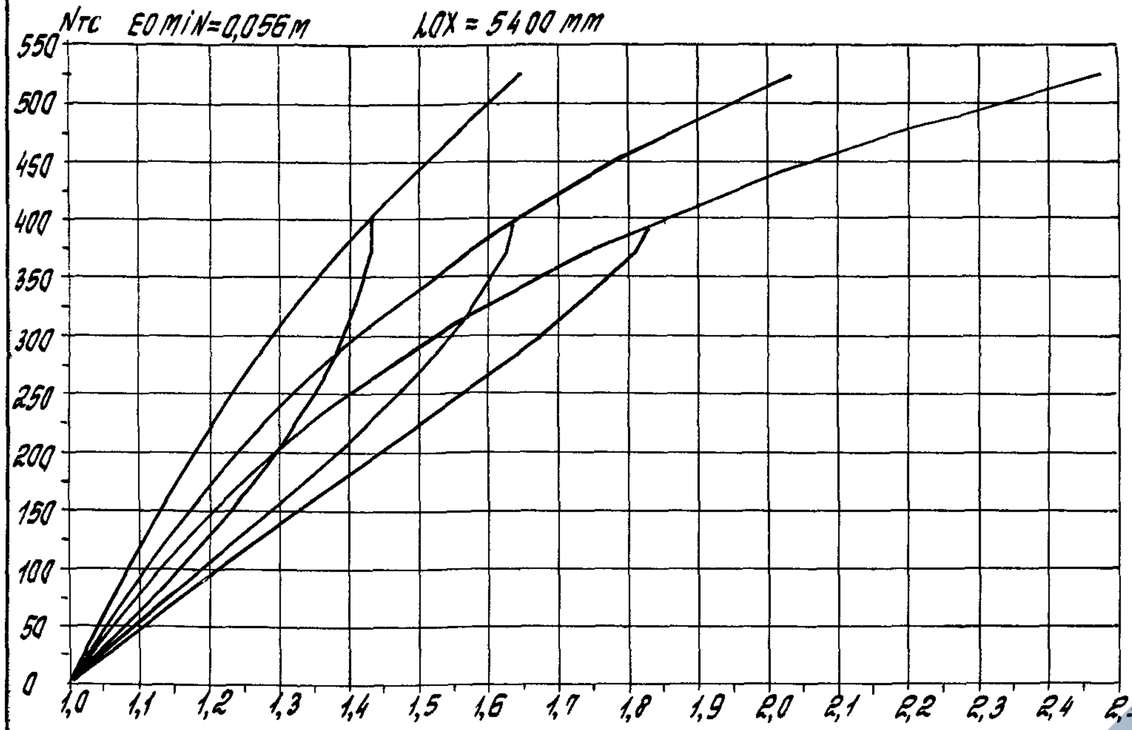
1.020.1-4 0-9 002

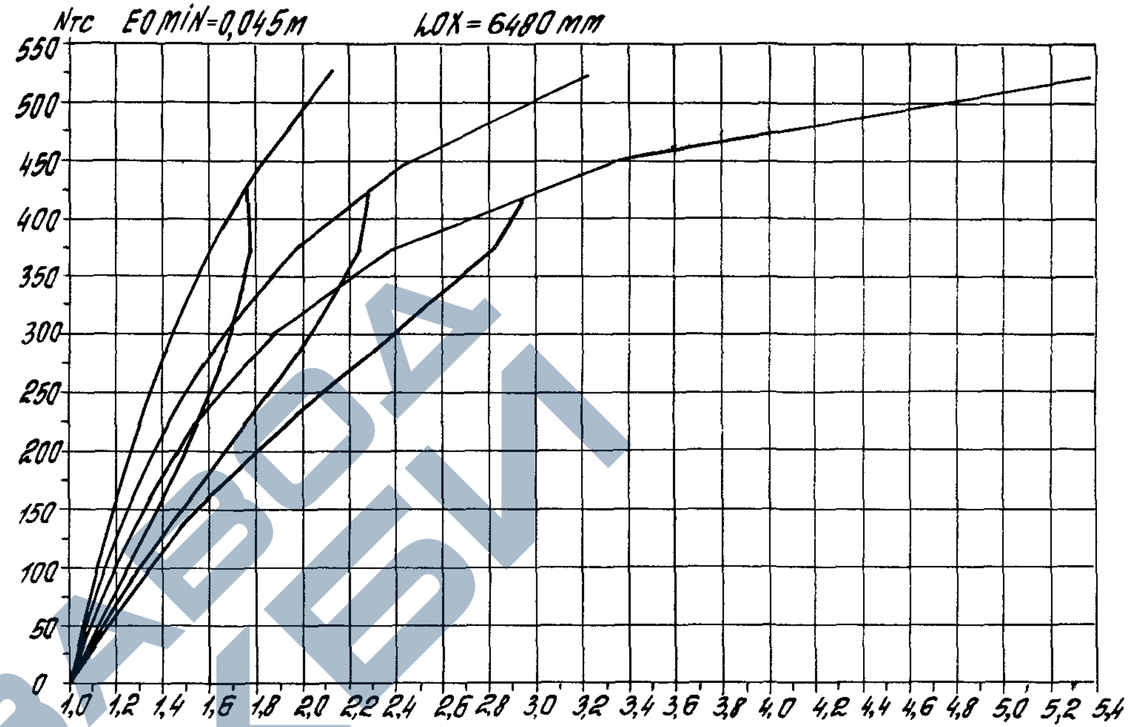
Лист 255

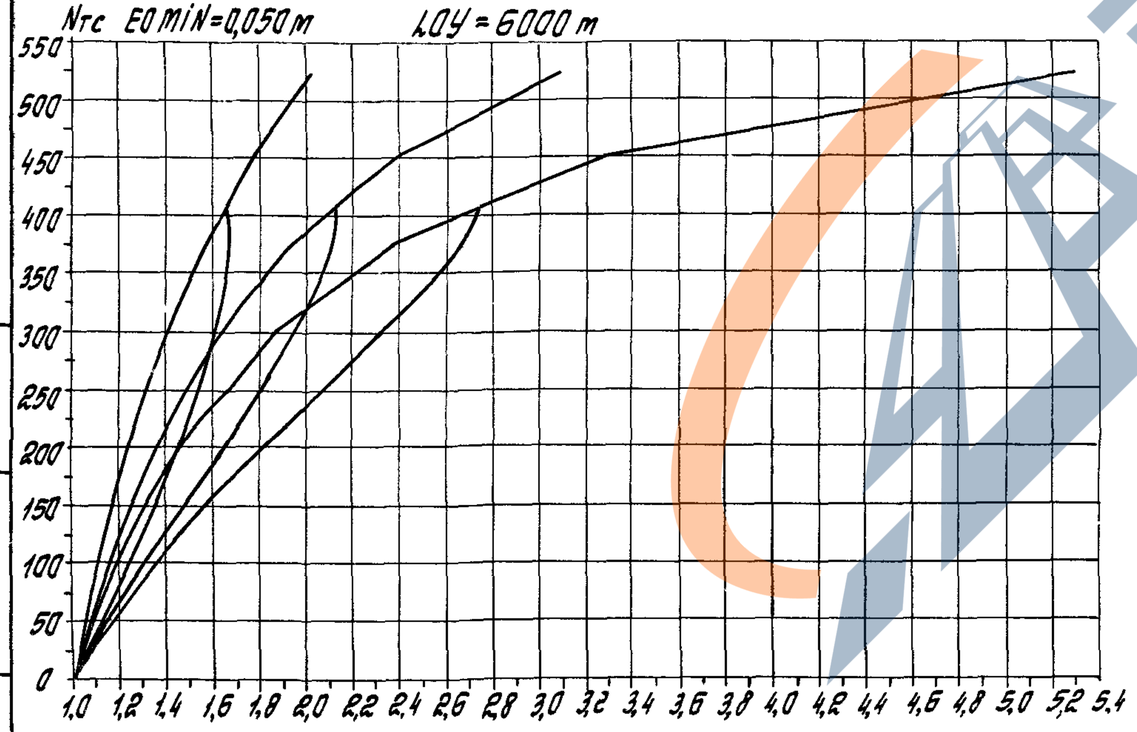
24166-03 32

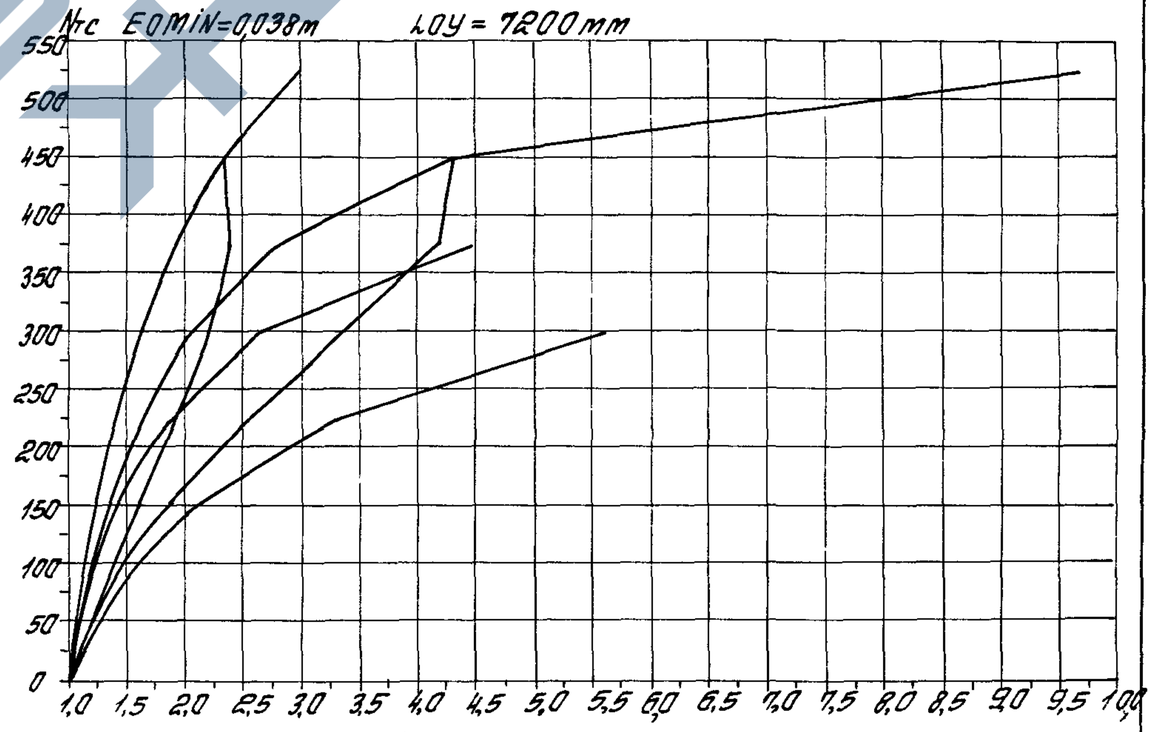
https://zavodjbi.com/

https://zavodjbi.com/









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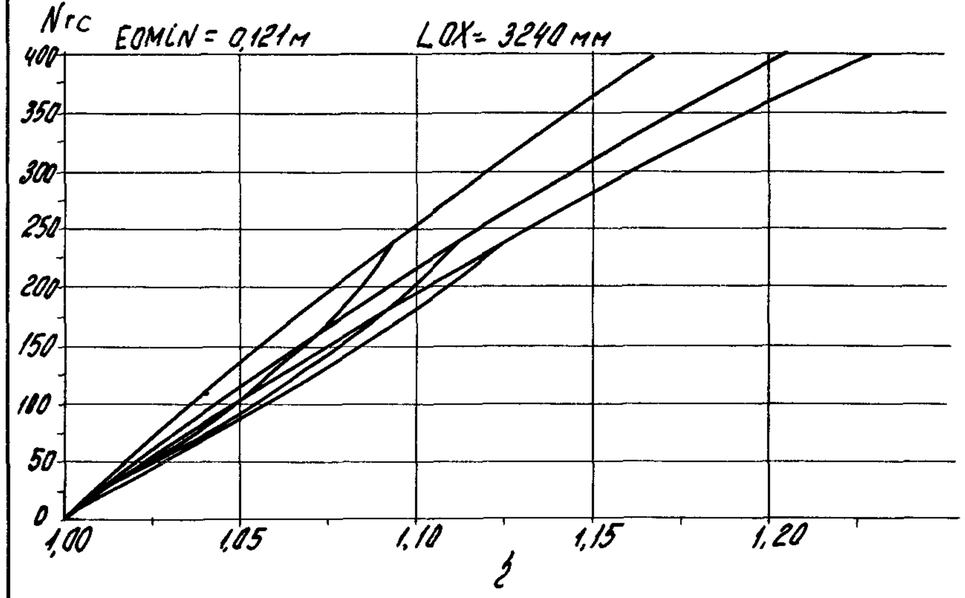
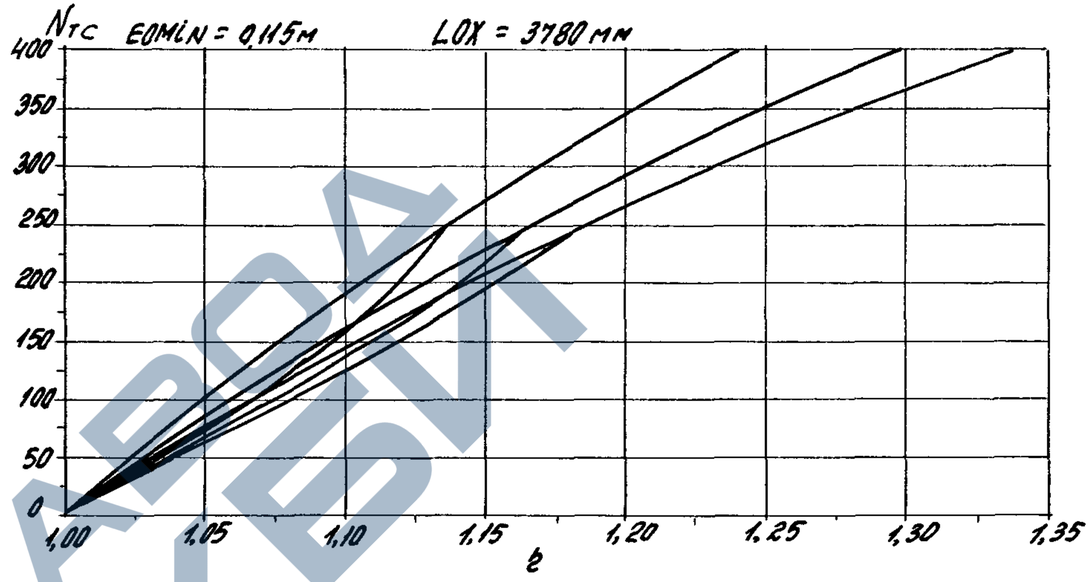
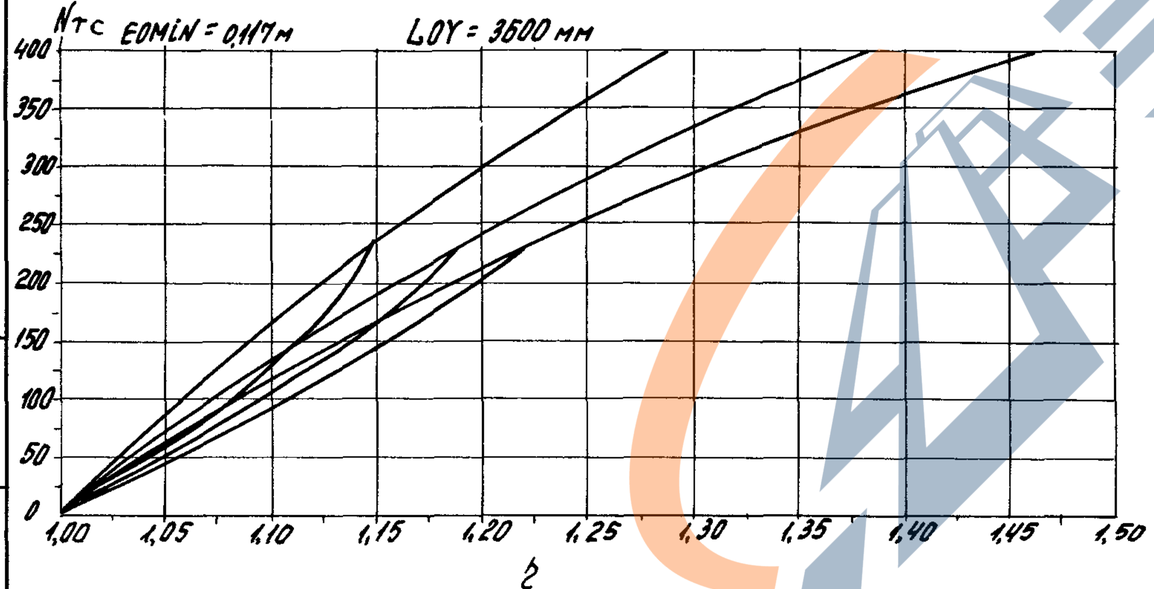
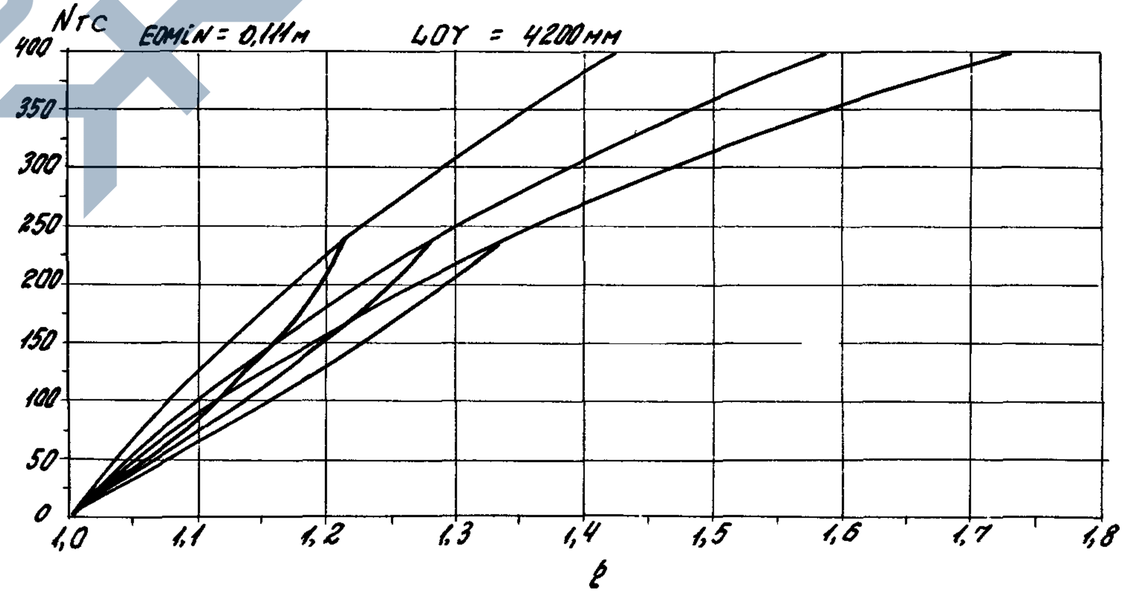
https://zavodjbi.com/









Инв.№ подл. | Подпись и дата | Взам.инв.№

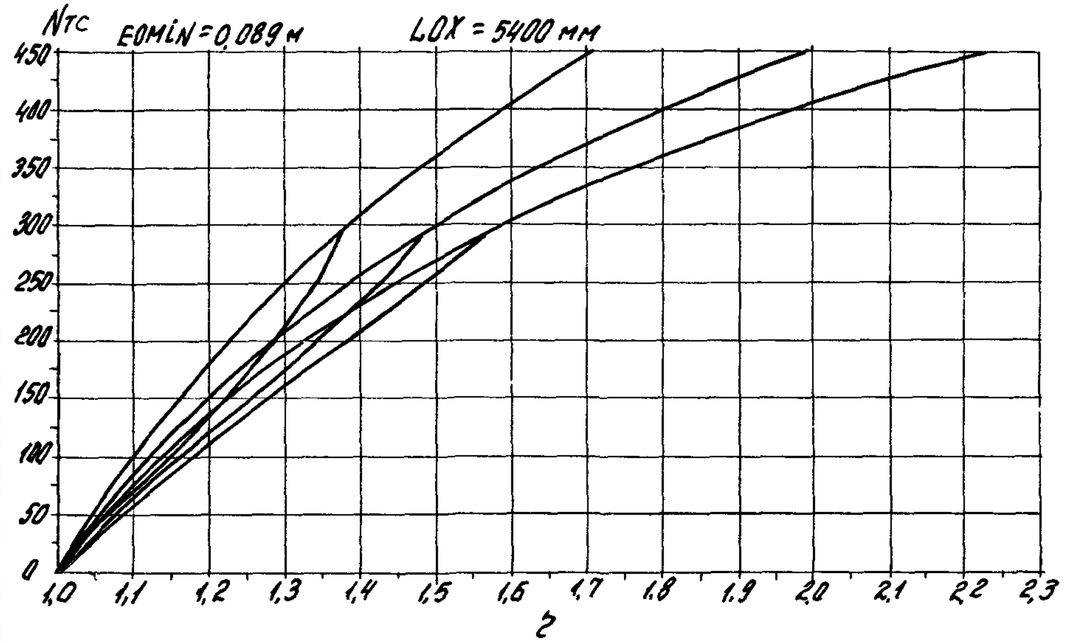
1.020.1-4 0-9

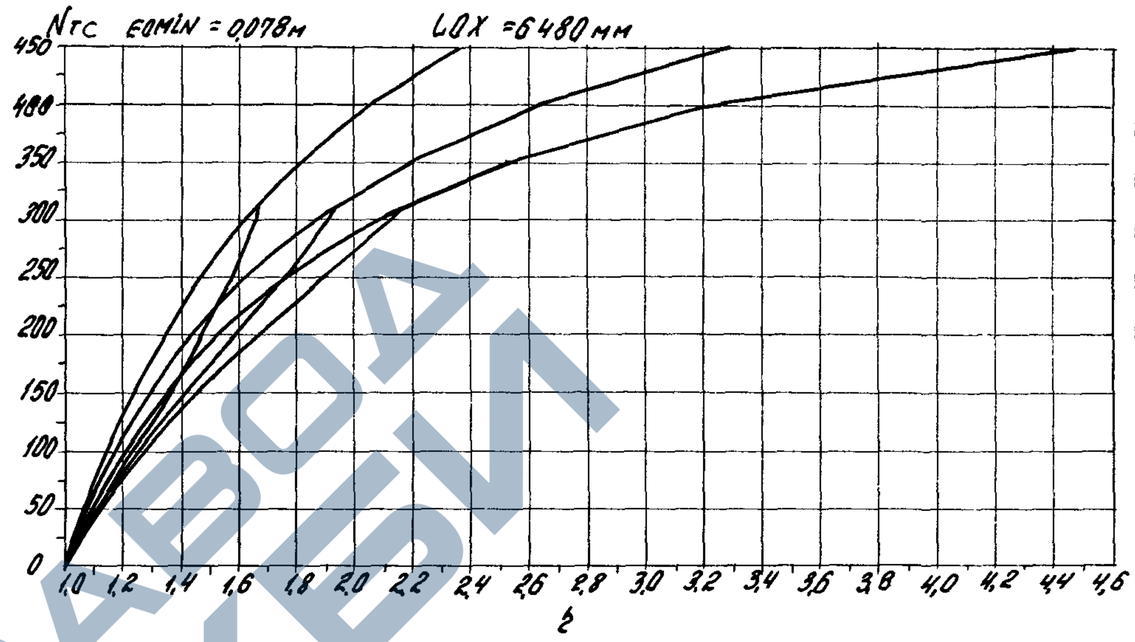
ЛИСТ 257

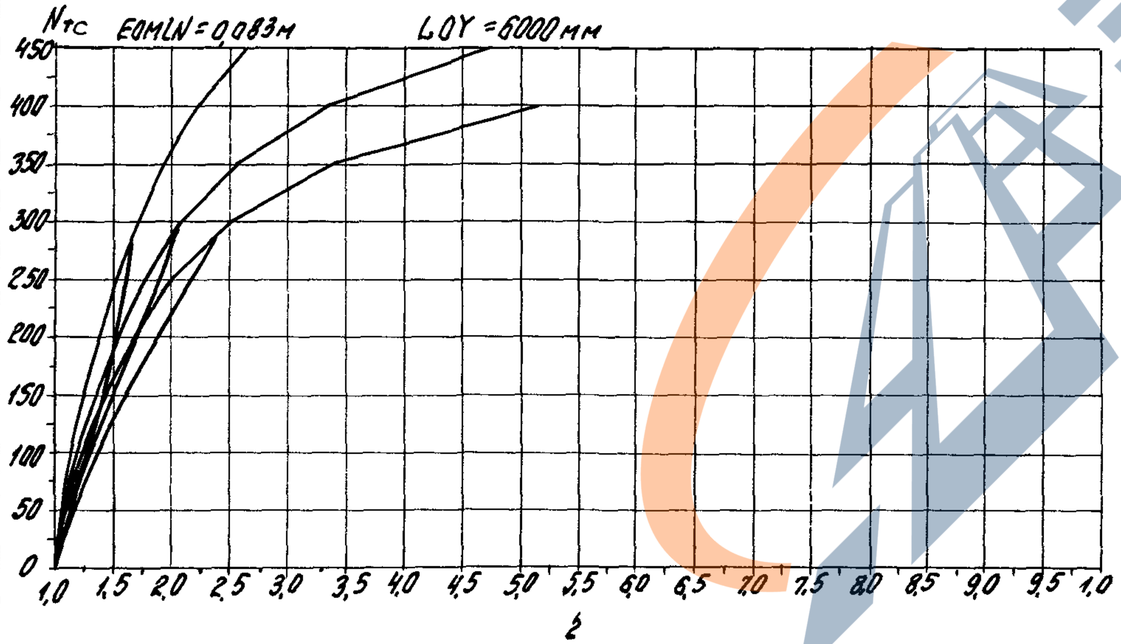
24166-03 34

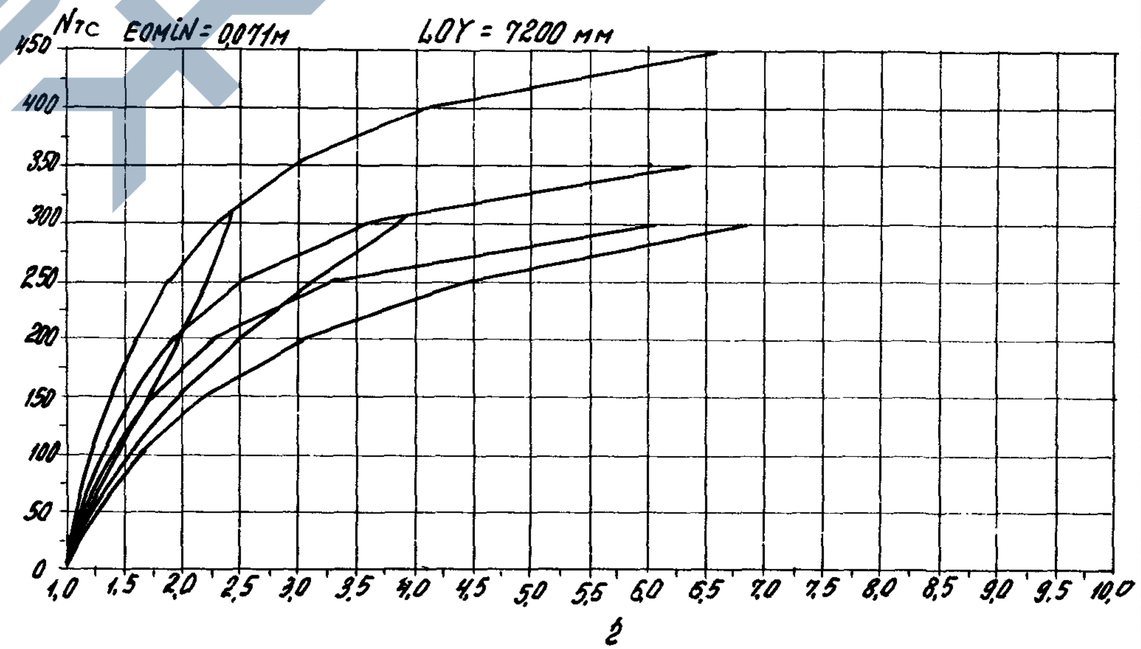
https://zavodjbi.com/

https://zavodjbi.com/









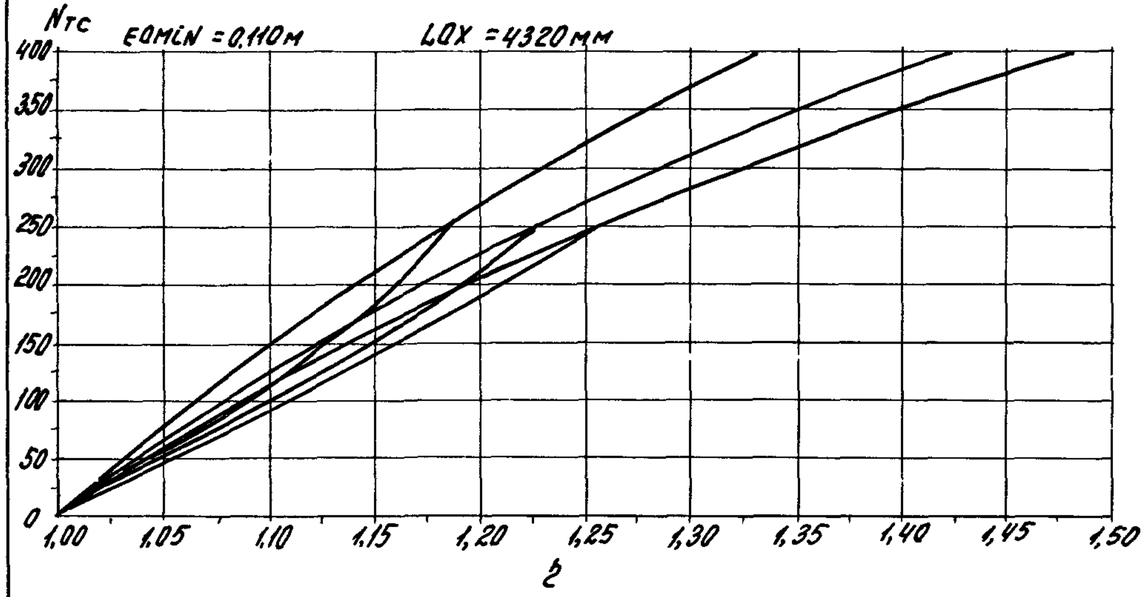
Инв.№ подл. | Подпись и дата | Взам. инв.№

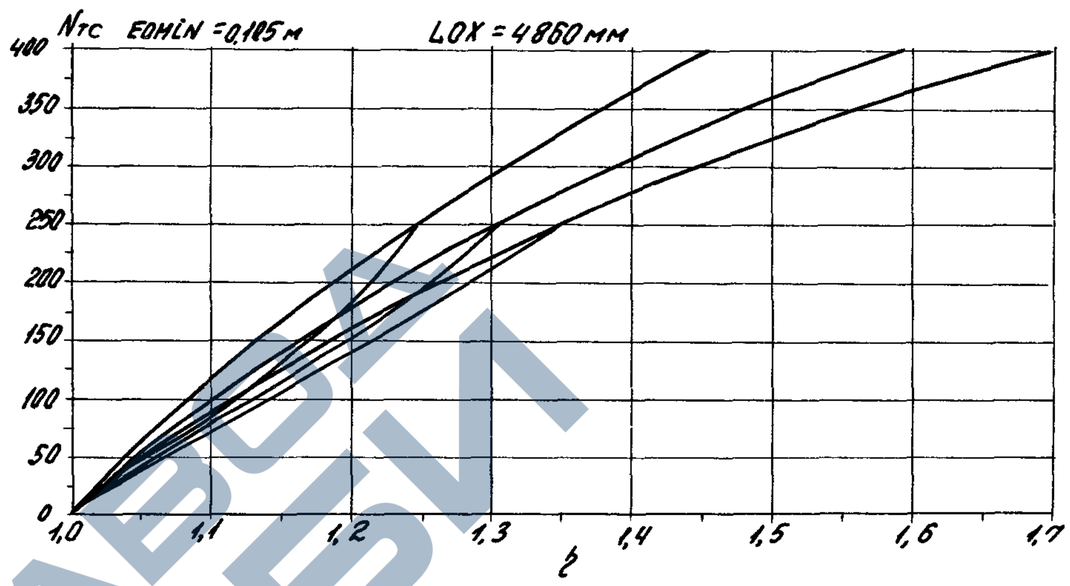
1.020.1-4 0-9

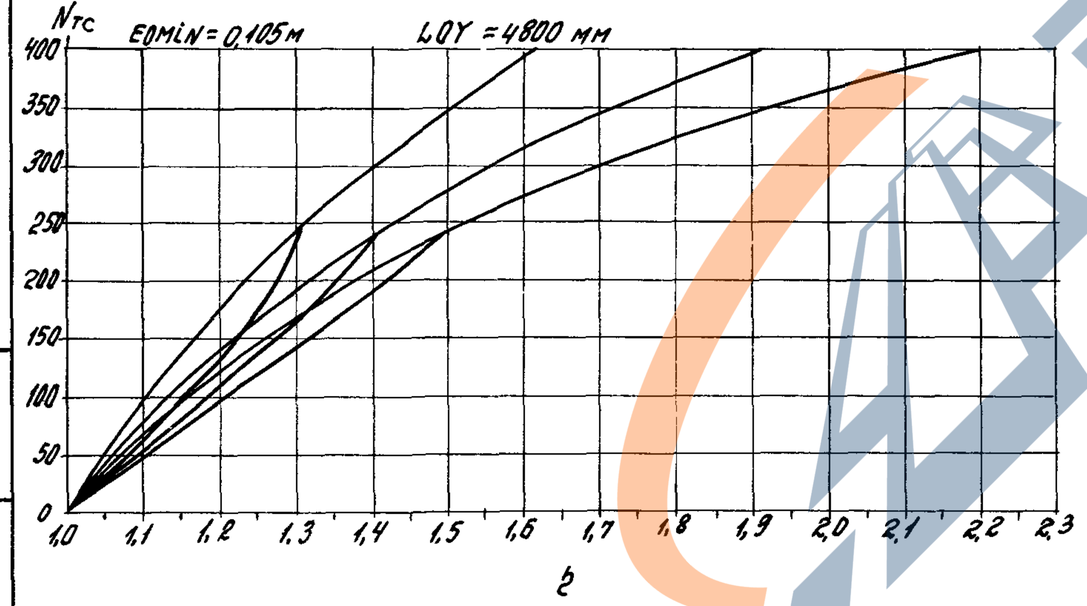
Лист 258

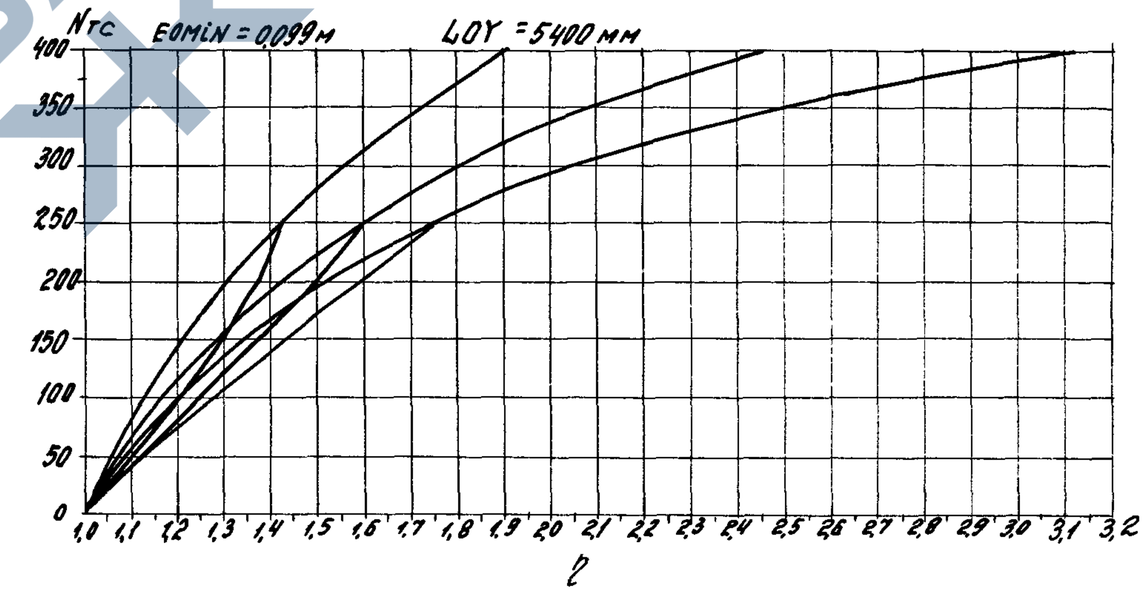
24166-09 35

https://zavodjbi.com/









Инв. № подл. | Подпись и дата | Взам. инв. №

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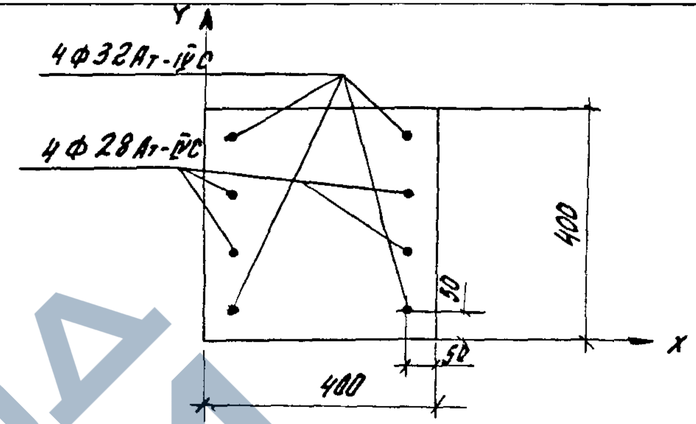
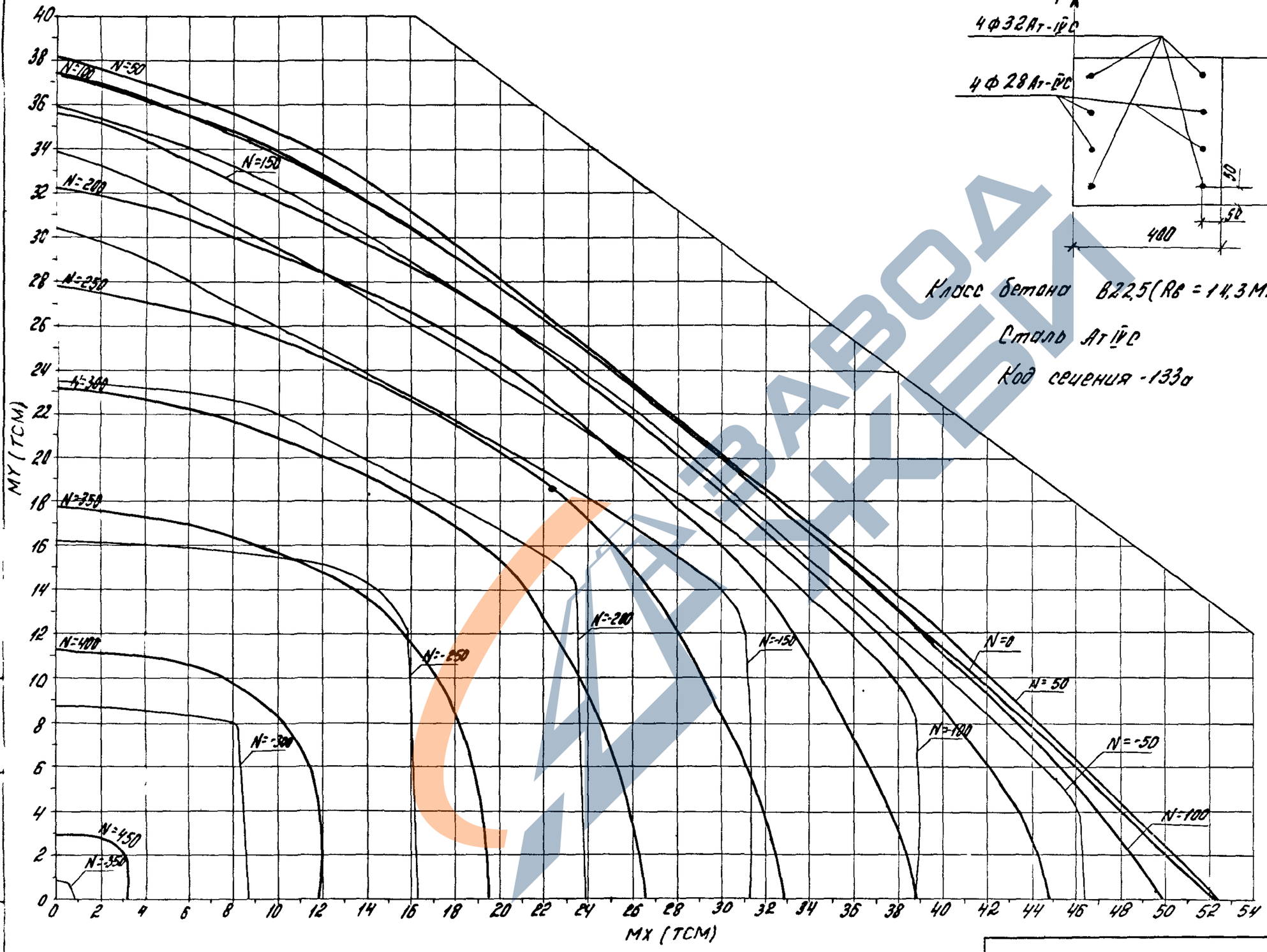


Класс бетона В22,5 (Rв = 14,3 МПа при учете γ_{b2} = 1,10)

Сталь Ат IVС

Код сечения - 133а



Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4. 0-9 – 002

260

24166-03 37

https://zavodjbi.com/

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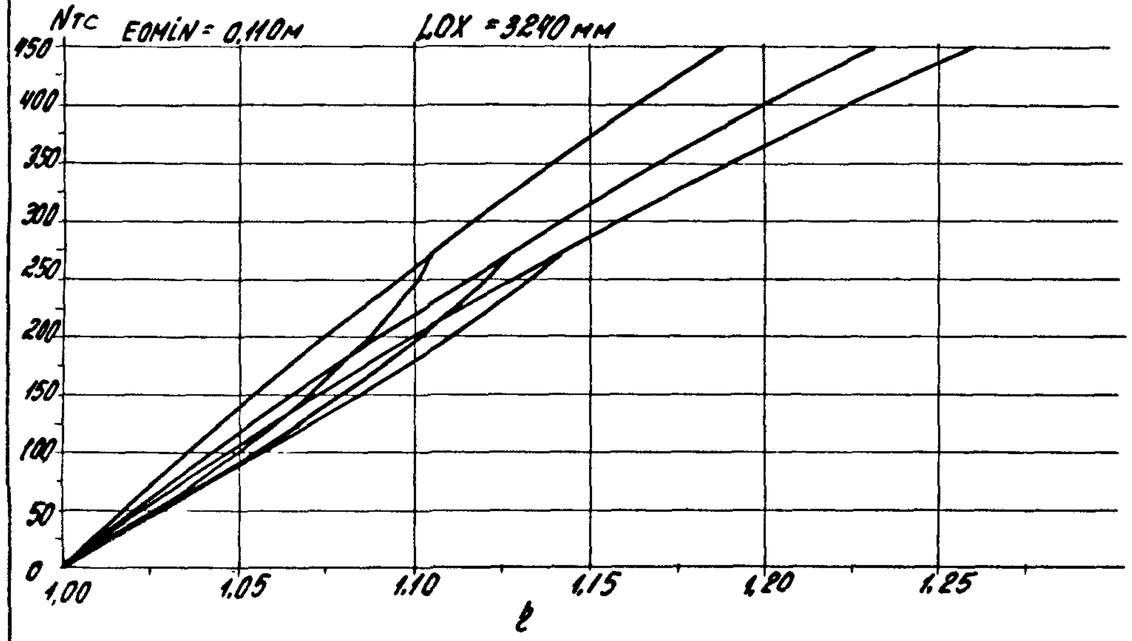

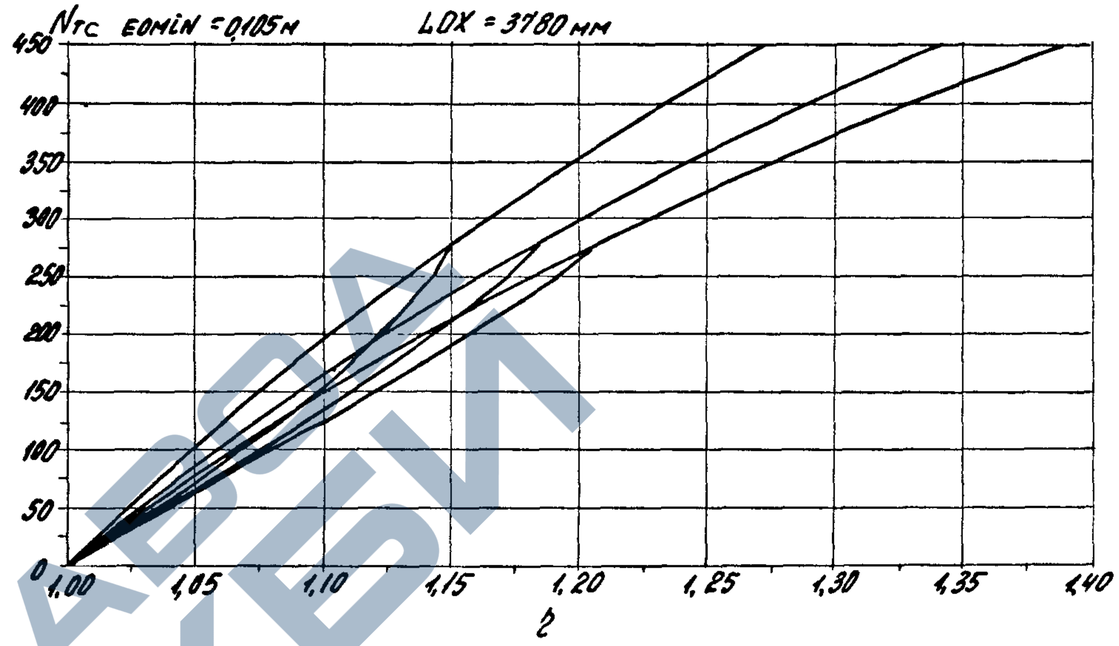

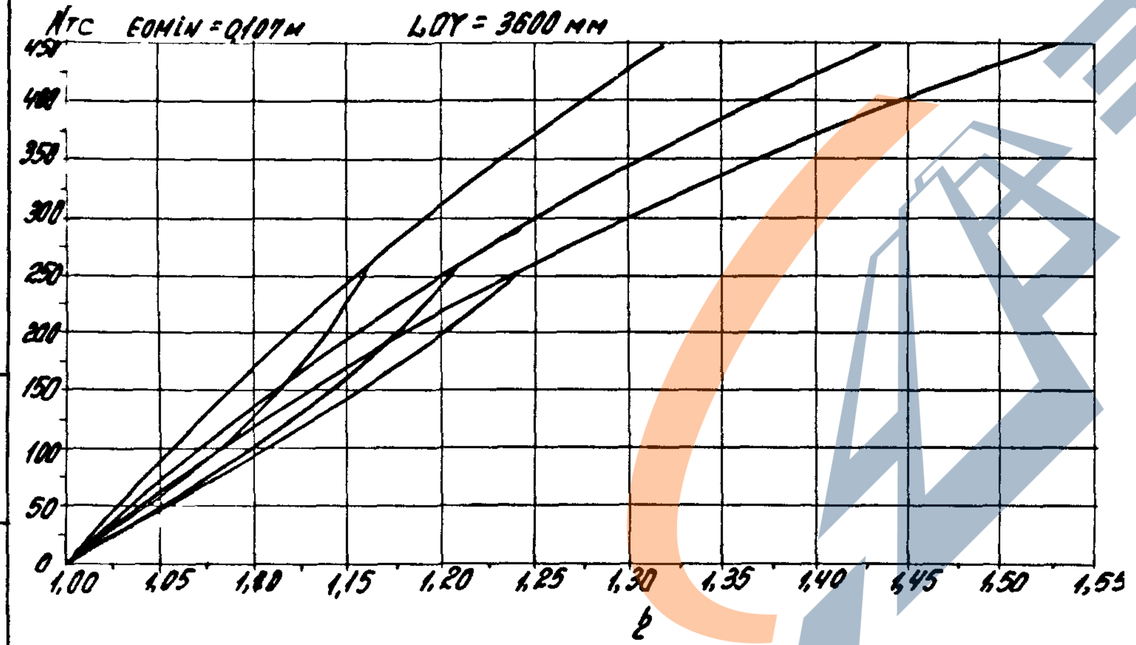

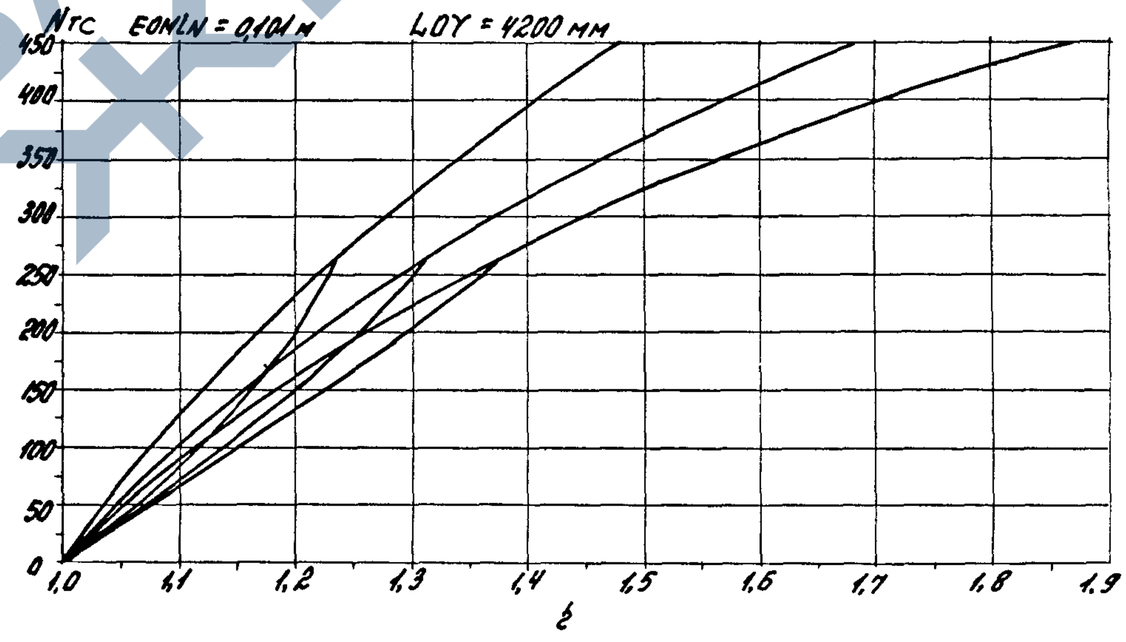

Инв.№ подл. | Подпись и дата | Взам. инв.№

1.020.1-4. 0-9 - 002

Лист 261

24166-03 38

https://zavodjbi.com/

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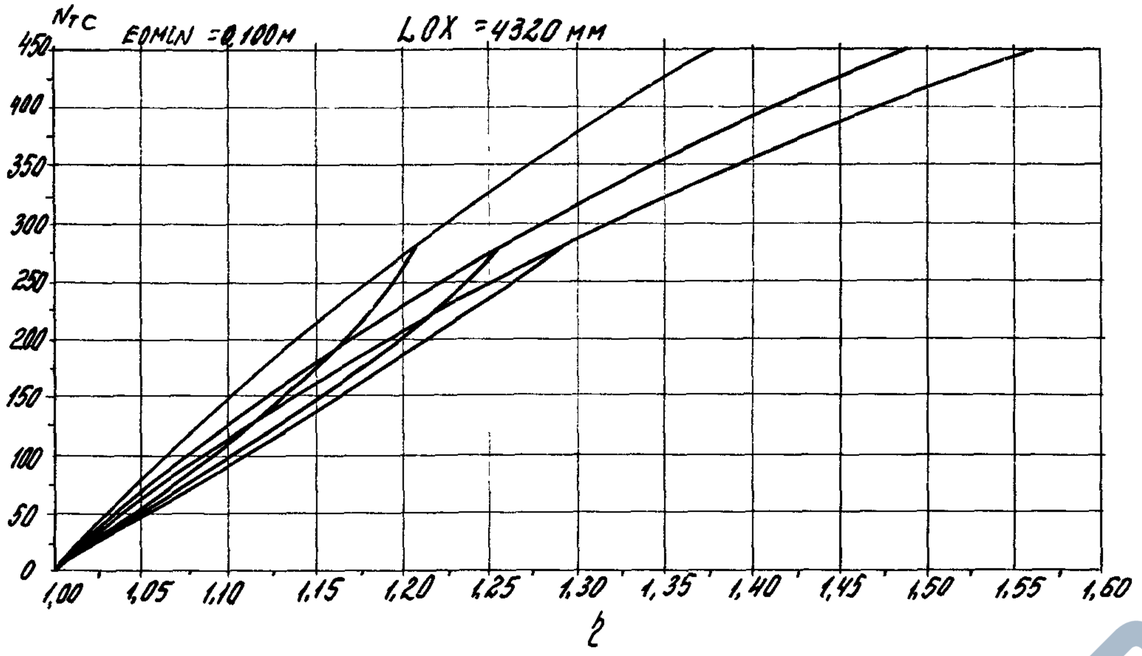

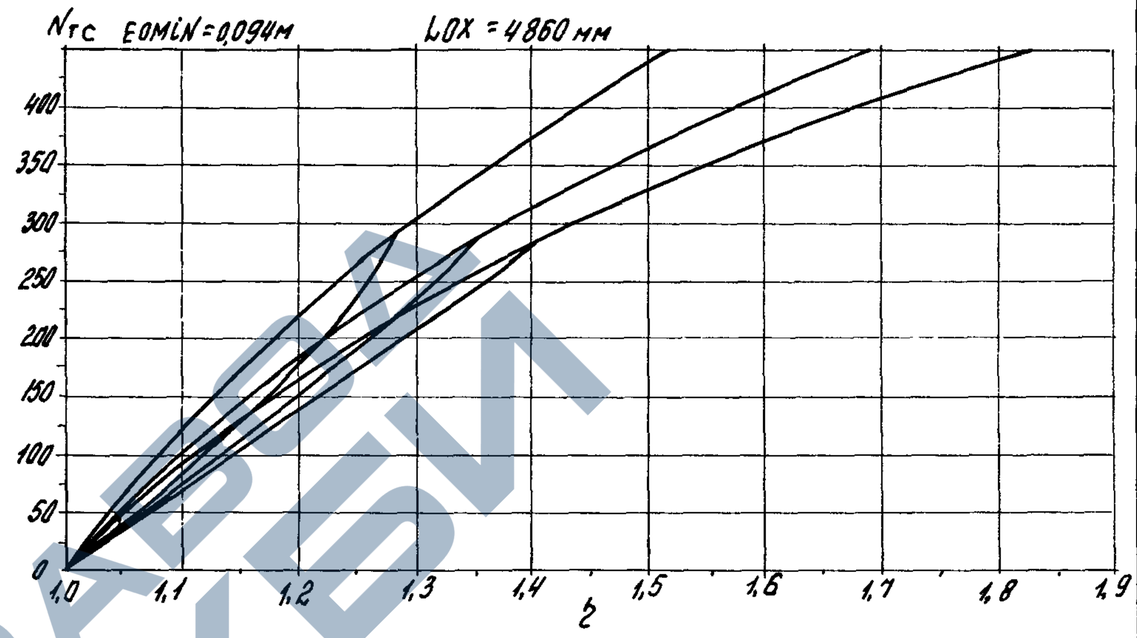

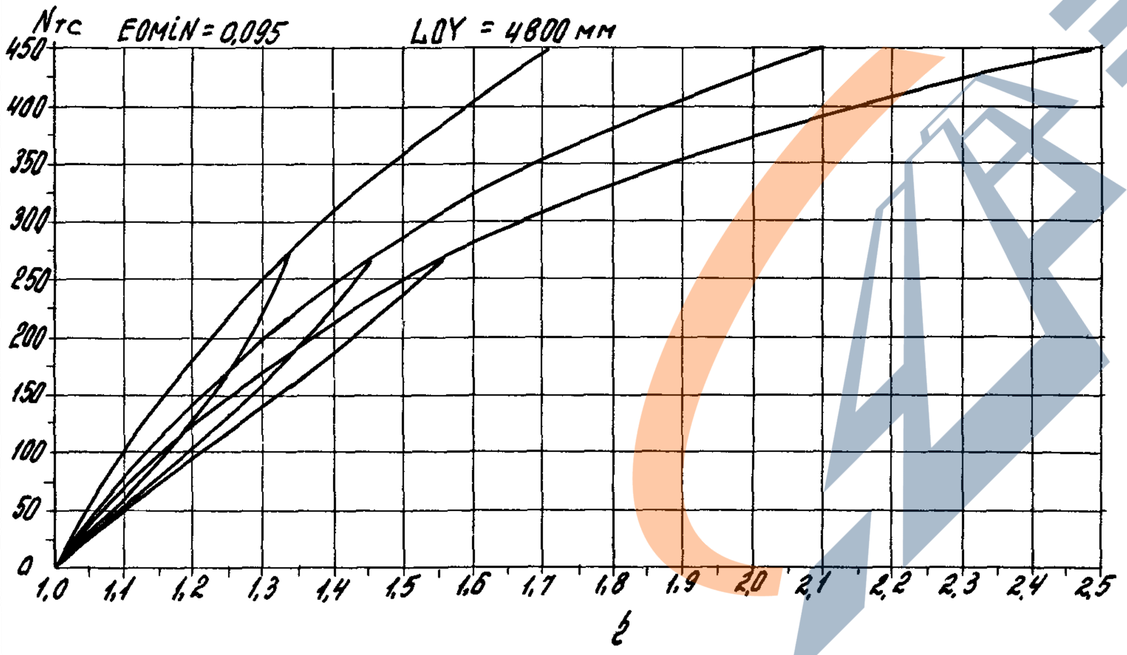

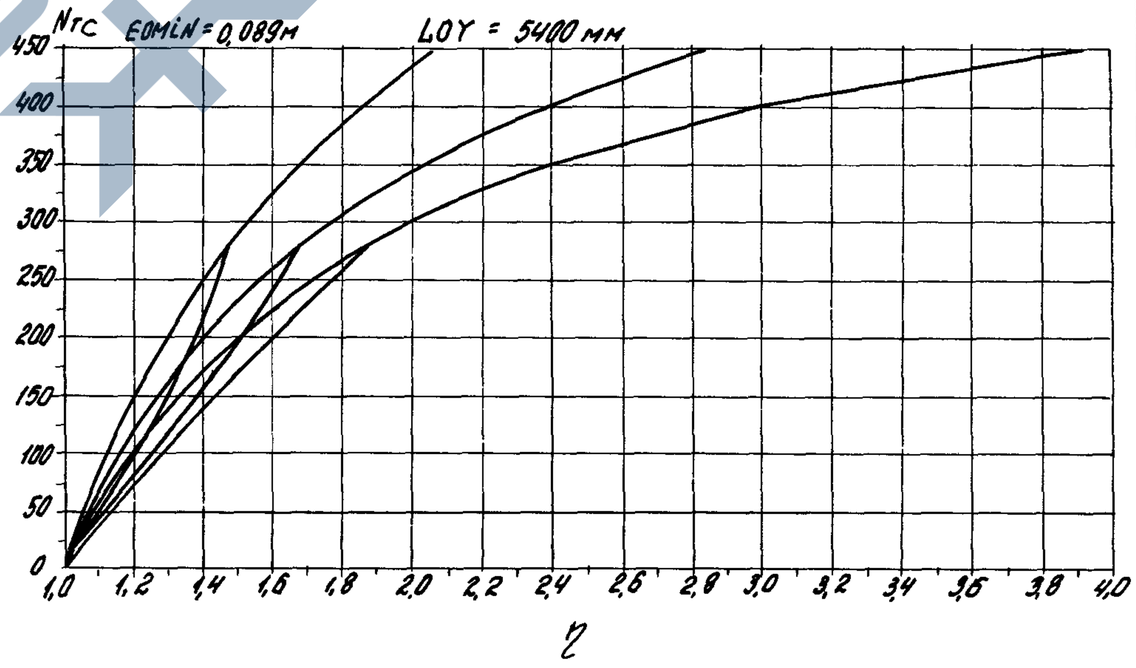

1.020.1-4 0-9	Лист 262

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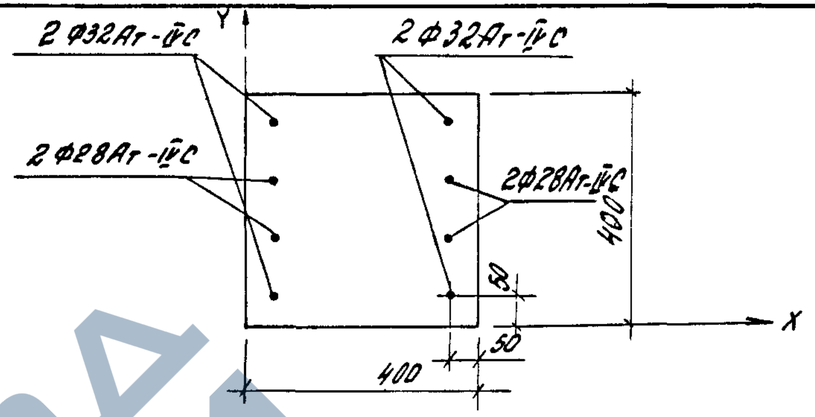
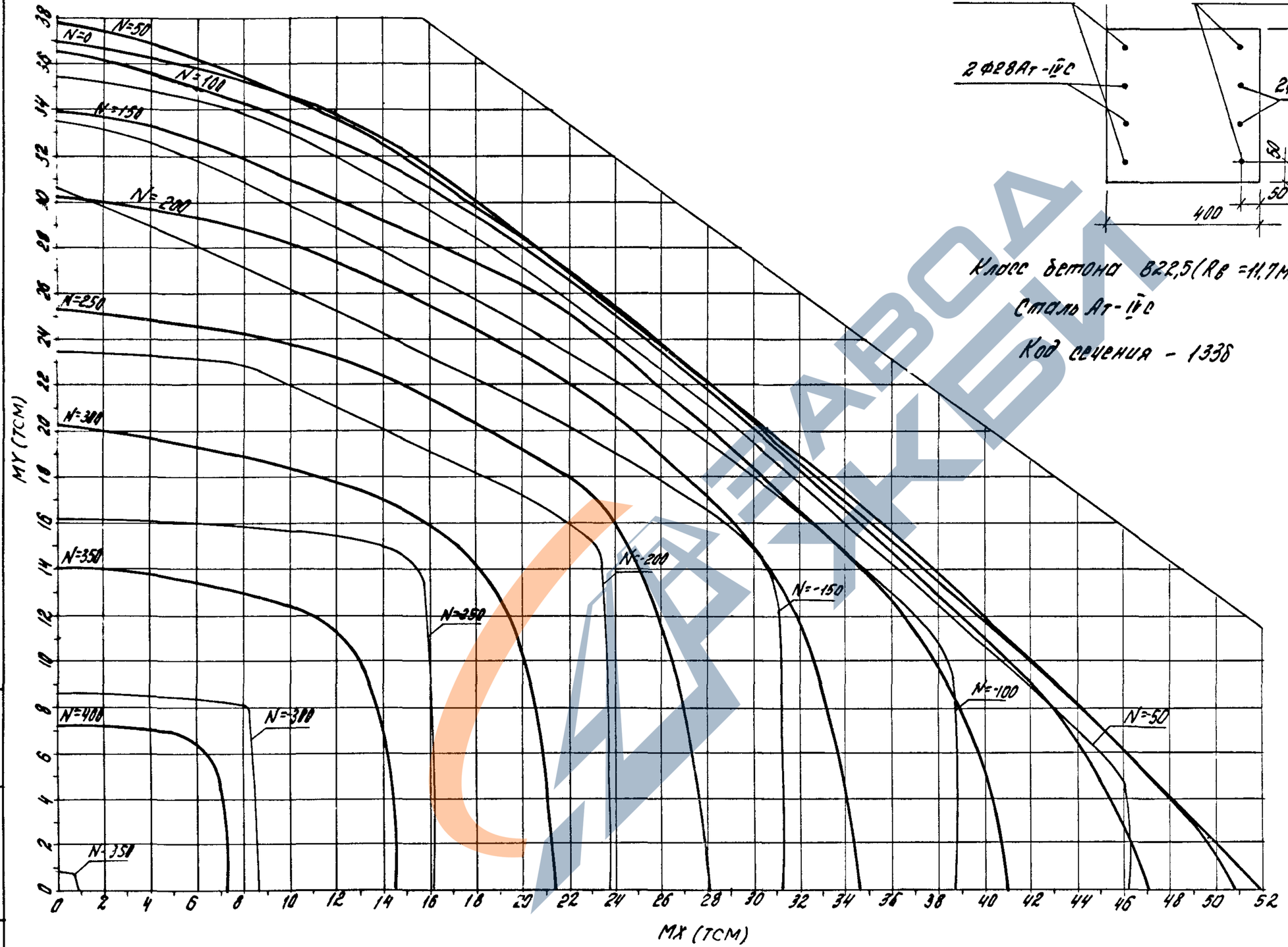


Класс бетона В22,5 ($R_в$ =11,7МПа при учете $\gamma_{в2}$ = 0,90)

Сталь Ат-IVс

Код сечения - 1338



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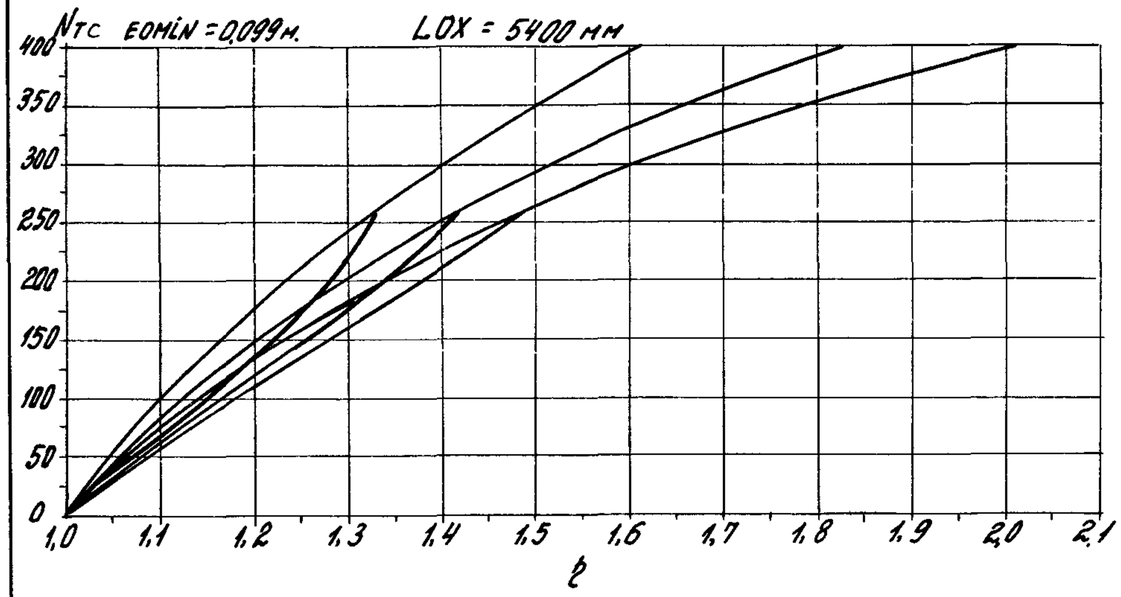

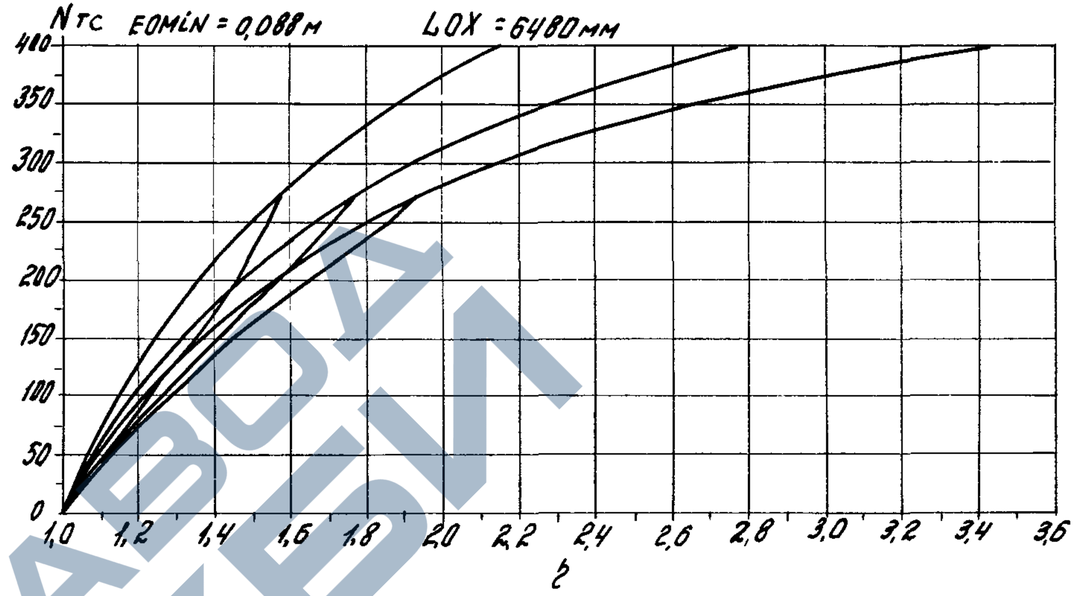

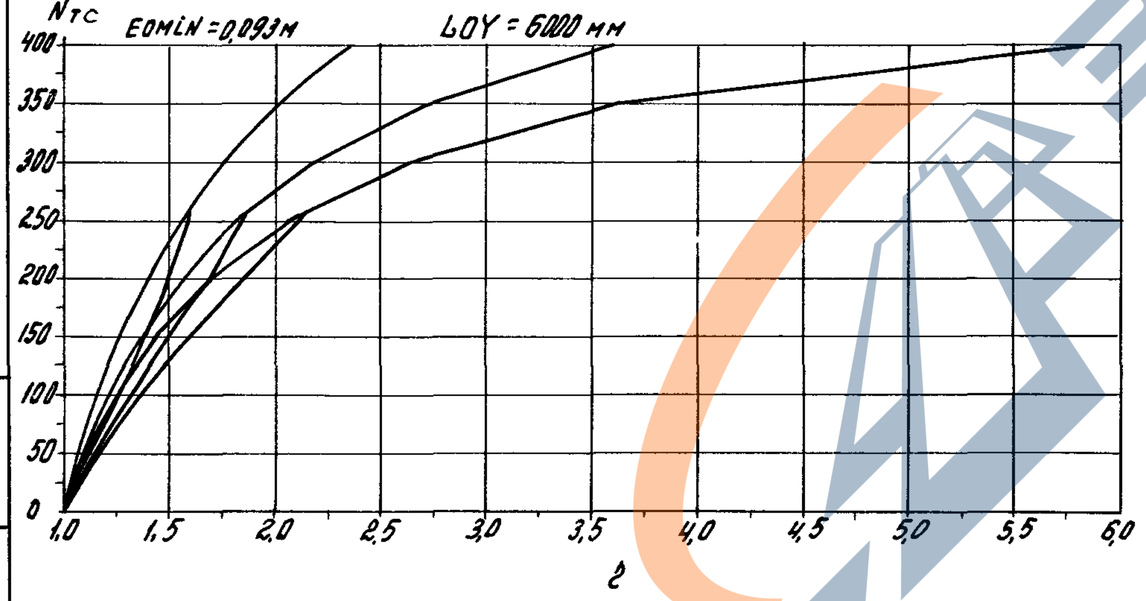

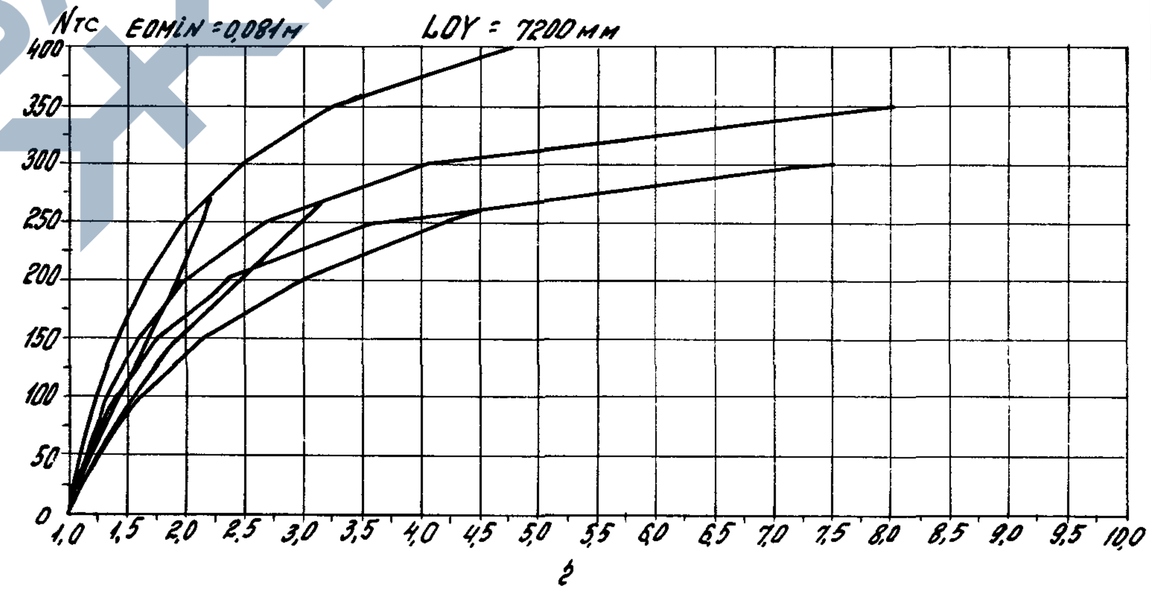

Инв. № подл. | Подпись и дата | Взам. инв. №

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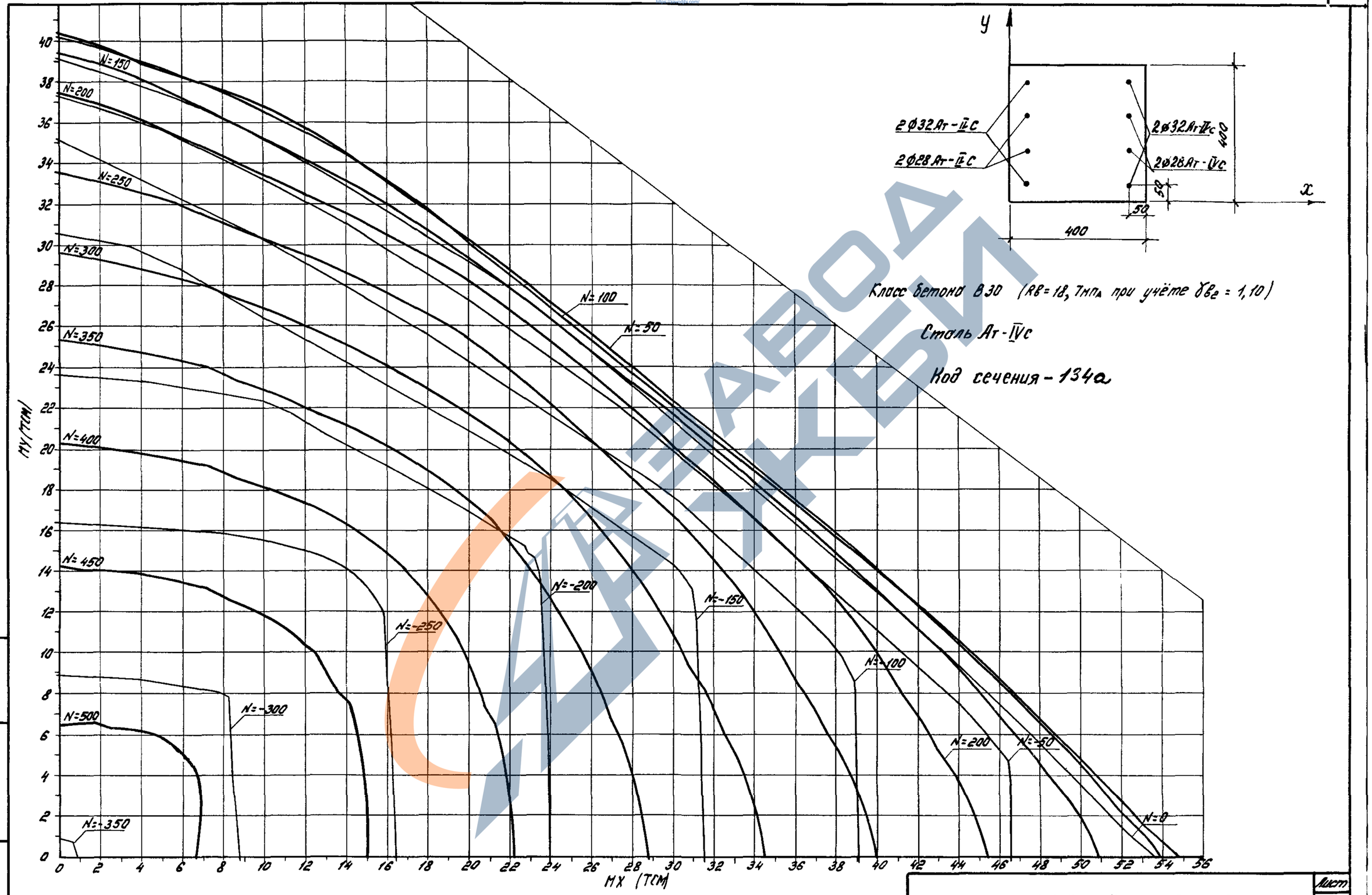

Класс бетона В30 (R_B = 18,7 тнп при учёте γ_{B_2} = 1,10)

Сталь Ат-IVс

Код сечения – 134а

Инв.№ подл. | Подпись и дата | Взам. инв.№

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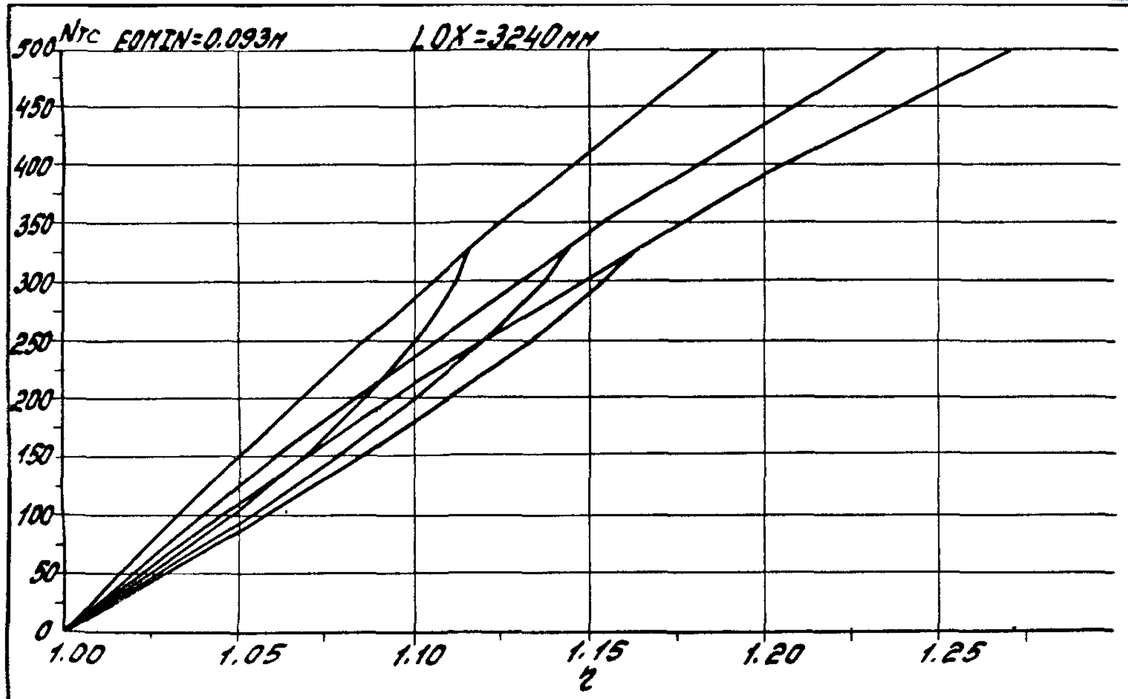

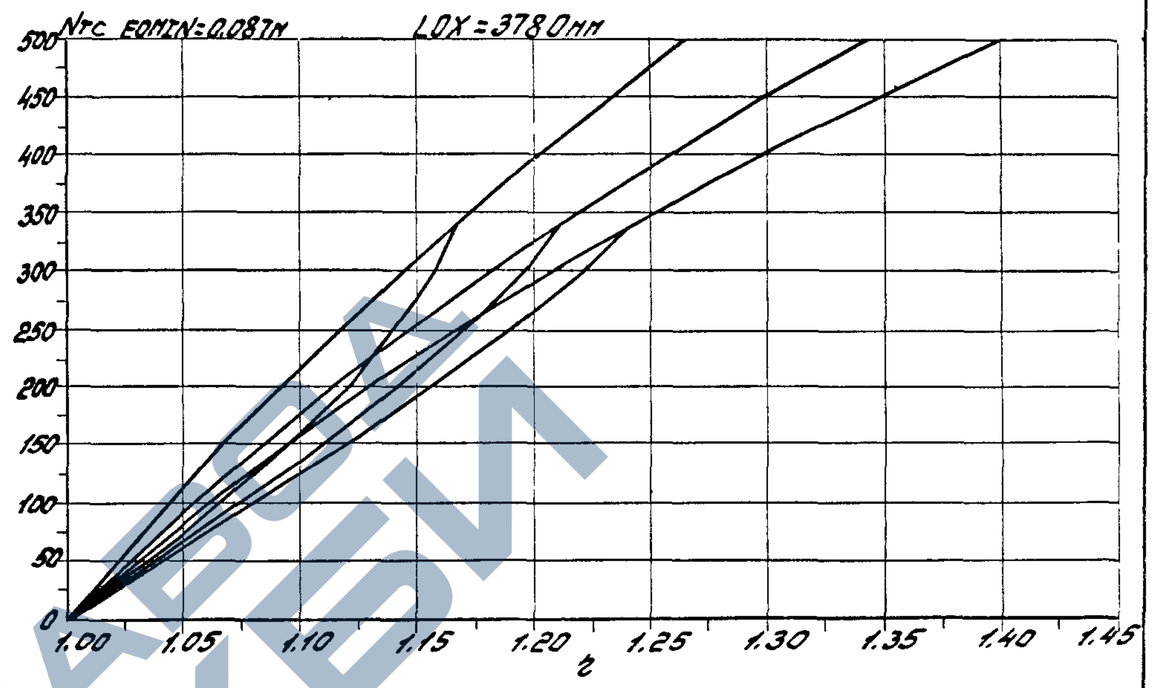

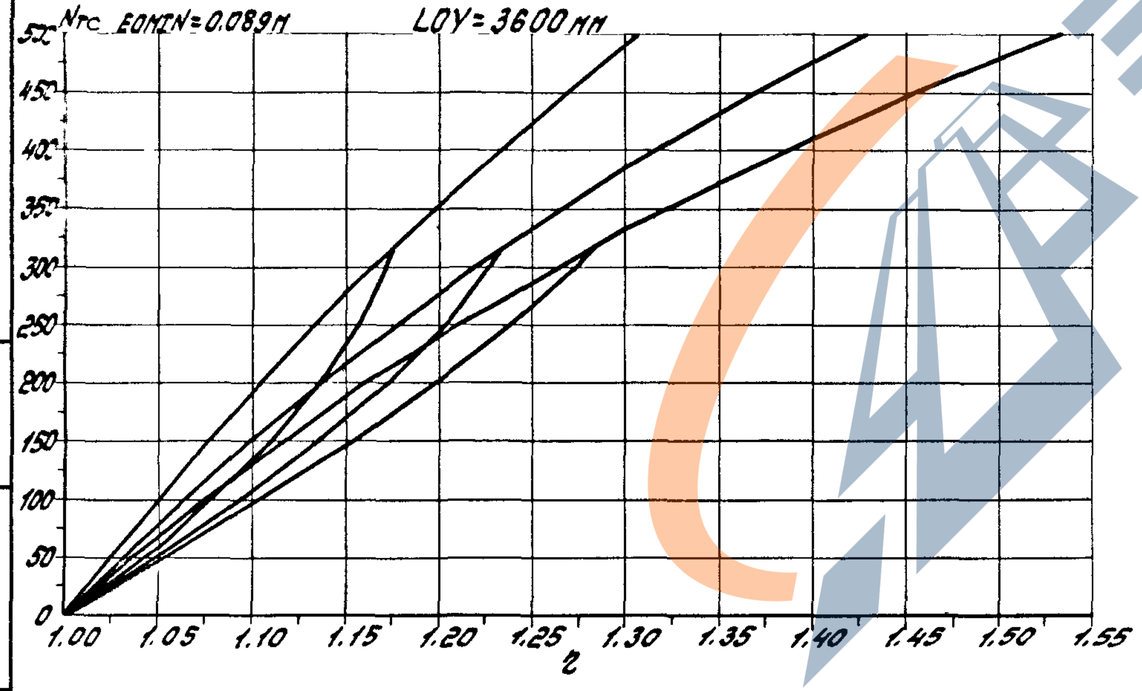

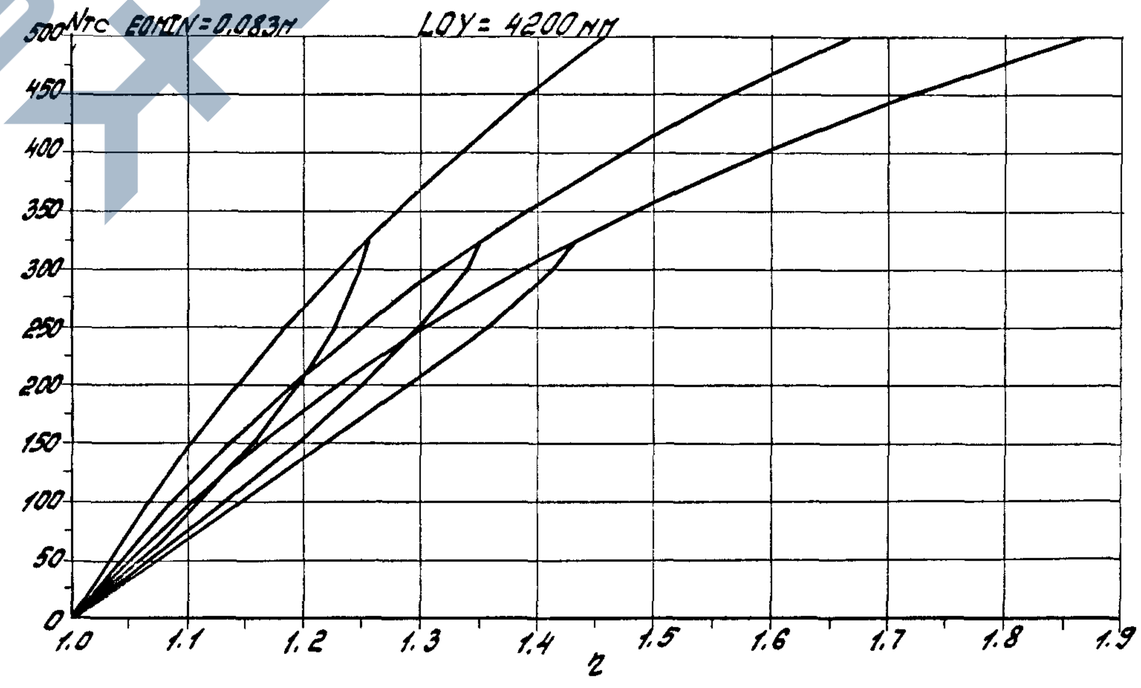

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4. 0-9-002

Лист 266

24166-03 43

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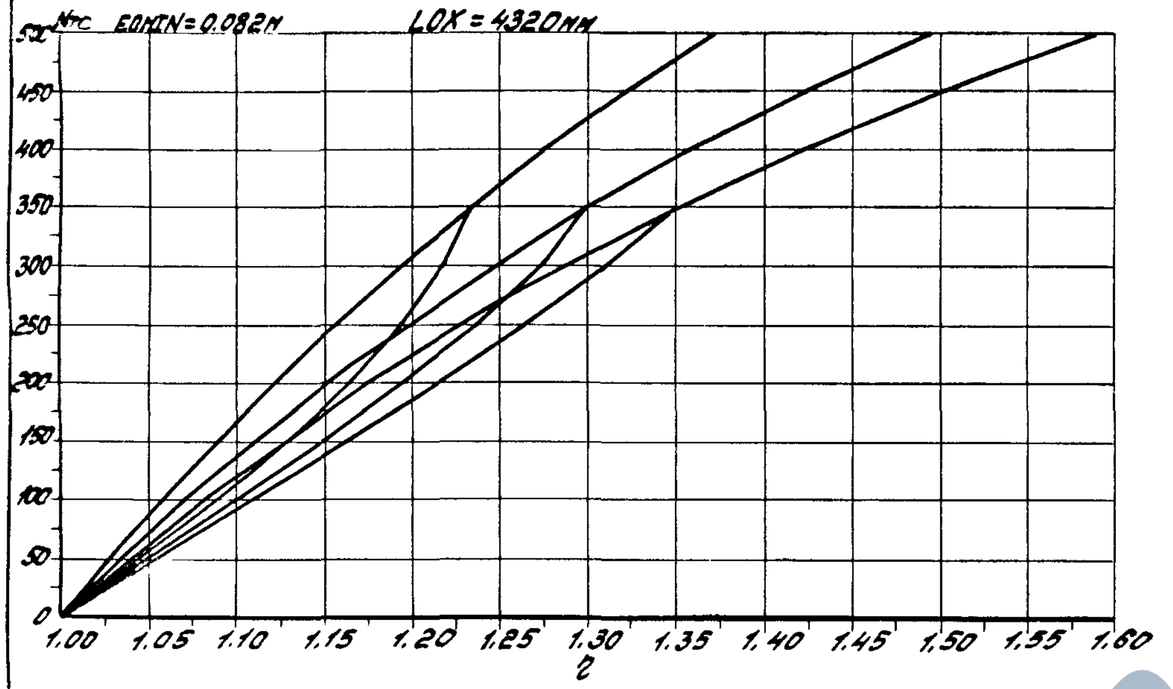

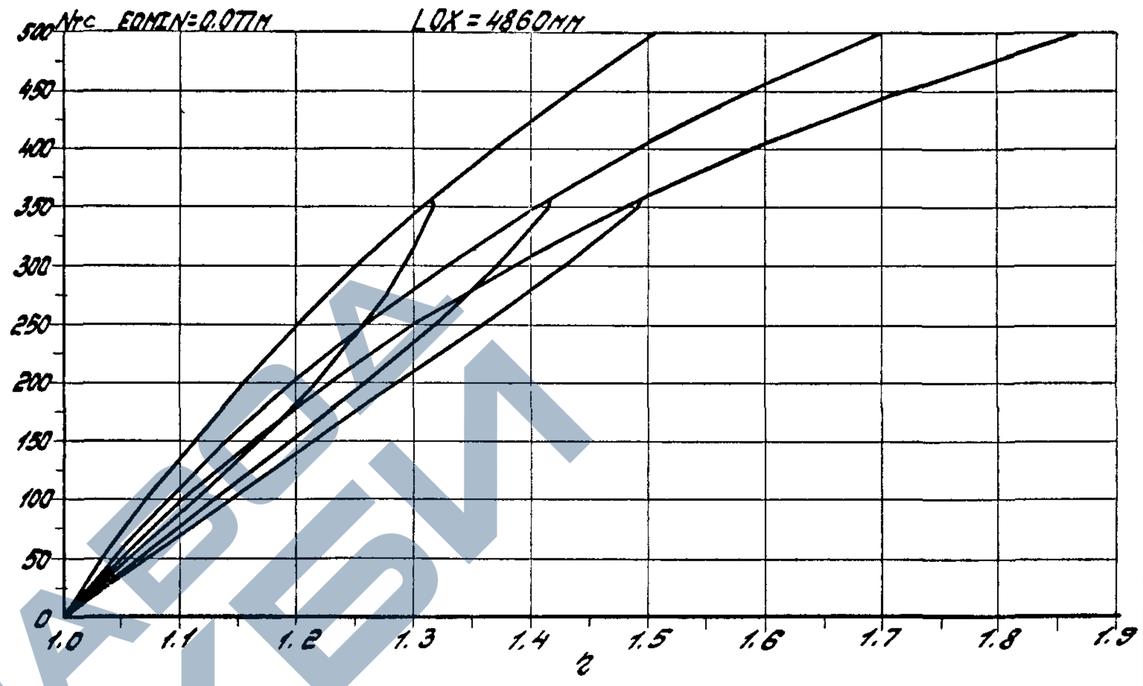

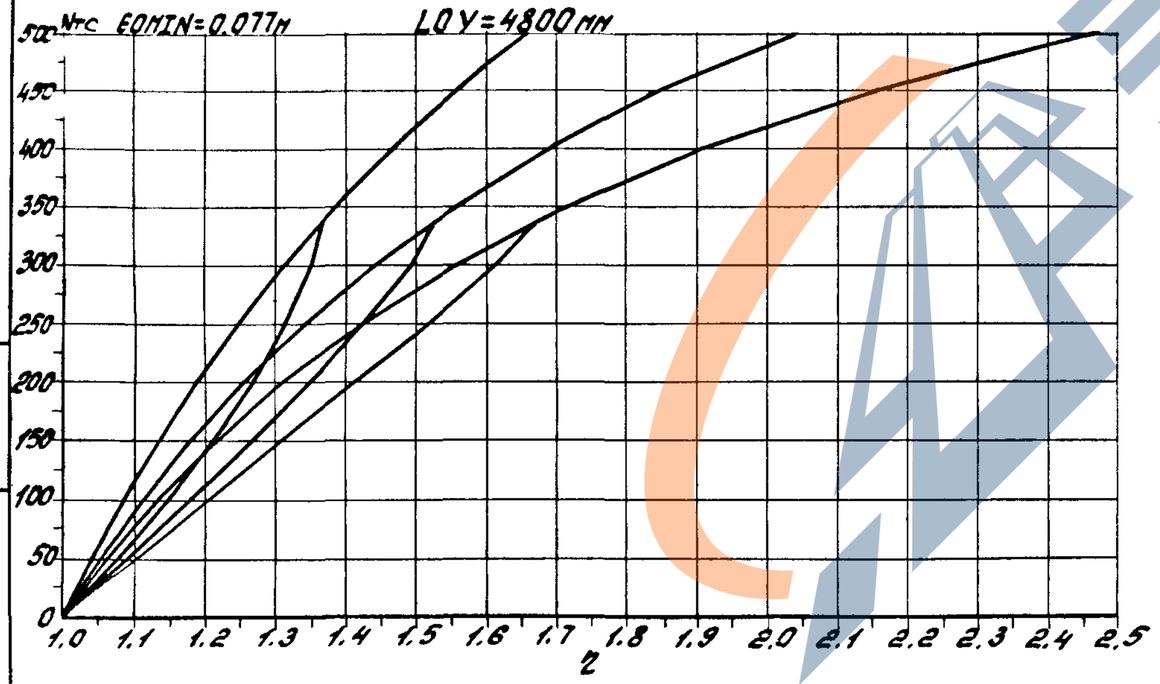

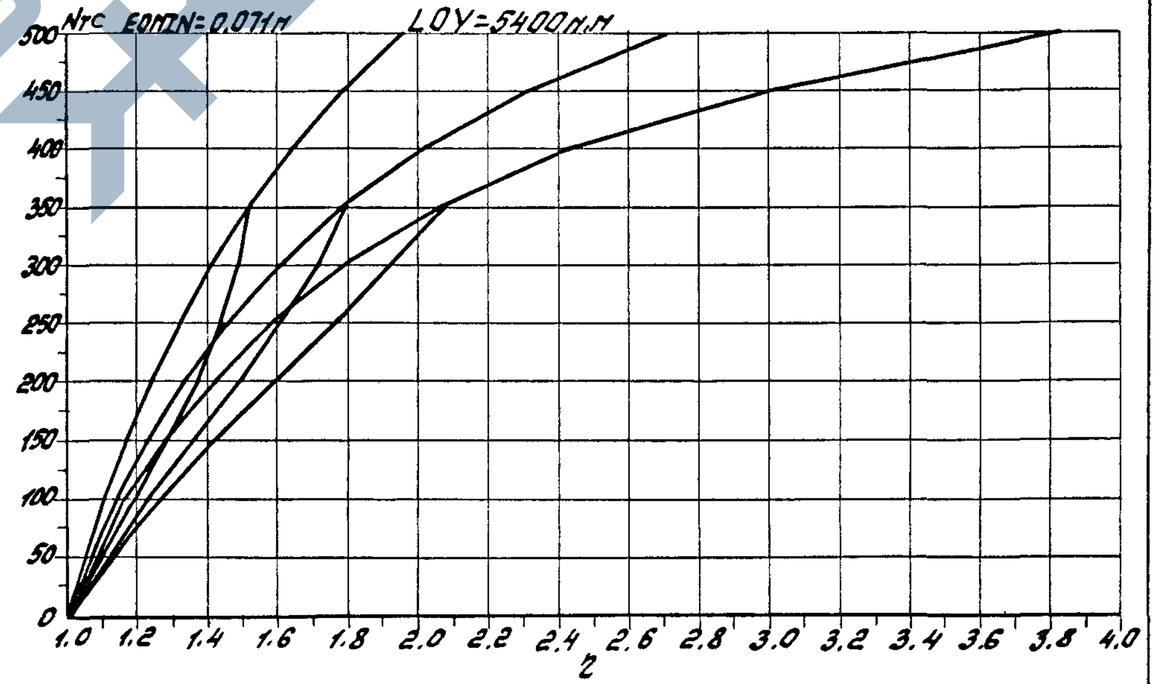

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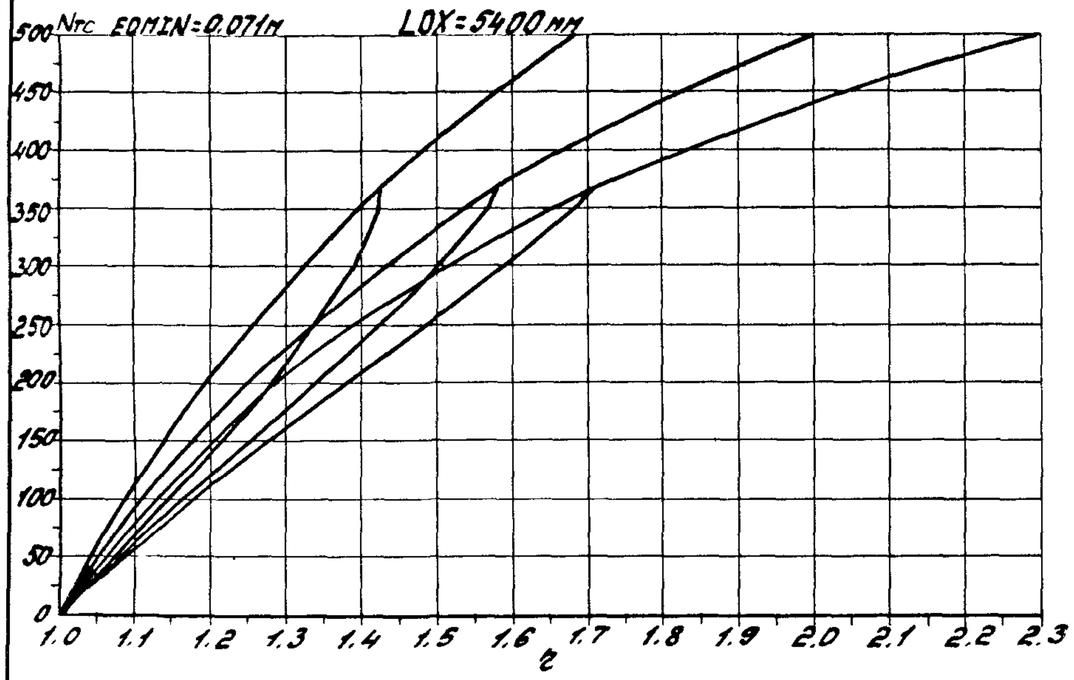
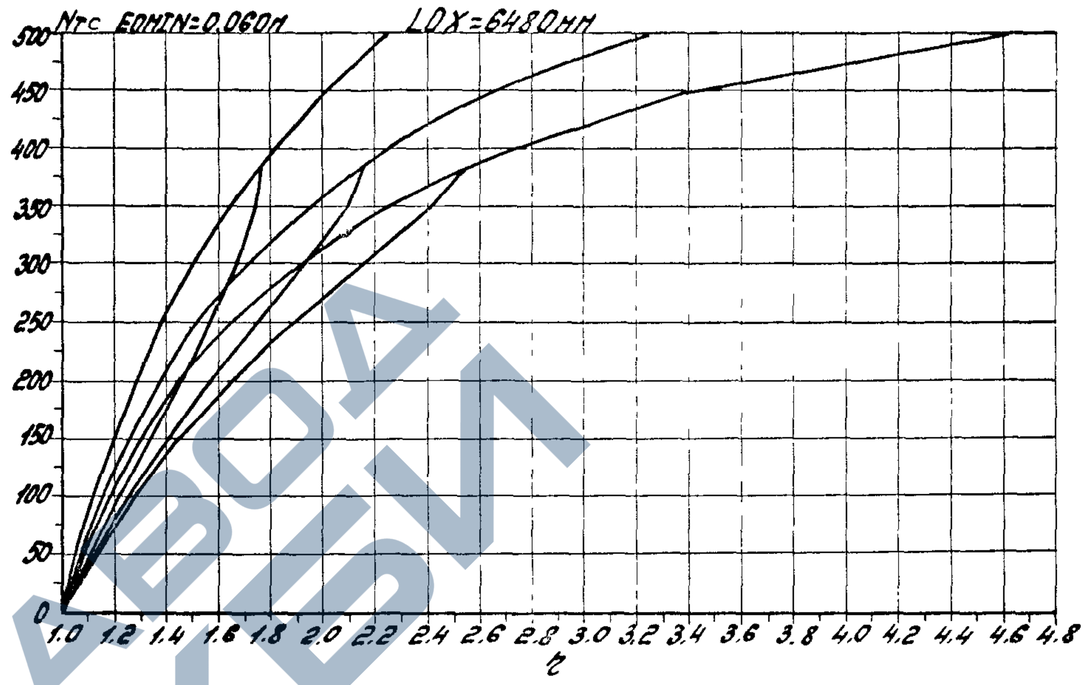
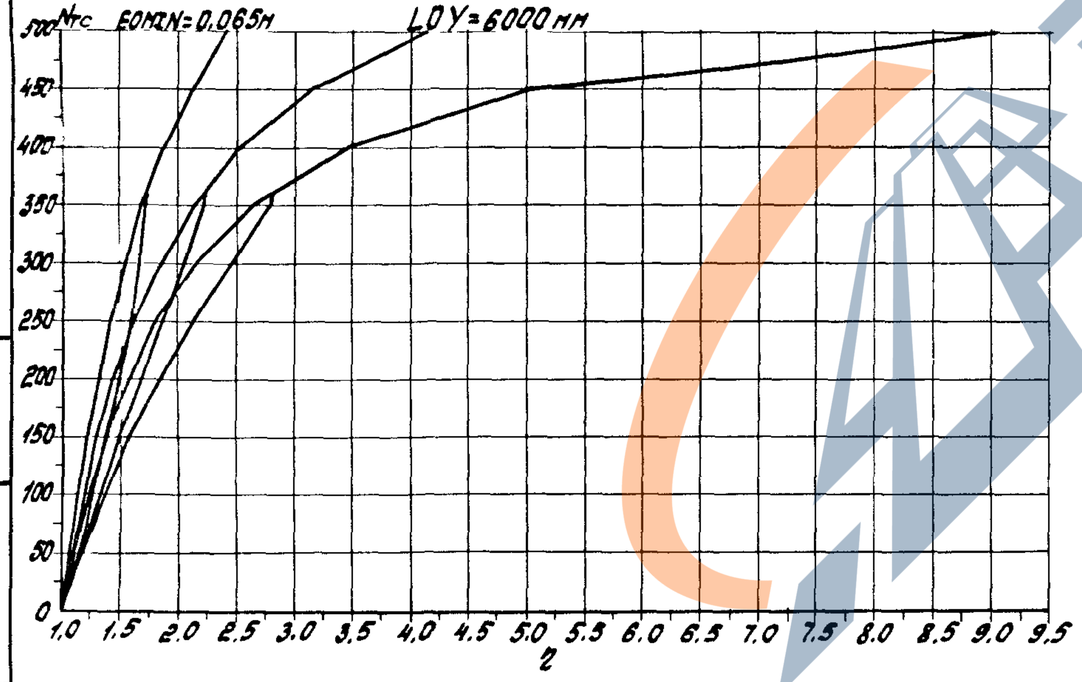
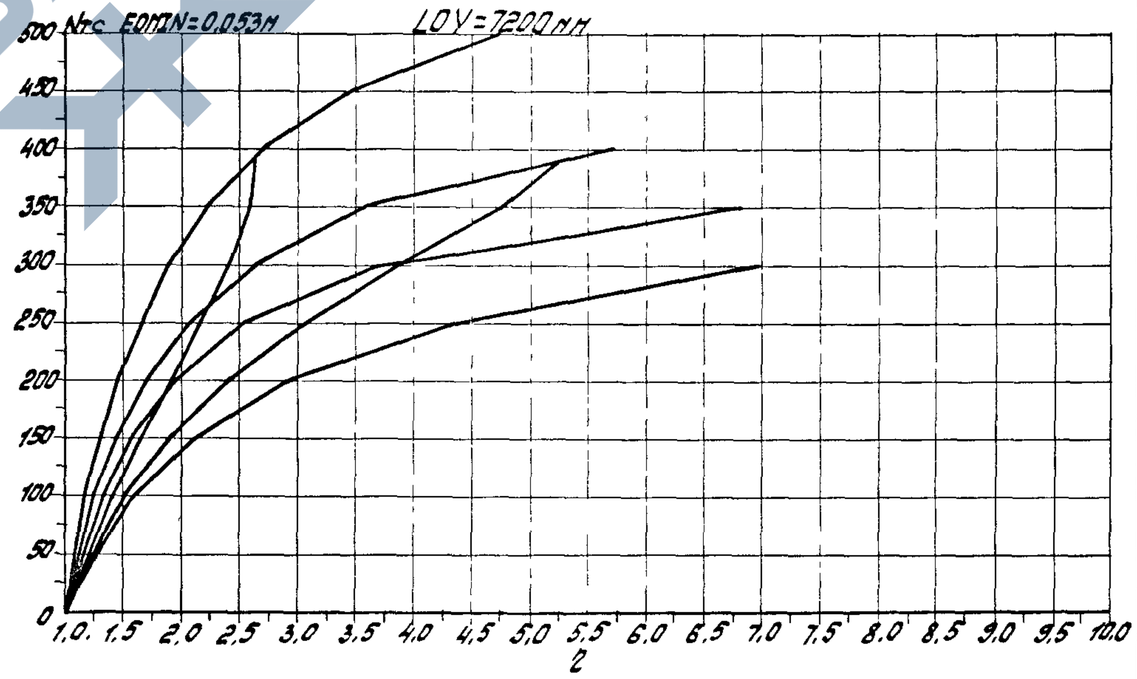








Инв.№ подл. | Подпись и дата | Взам.инв.№

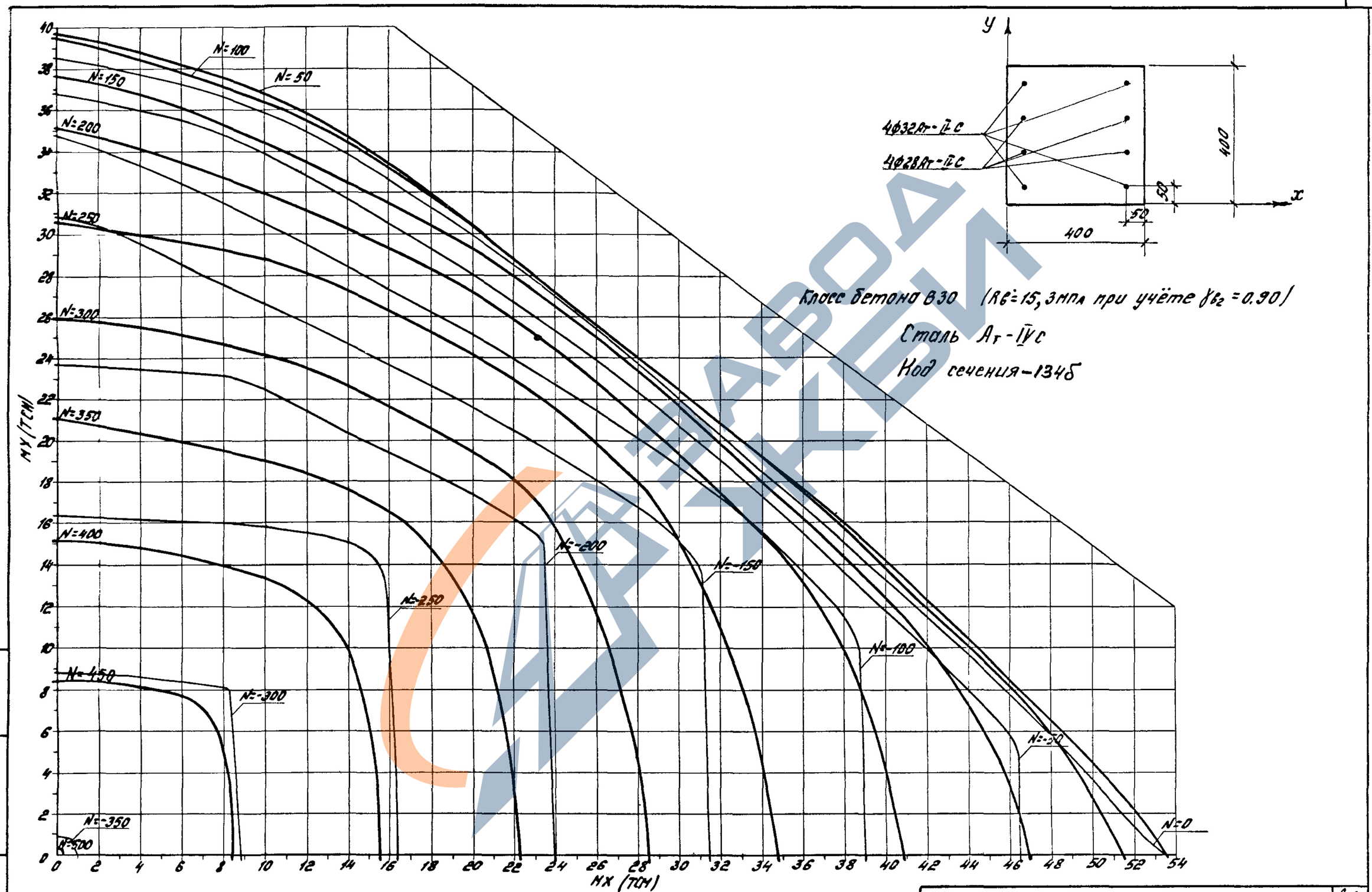
1.020.1-4. 0-9-002

Лист 268

24166-03 45

https://zavodjbi.com/

https://zavodjbi.com/



Класс бетона В30 ($R_в$=15,3 мпа при учёте $\gamma_{в2}$=0.90)

Сталь $A_т$-IV С

Код сечения-134б

ЗАВОД ЖБИ

Инв. N подл.	Подпись и дата	Взам. инв. N

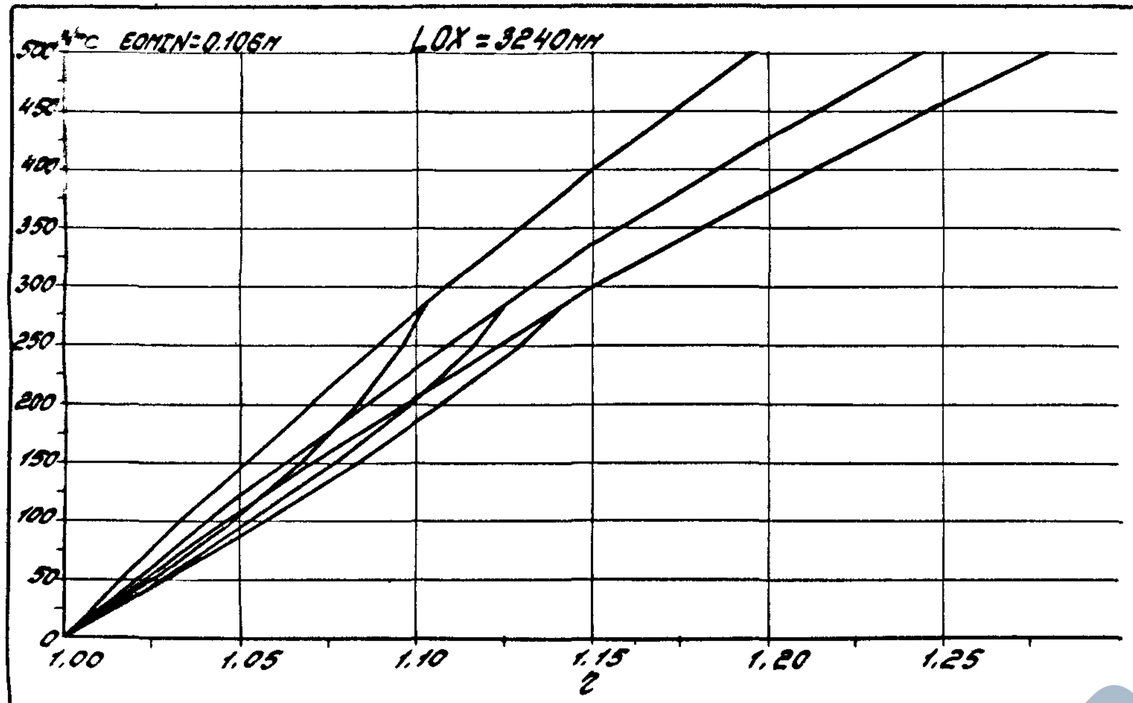
1.020.1-4. 0-9-002

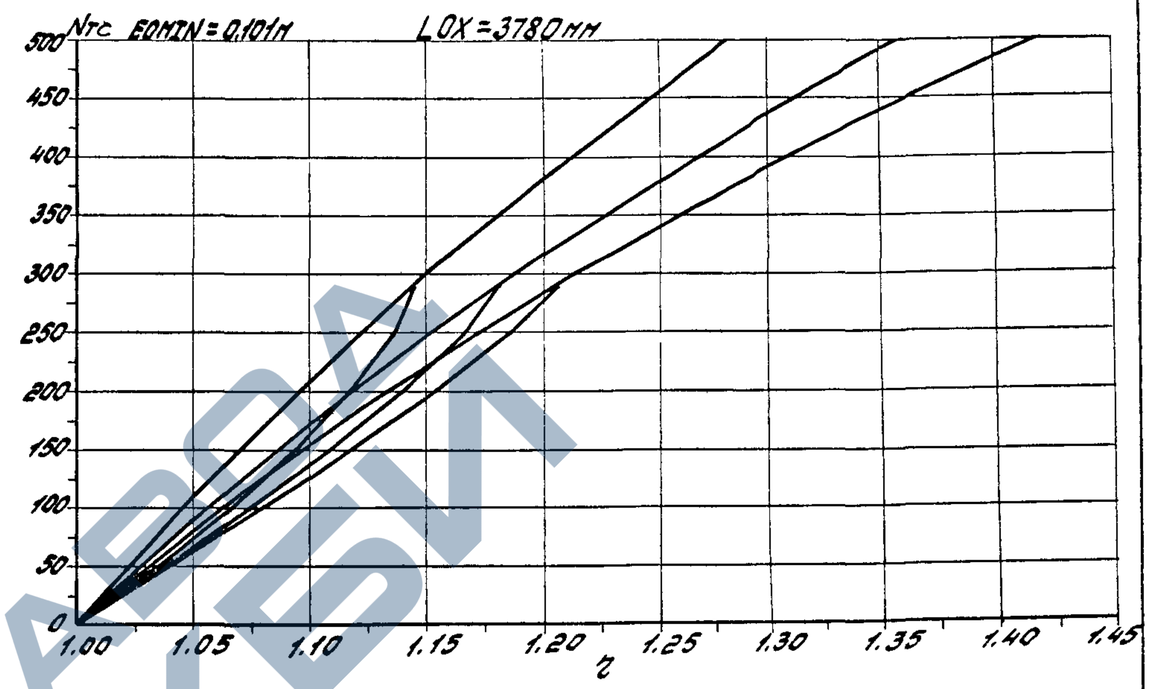
Лист 269

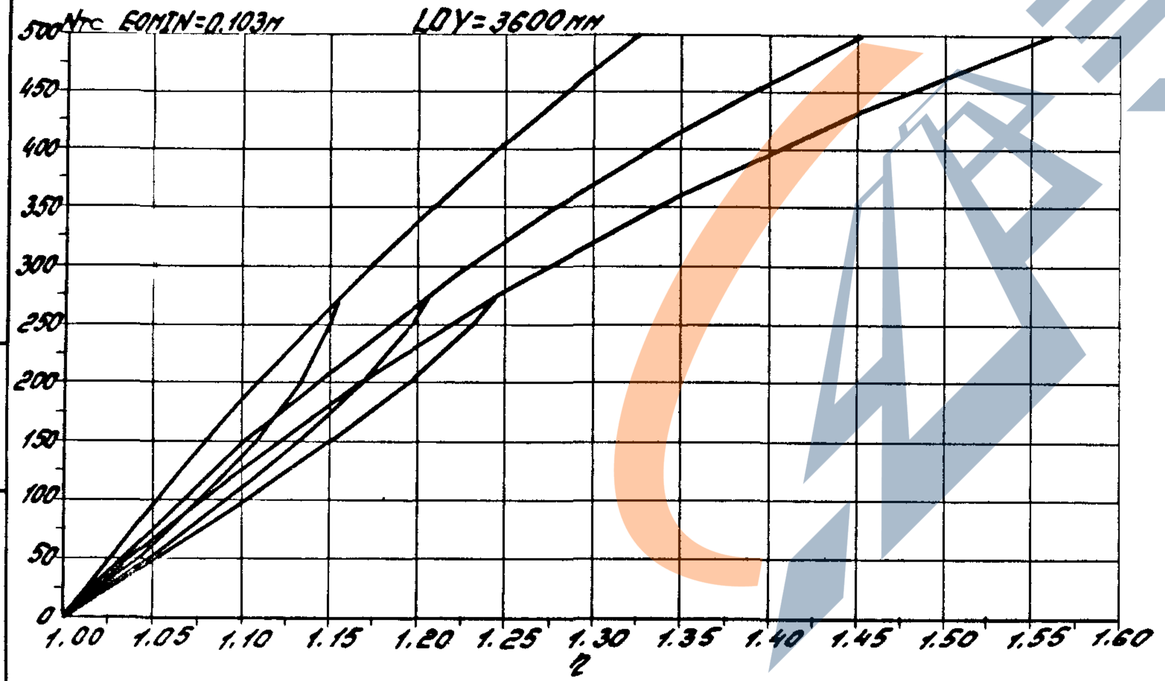
24166-03 46

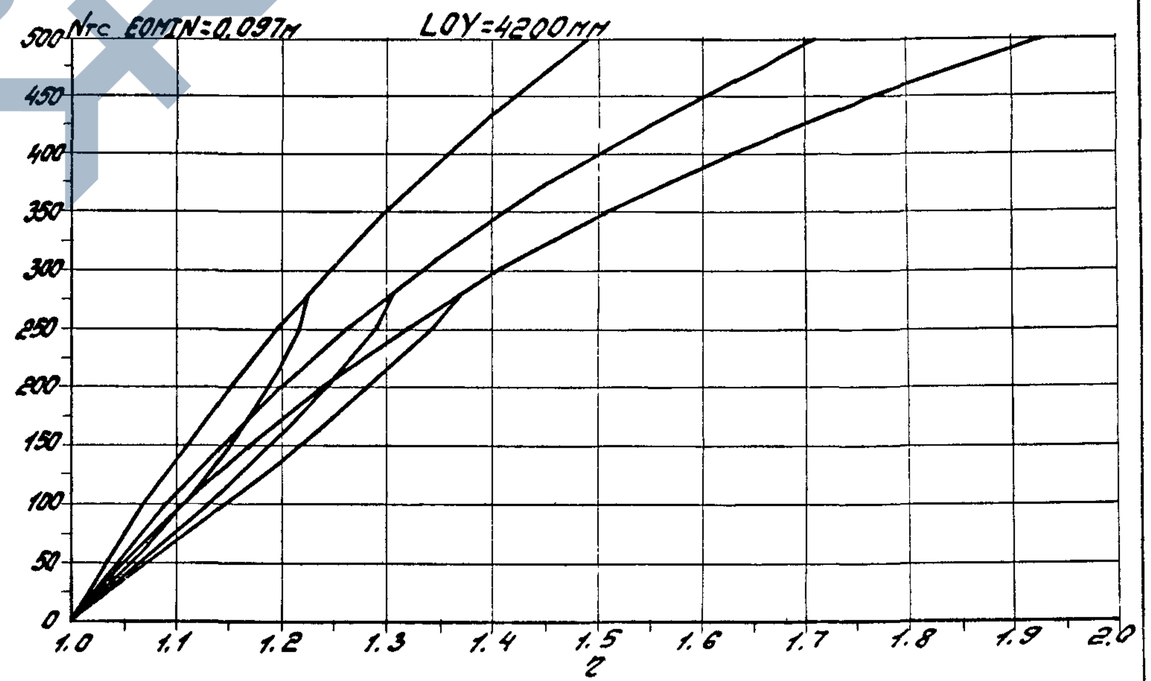
https://zavodjbi.com/

https://zavodjbi.com/









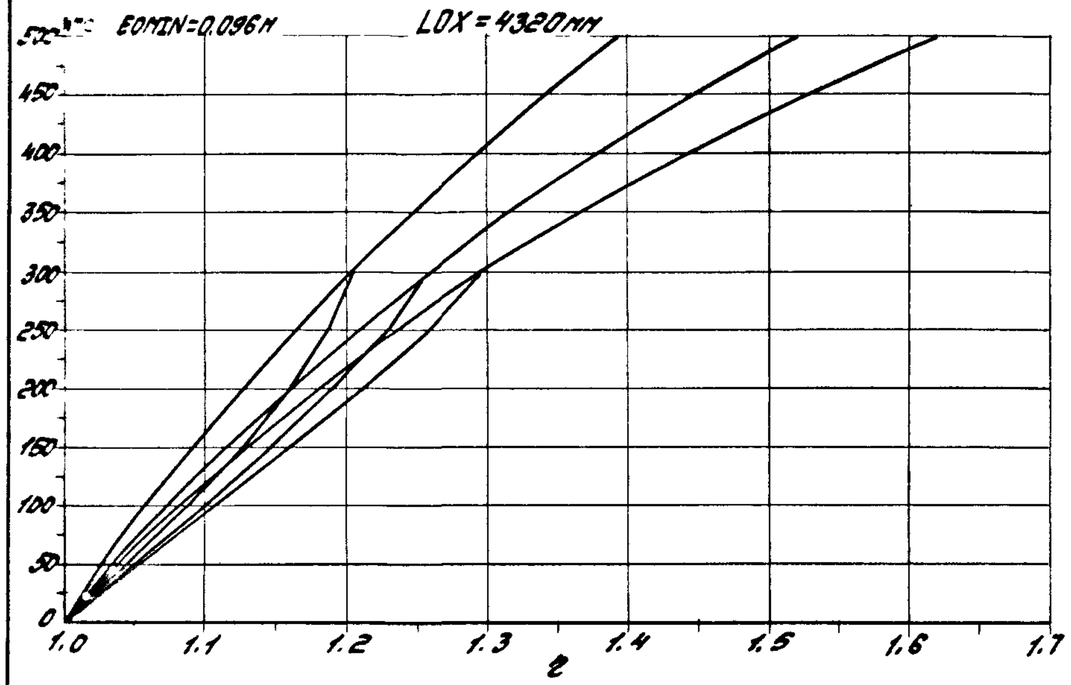
Инв.№ подл. | Подпись и дата | Взам.инв.№

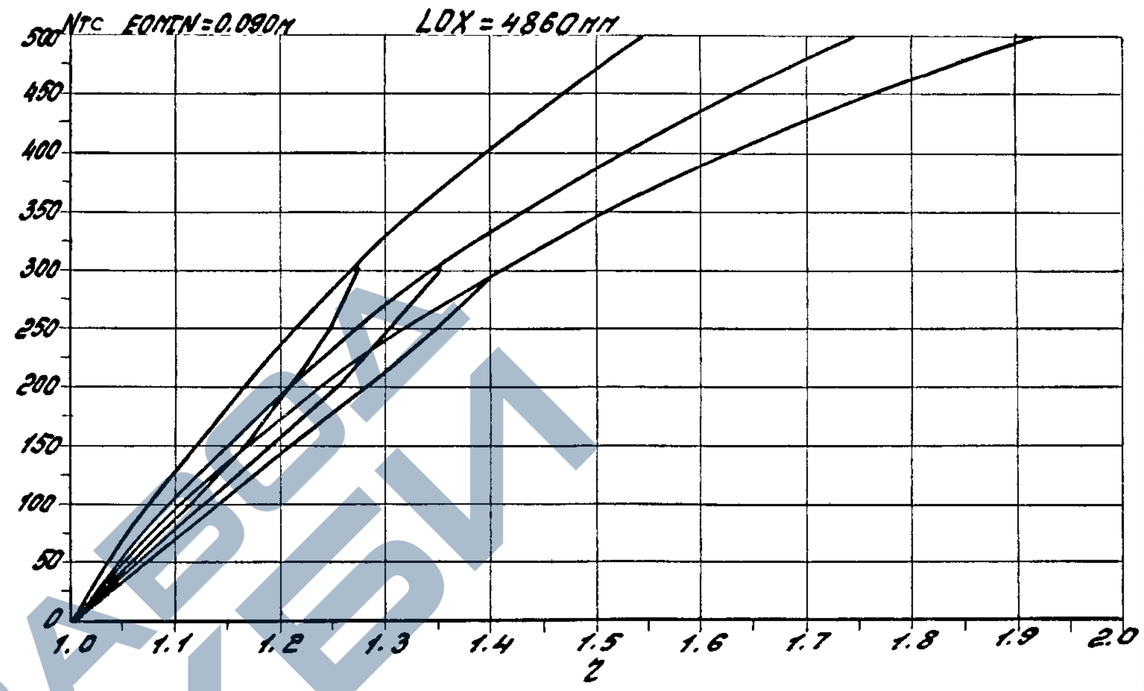
1.020.1-4. 0-9-002

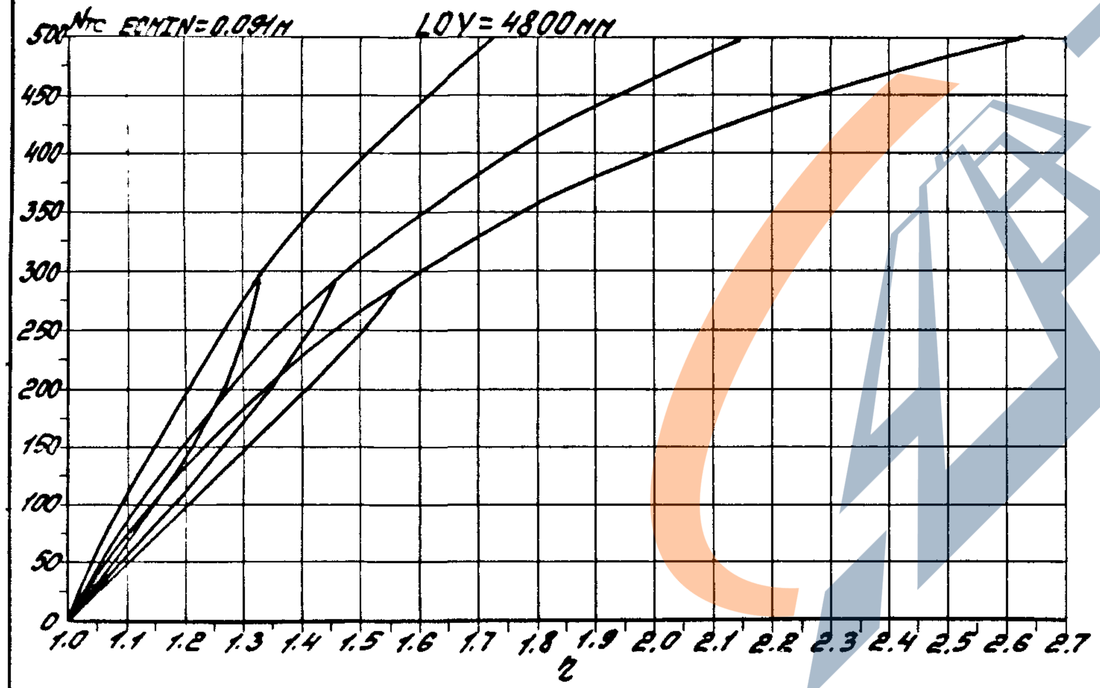
Лист 270

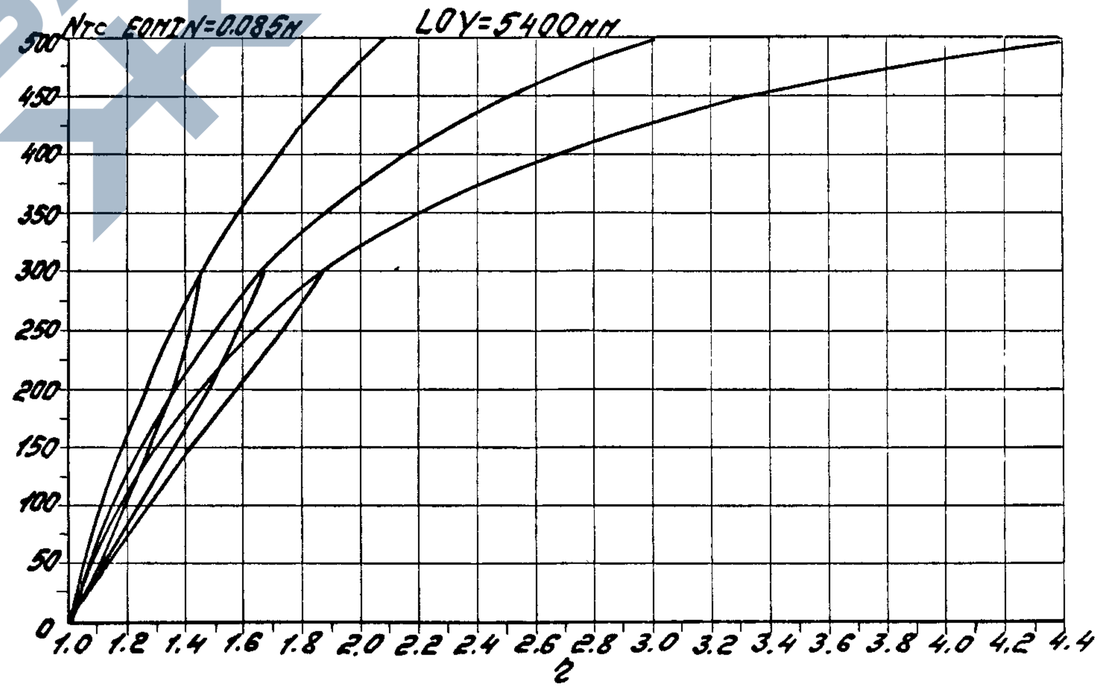
24166-03 47

https://zavodjbi.com/









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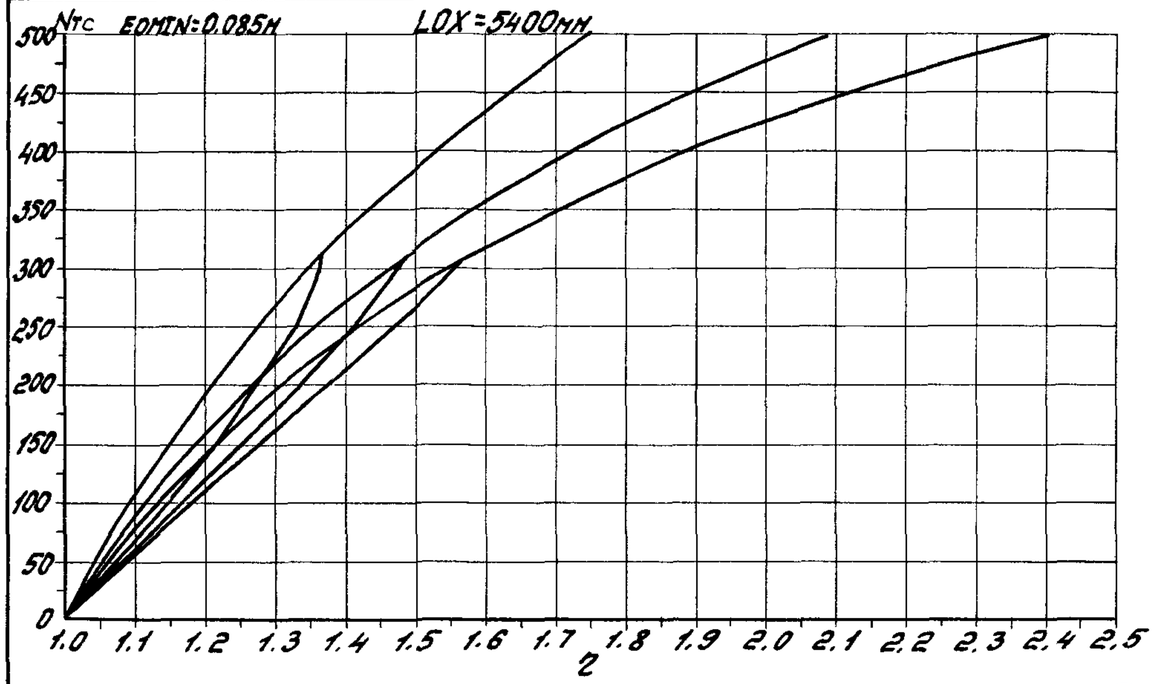
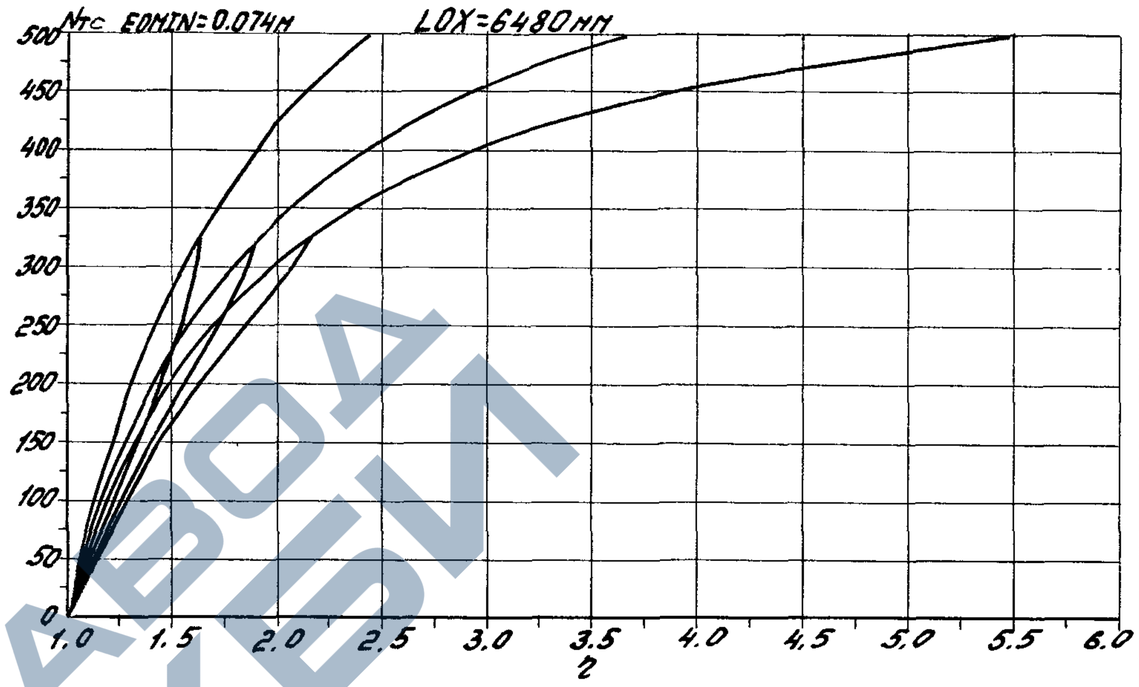
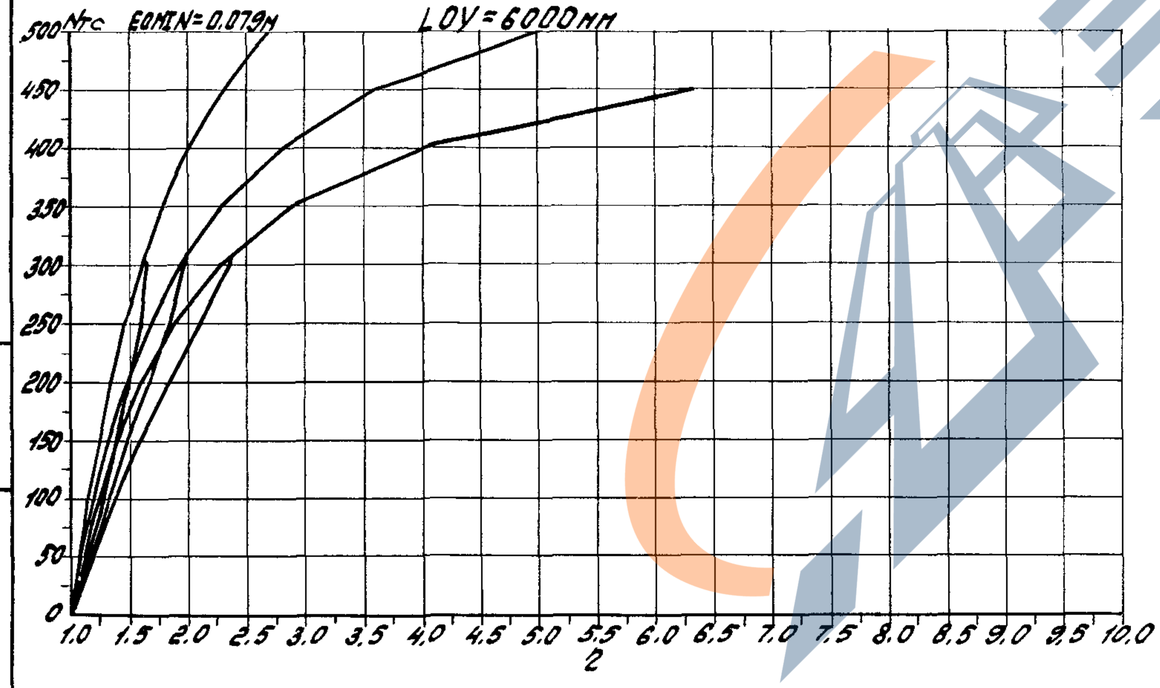
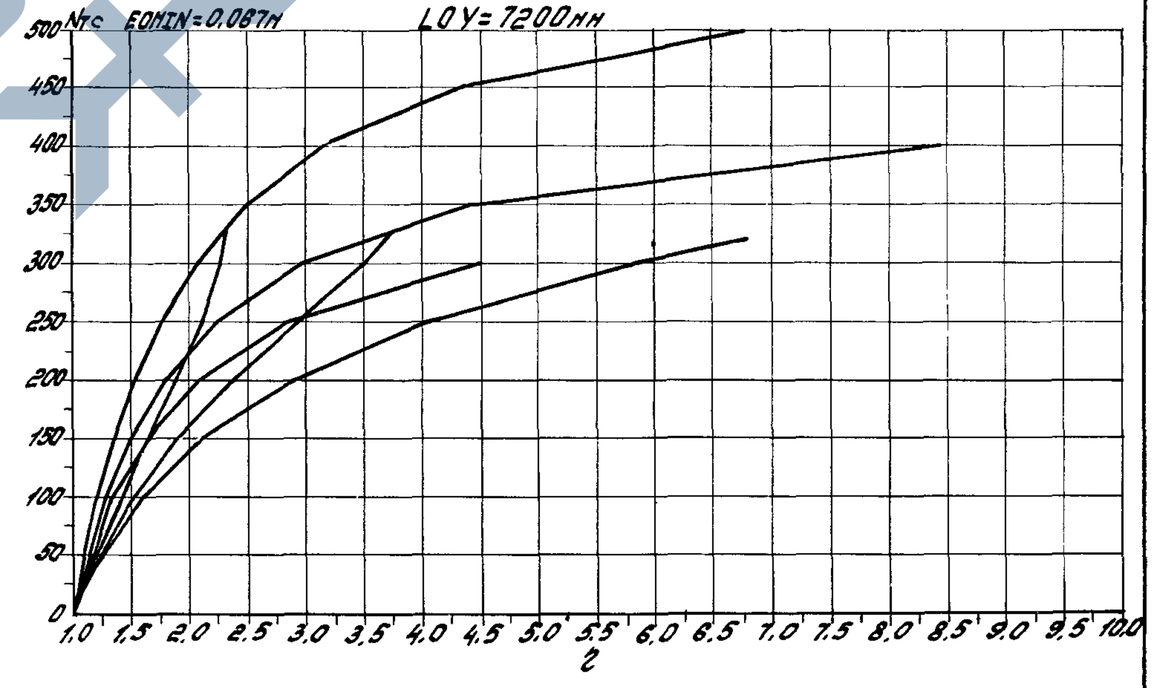
https://zavodjbi.com/









Инв.N подл. | Подпись и дата | Взам.инв.N

1.020.1-4 0-9 002

Лист 272

24166-08 49

https://zavodjbi.com/

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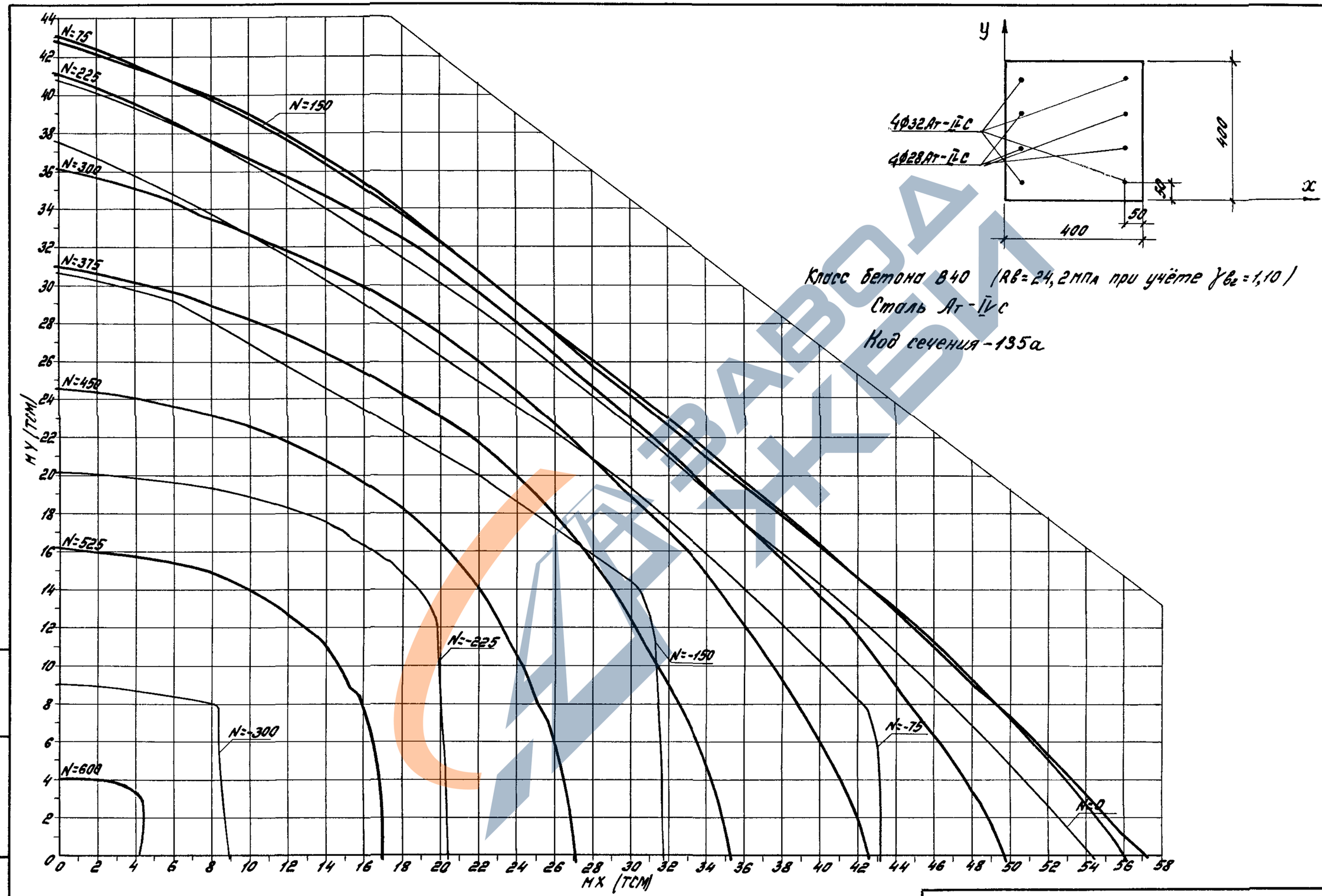

Класс бетона В40 (Rв=24,2МПа при учёте γ_{b2}=1,10)

Сталь Ат-IVс

Код сечения-135а

Инв.№ подл. | Подп. и дата | Взам.инв.№

1.020.1-4 0-9 002

Лист 273

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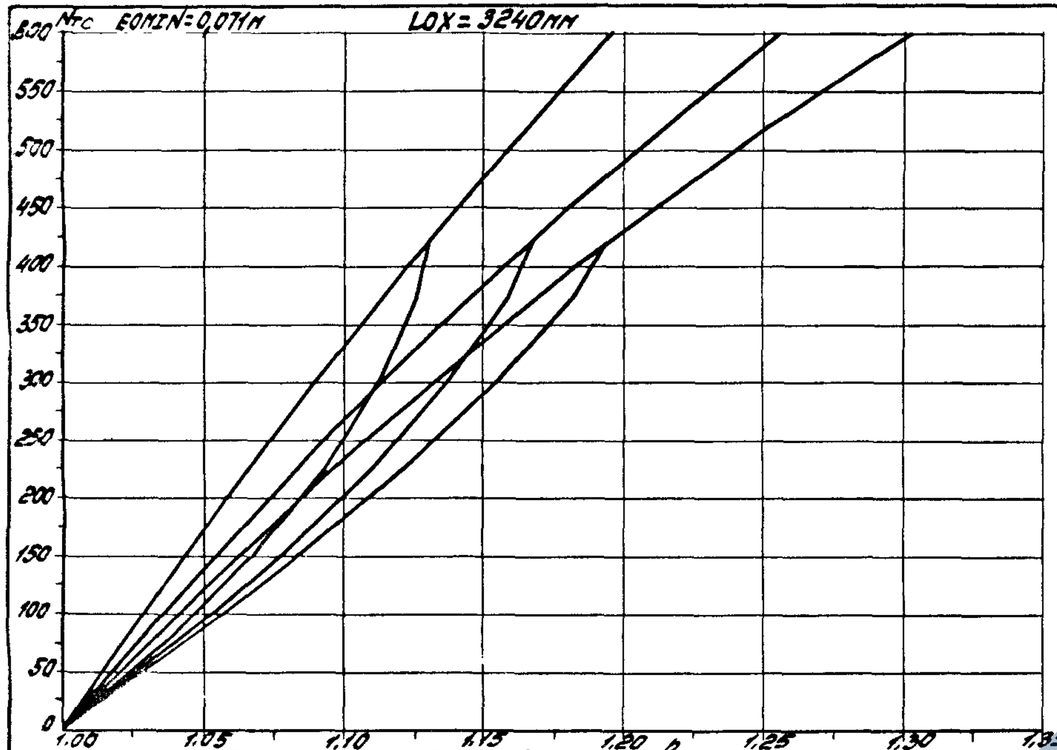

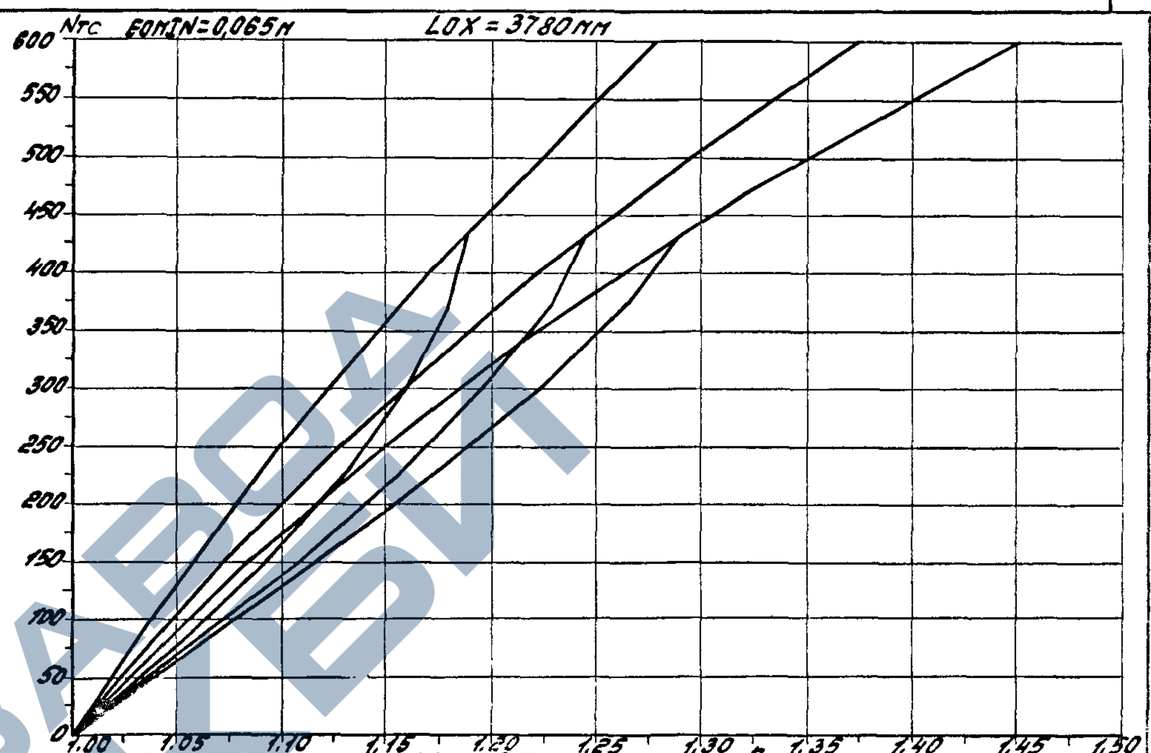

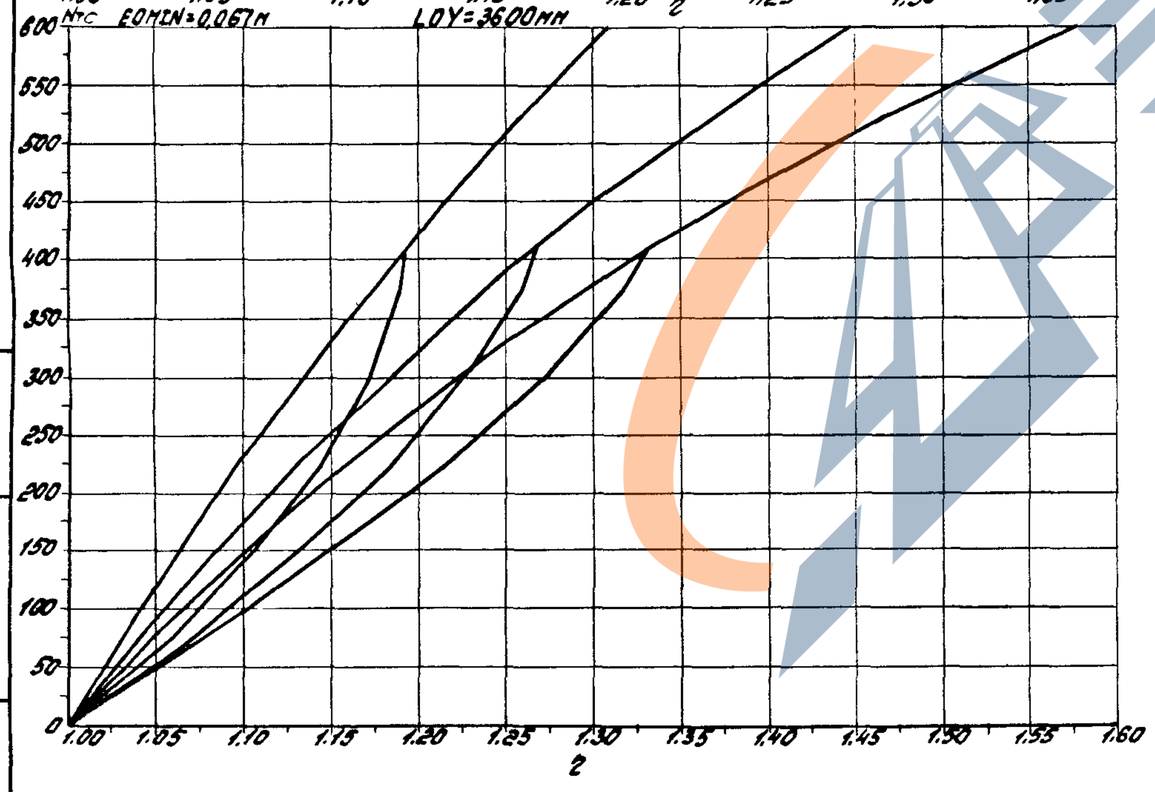

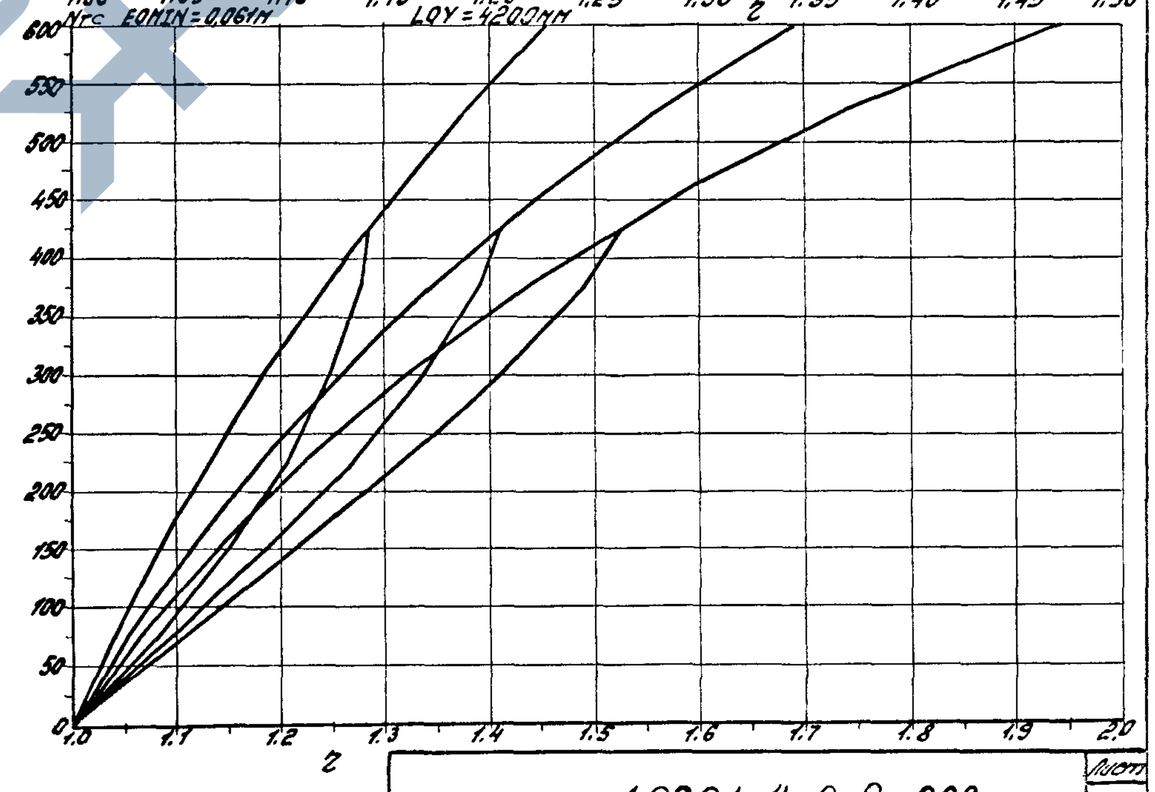

Инв.№ подл. | Подпись и дата | Взам. инв.№

1.020.1-4. 0-9-002

Лист 274

24166-03 51

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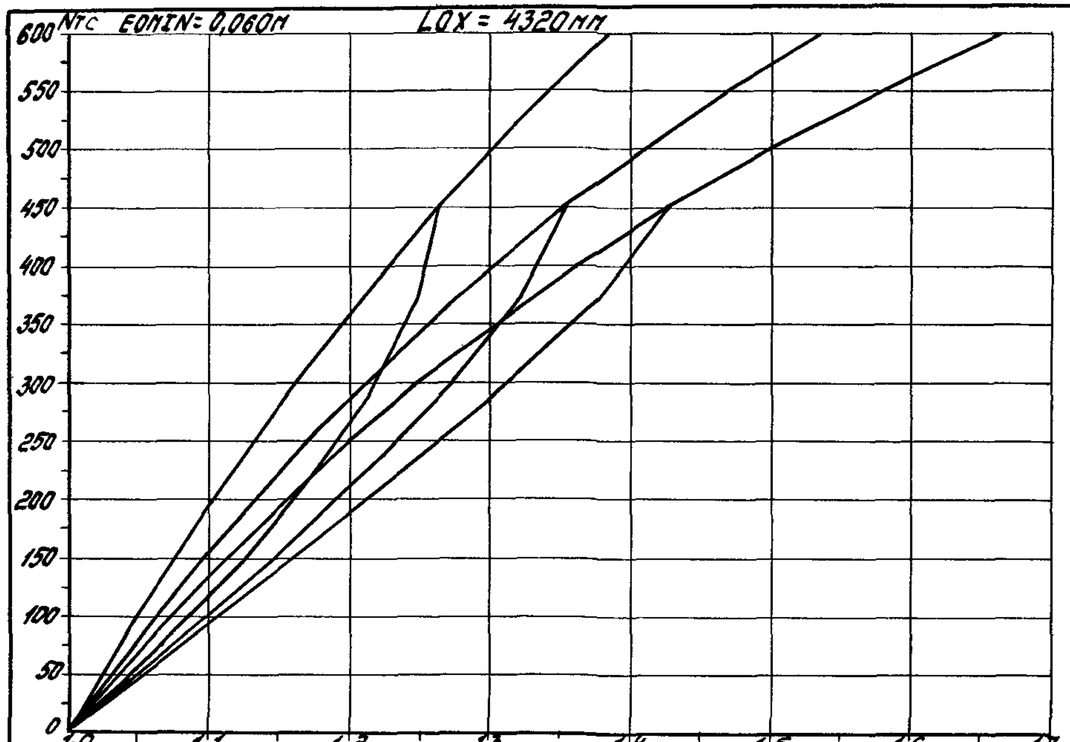

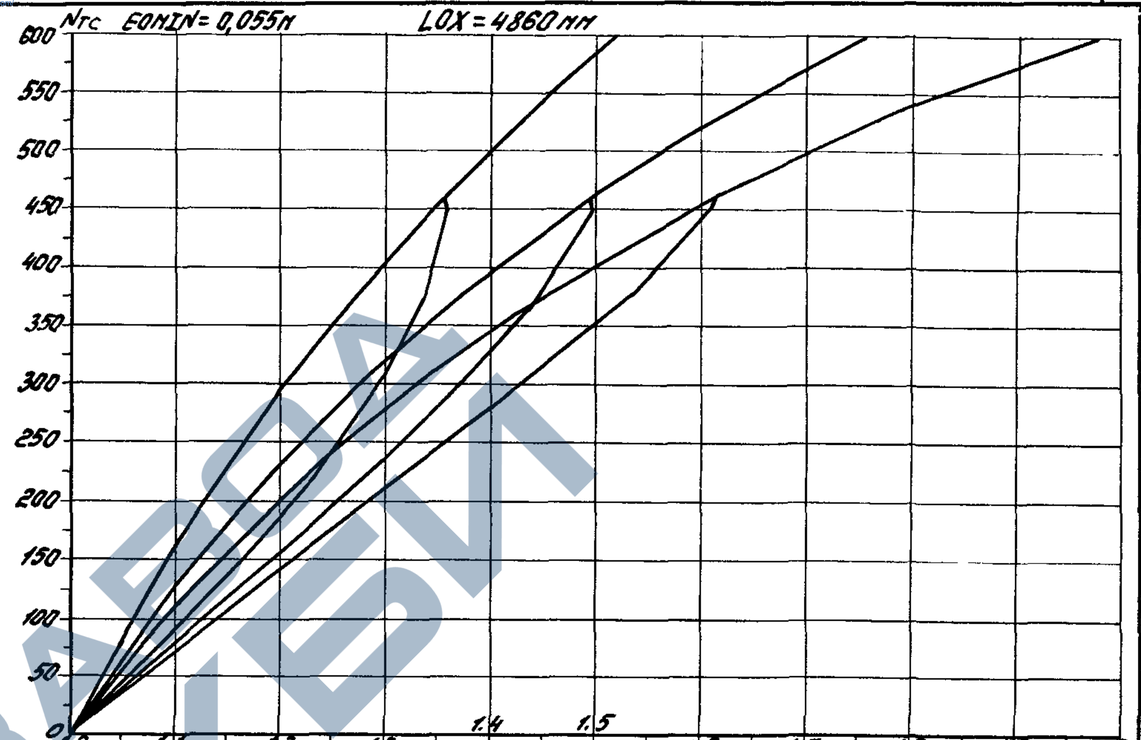

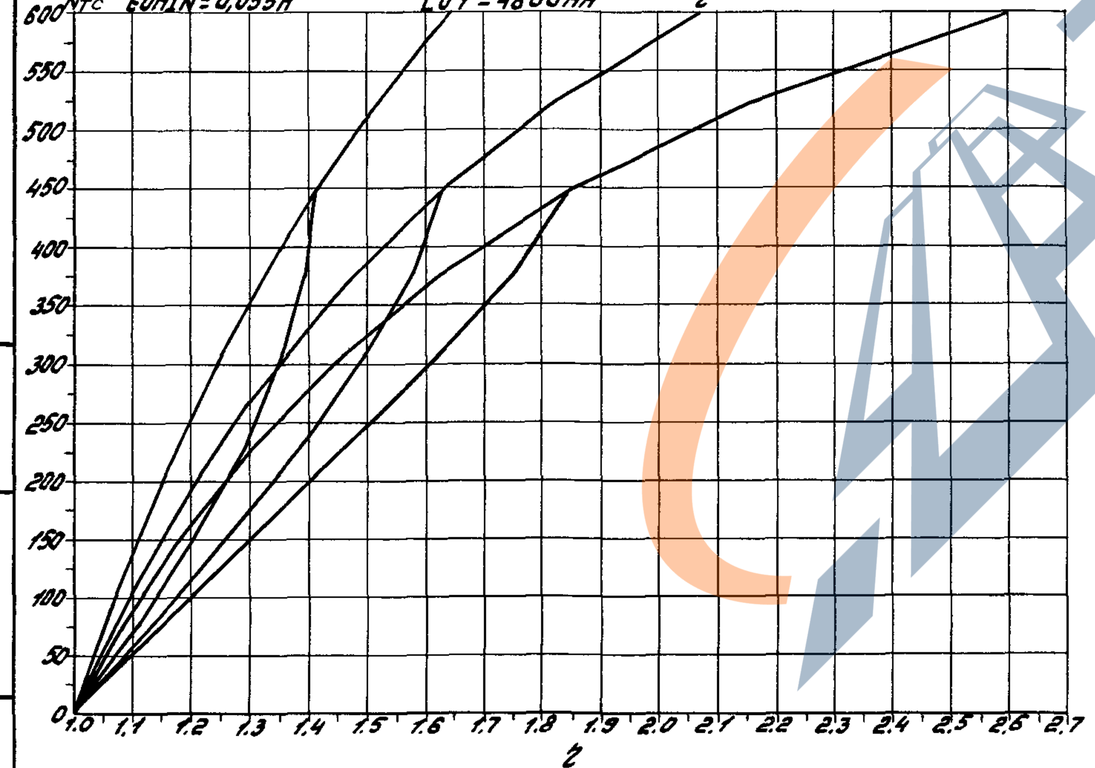

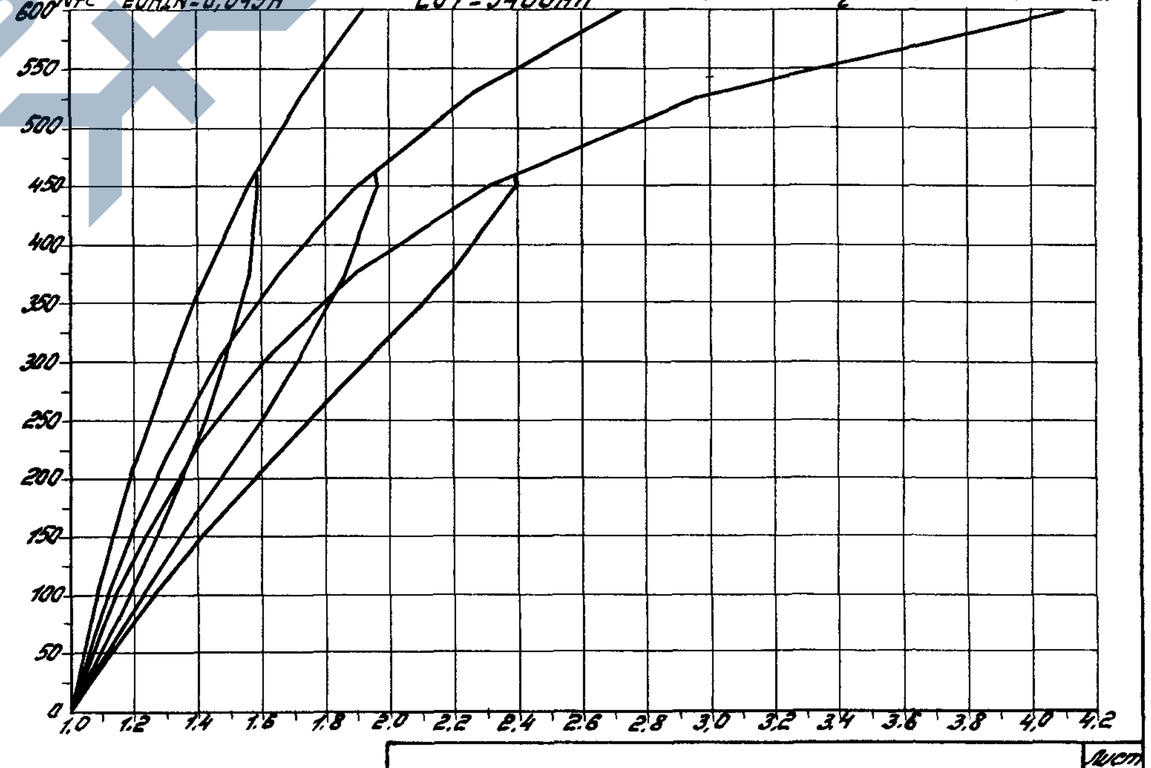

Инв.№подл. | Подпись и дата | Взам. инв.№

1.020.1-4 0-9 002

Лист 275

24166-03 52

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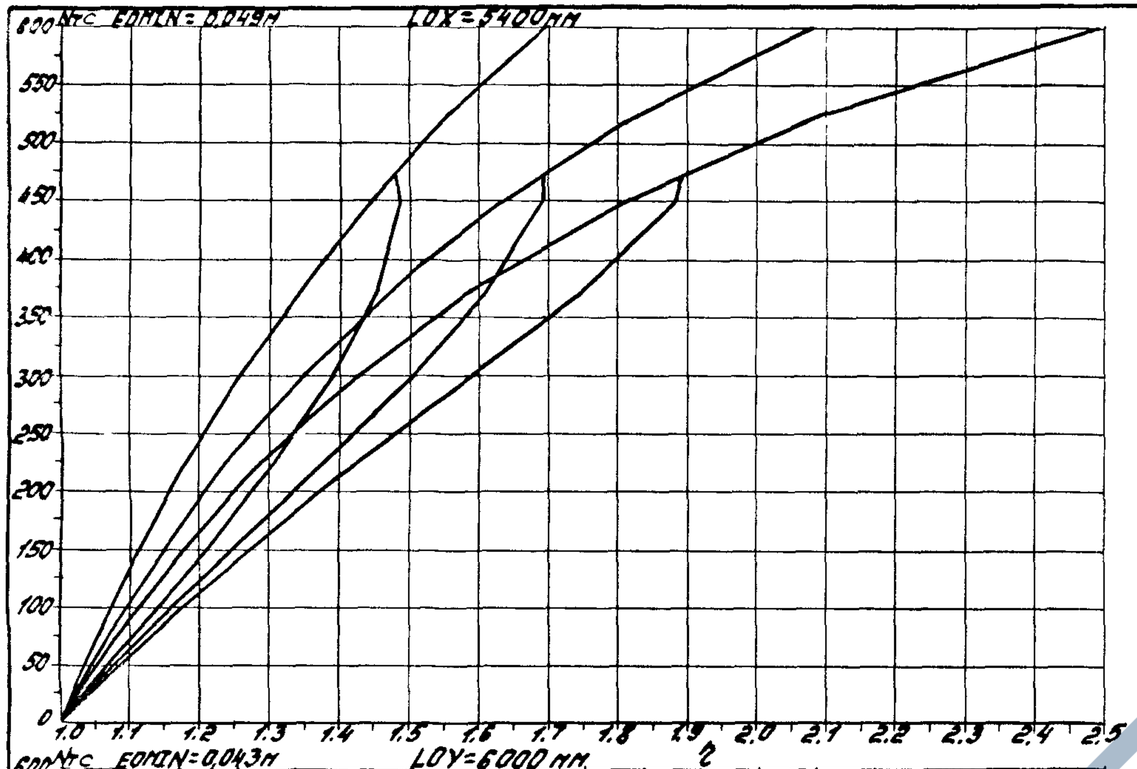
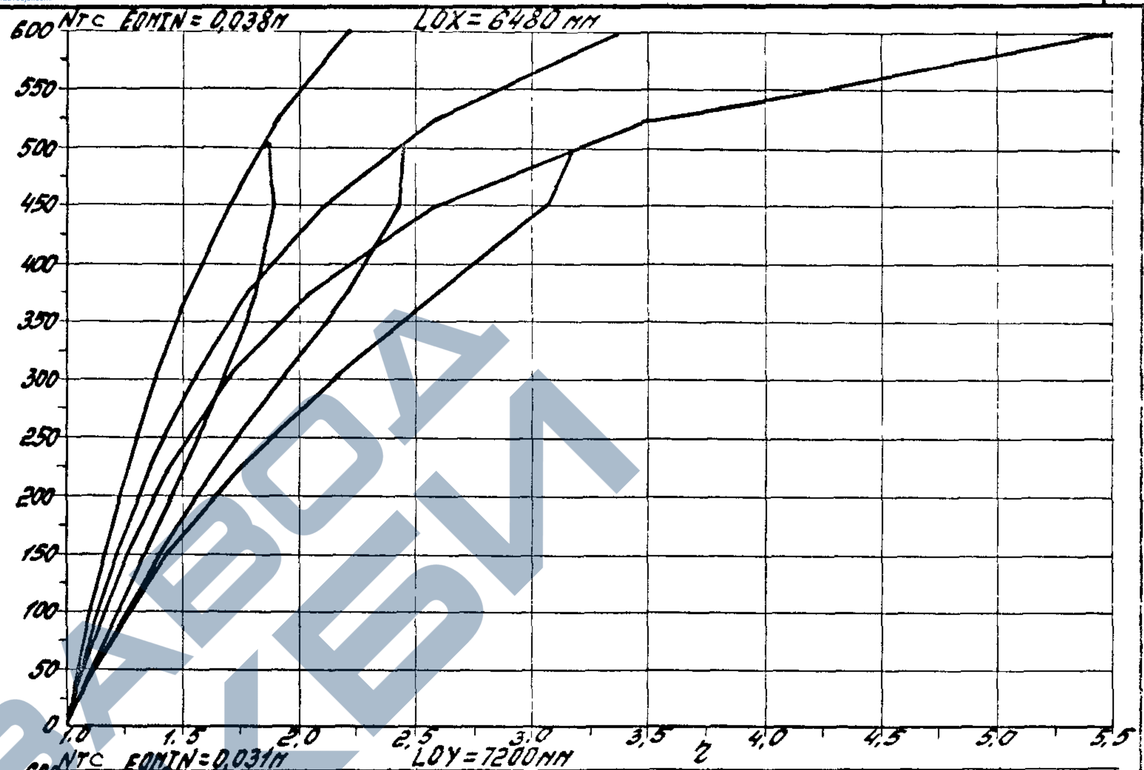
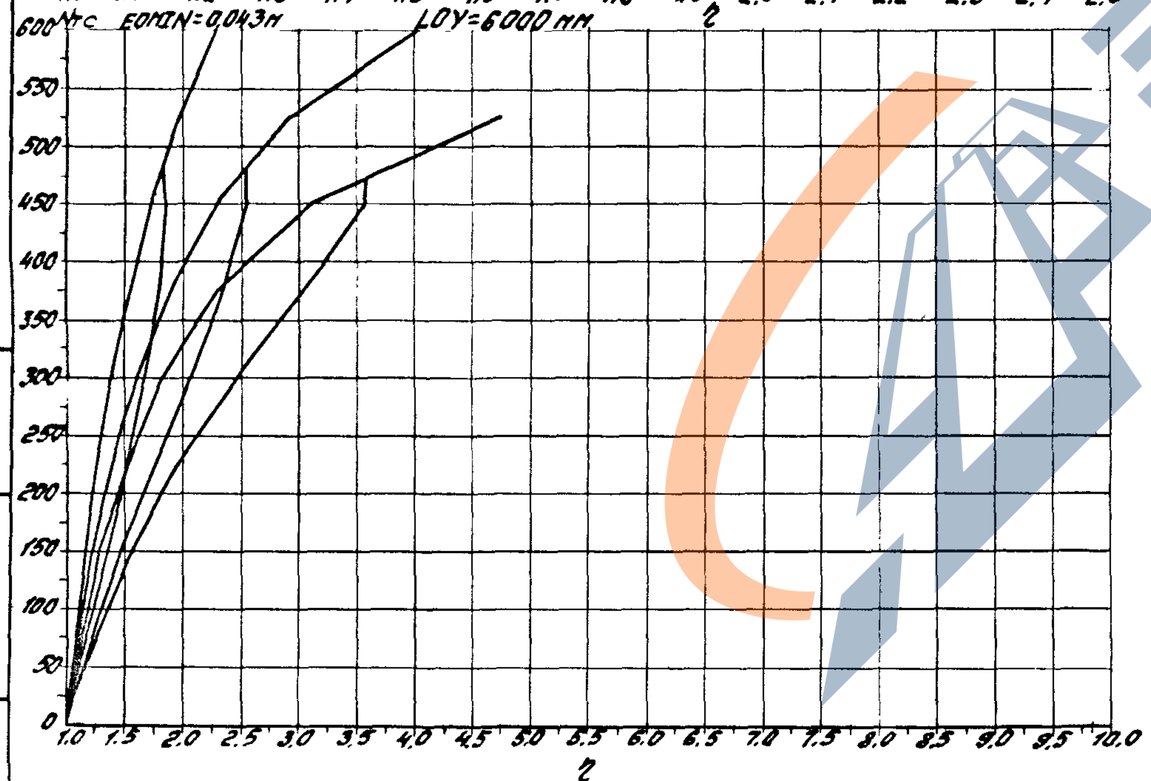
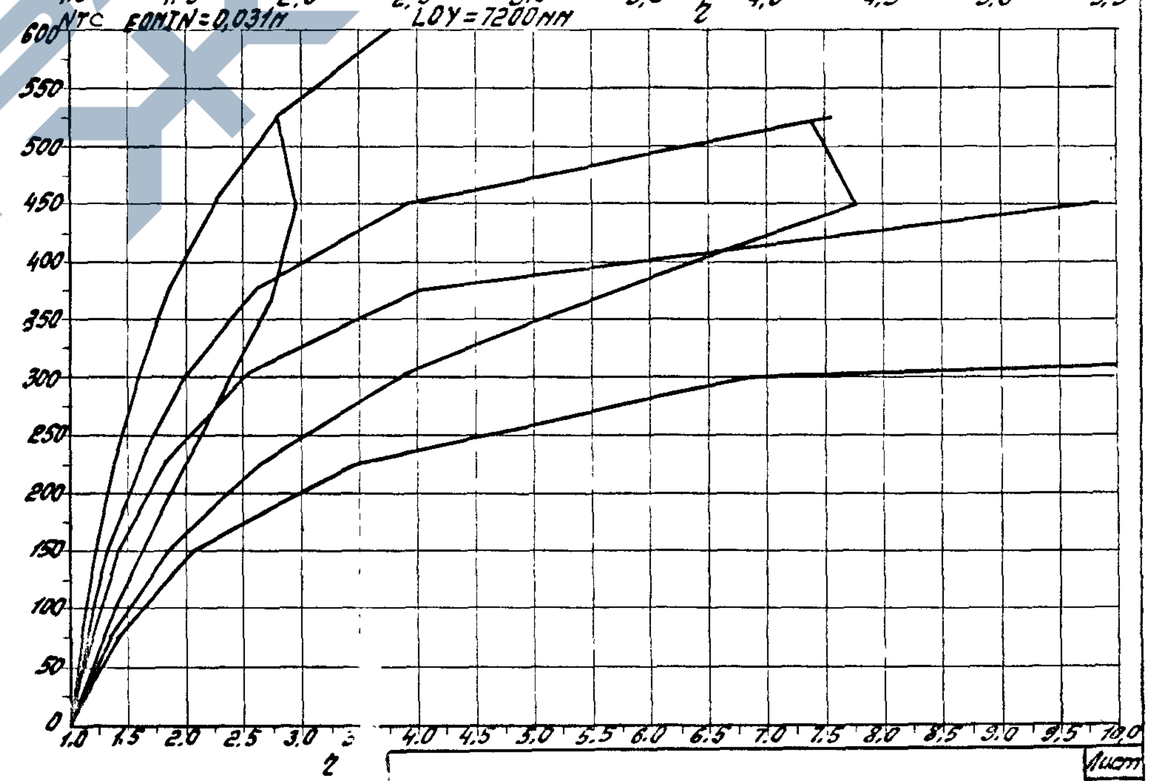
https://zavodjbi.com/





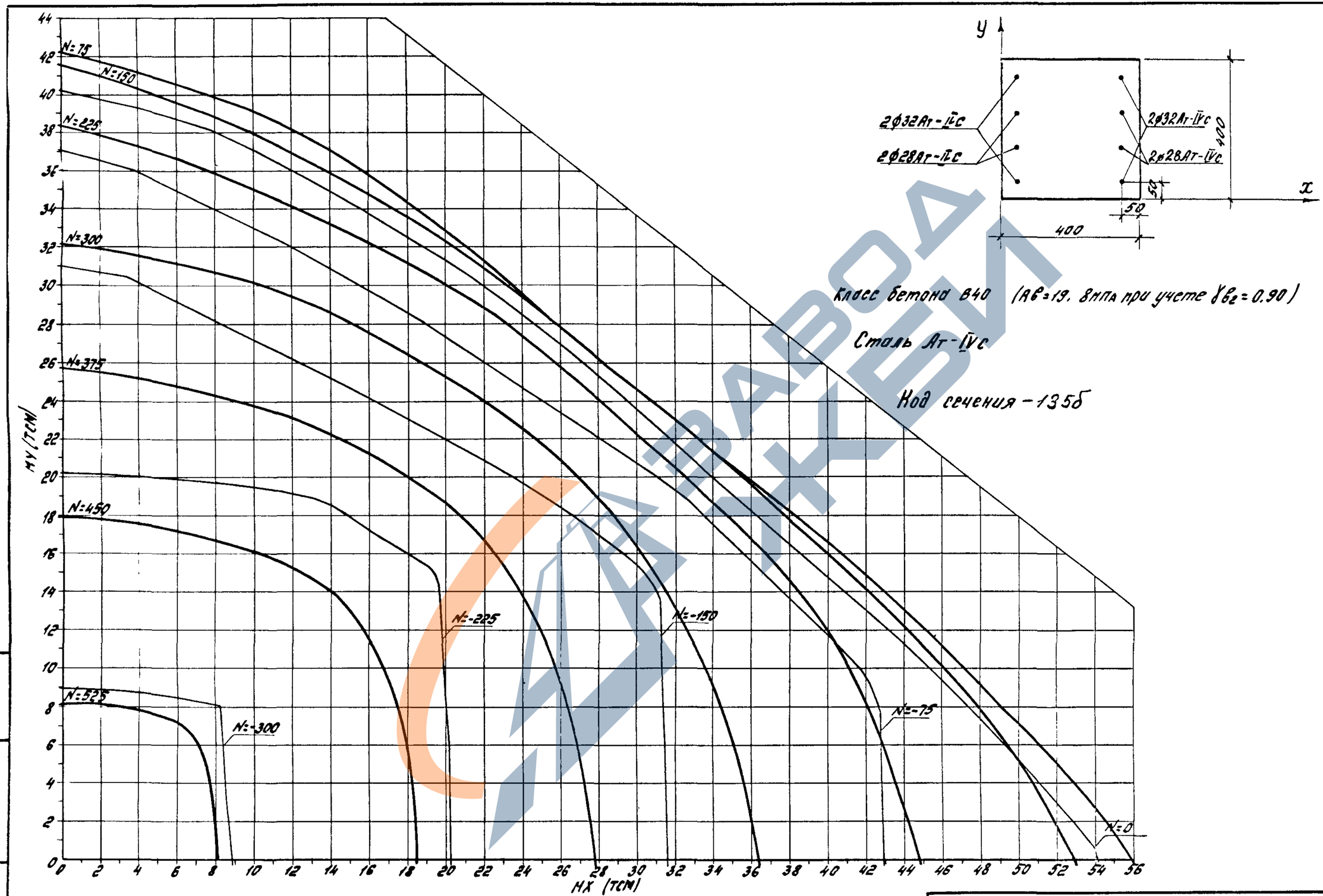




Инв.№ подл. | Подпись и дата | Взам.инв.№

https://zavodjbi.com/

https://zavodjbi.com/



Класс бетона В40 (R_B=19, 8МПа при учете γ_{B2}=0.90)

Сталь Ат-IVс

Код сечения – 135б

Инв.N подл. | Подпись и дата | Взам.инв.N

1.020.1-4. 0-9 – 002

Лист 277

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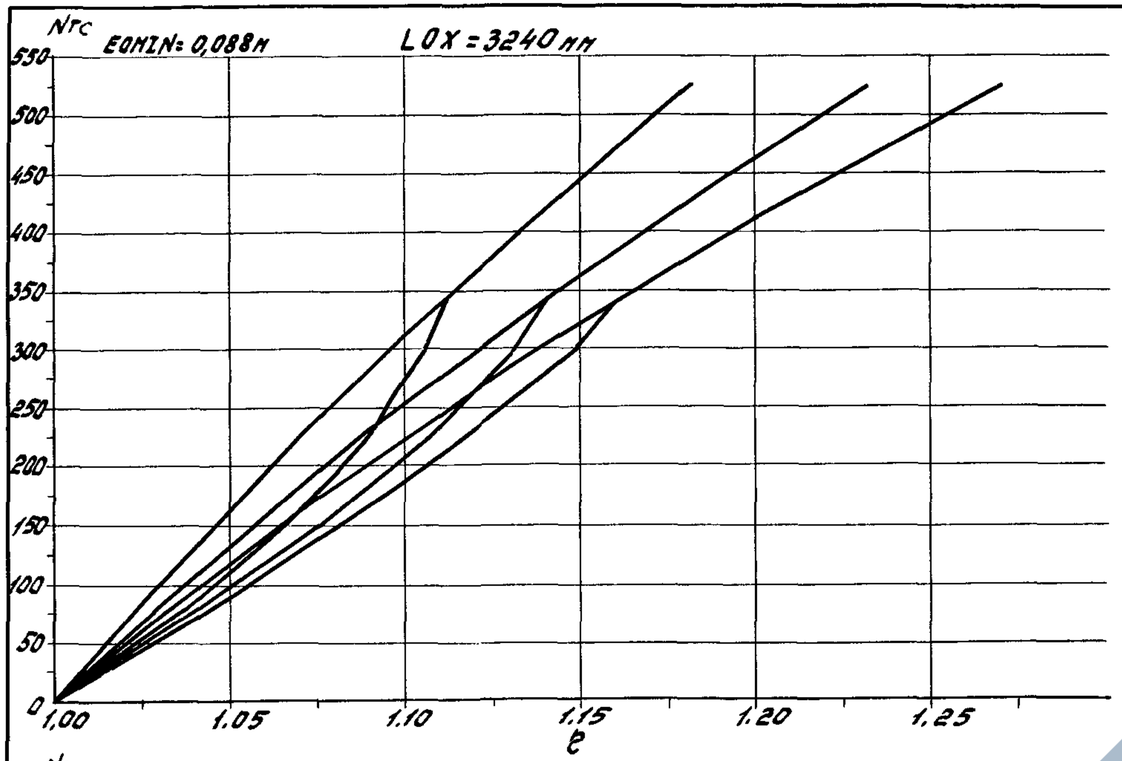
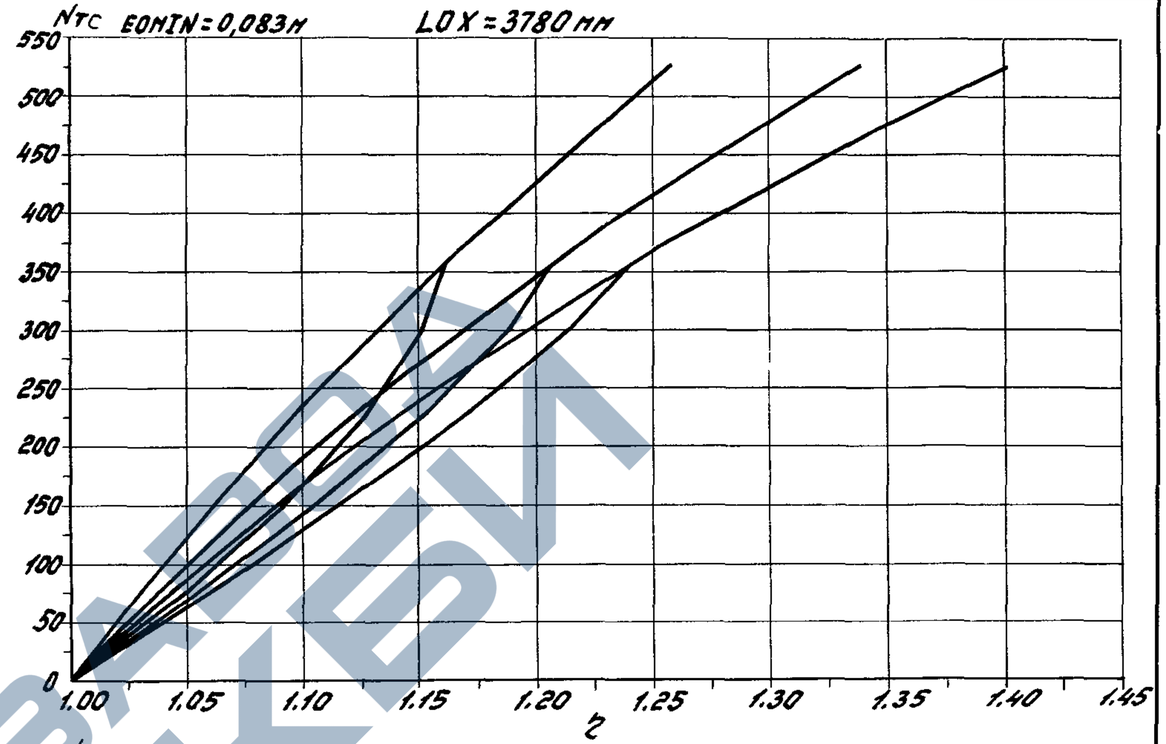
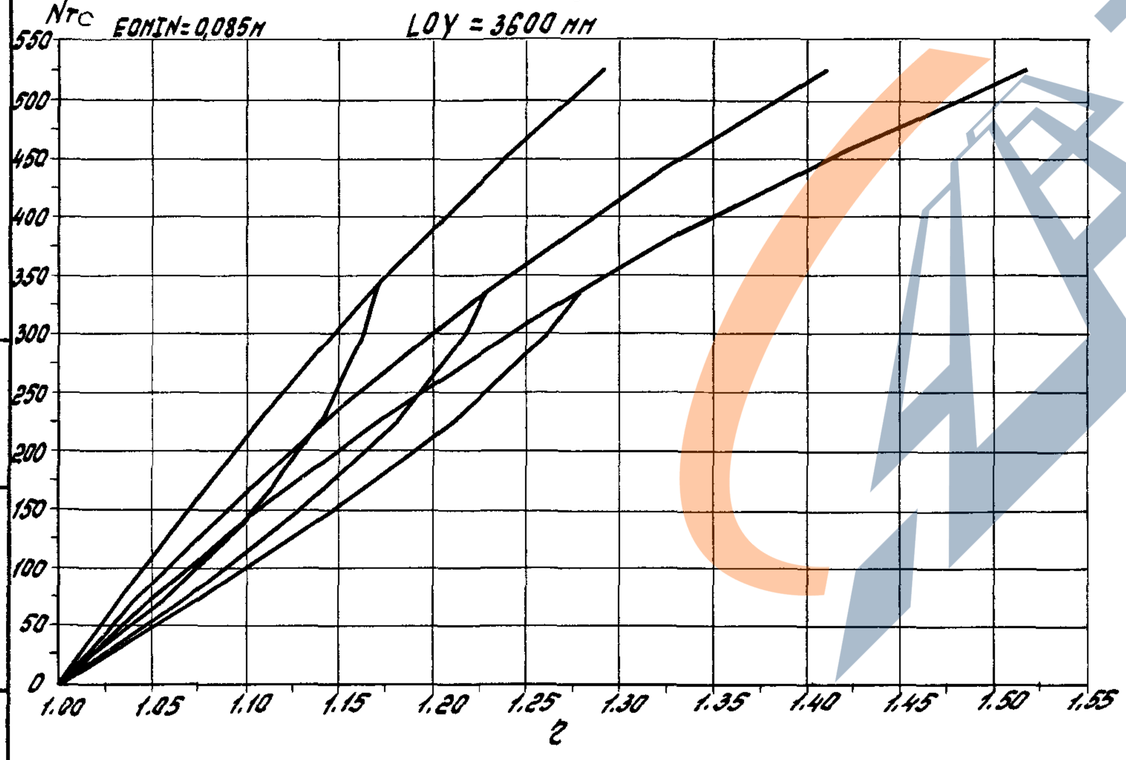
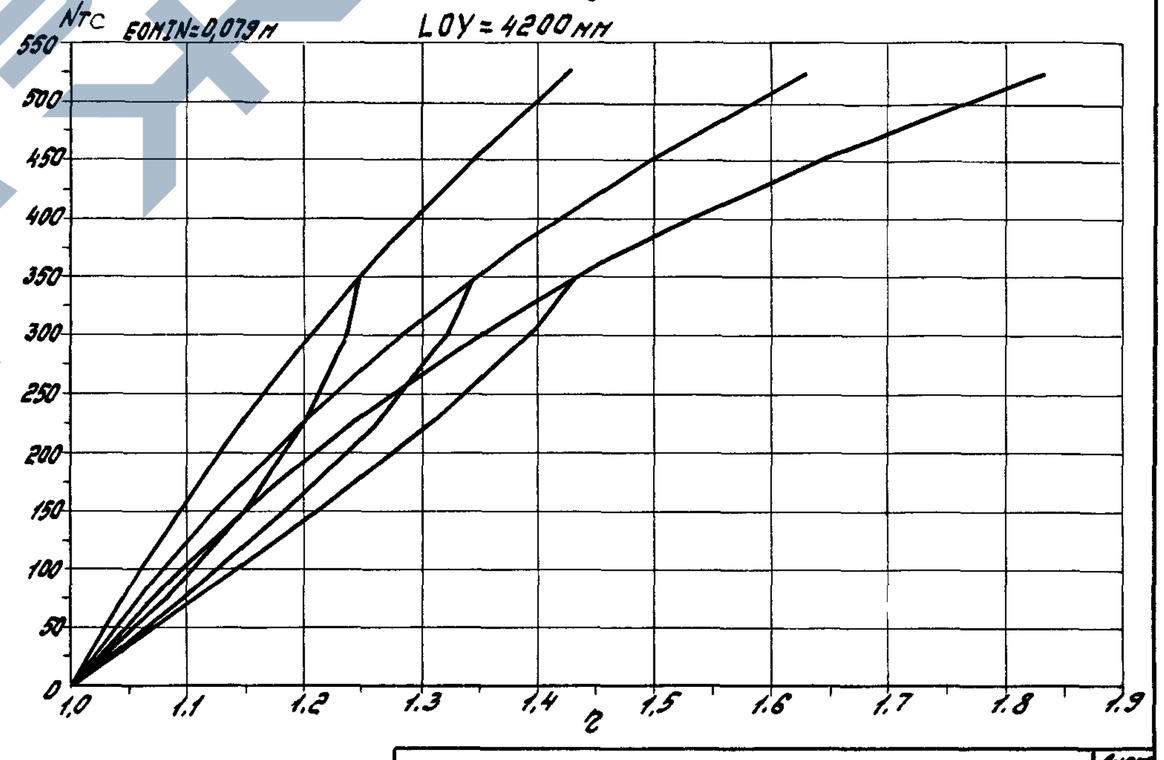








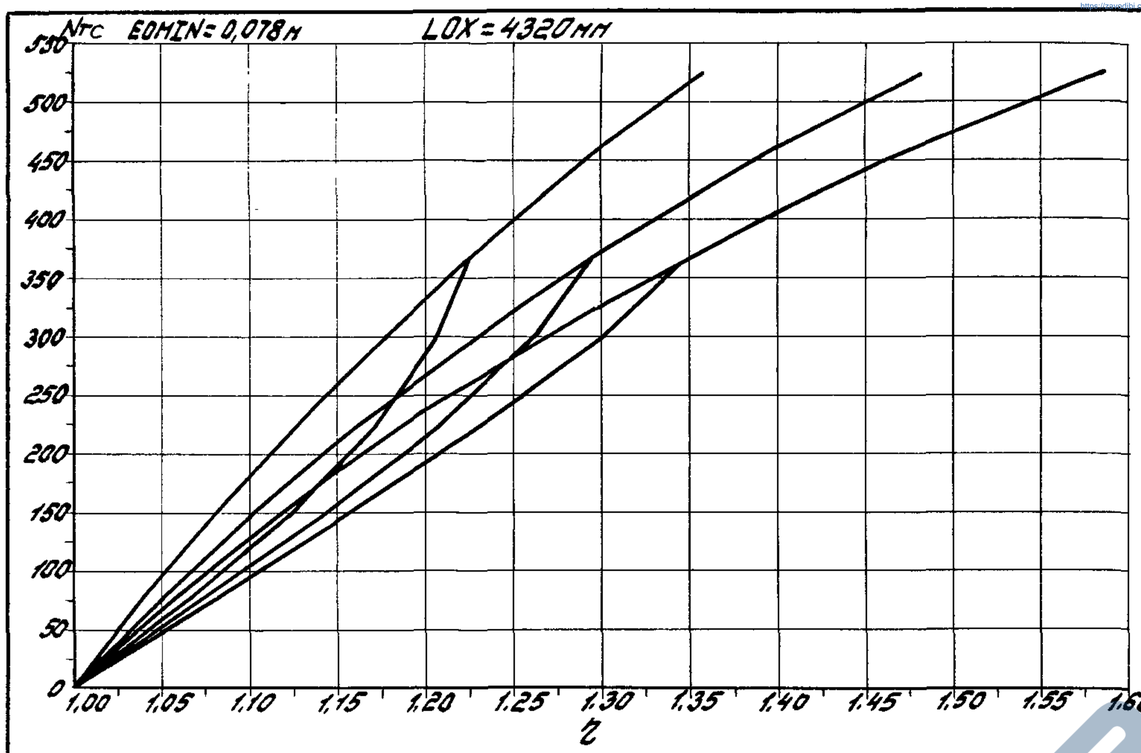
Инв.№ подл. | Подпись и дата | Взам.инв.№

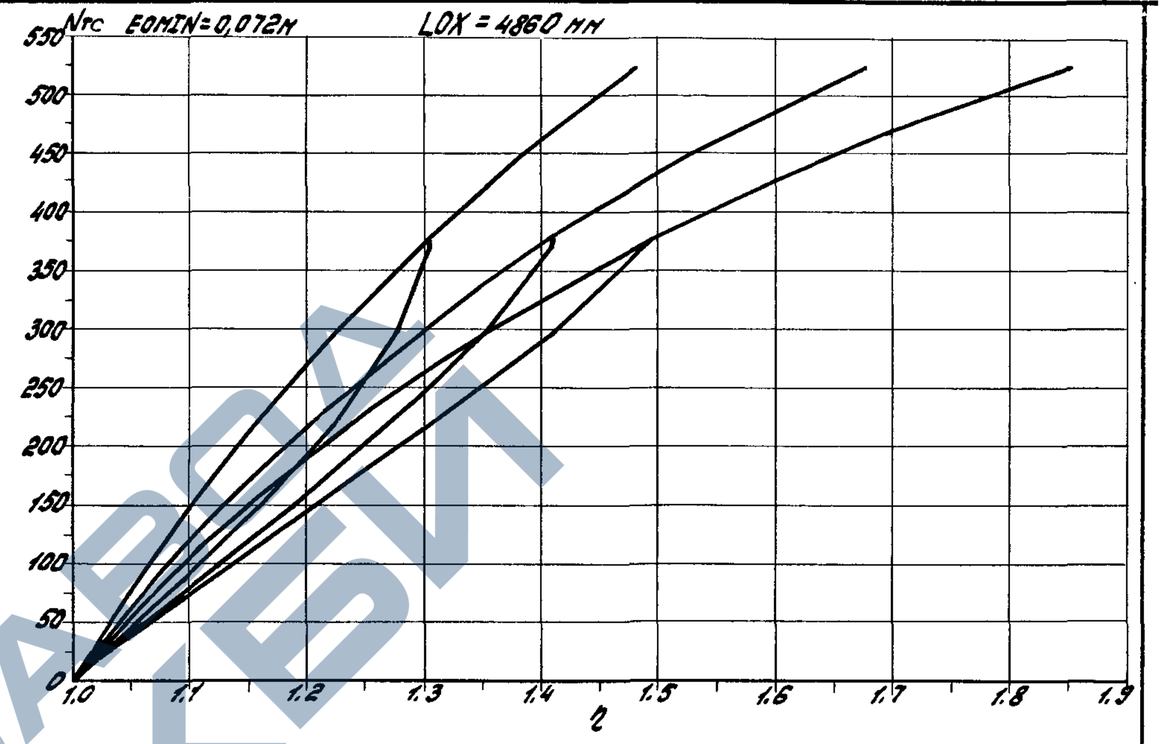
1.020.1-4 0-9 002

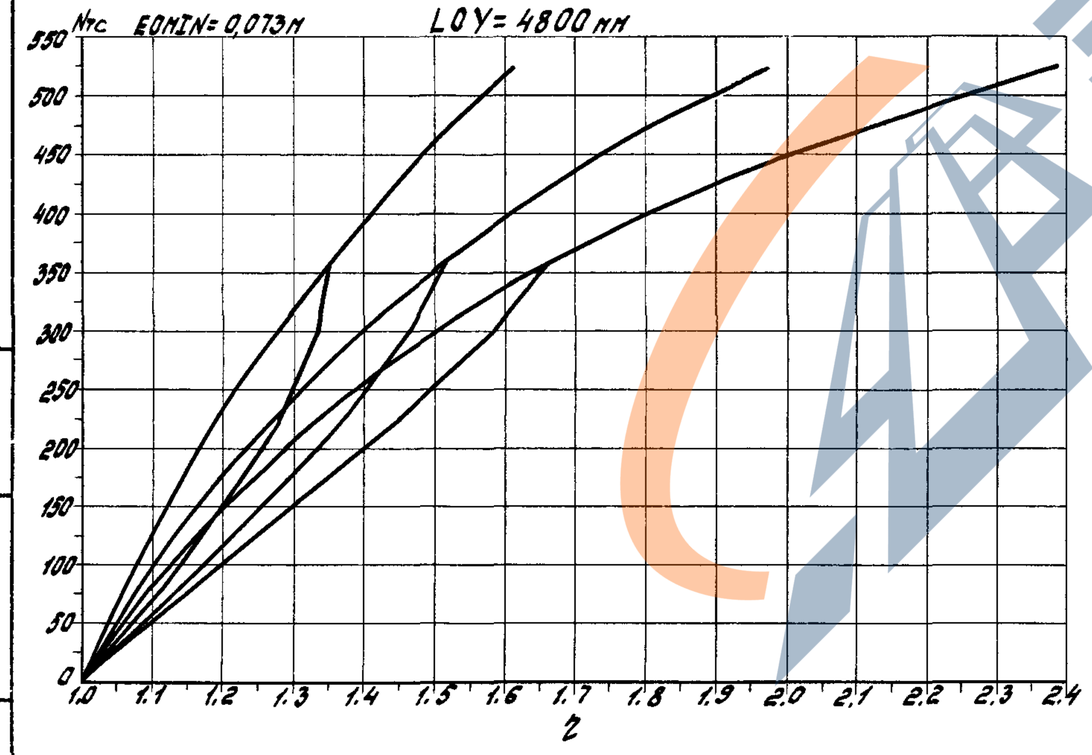
Лист 278

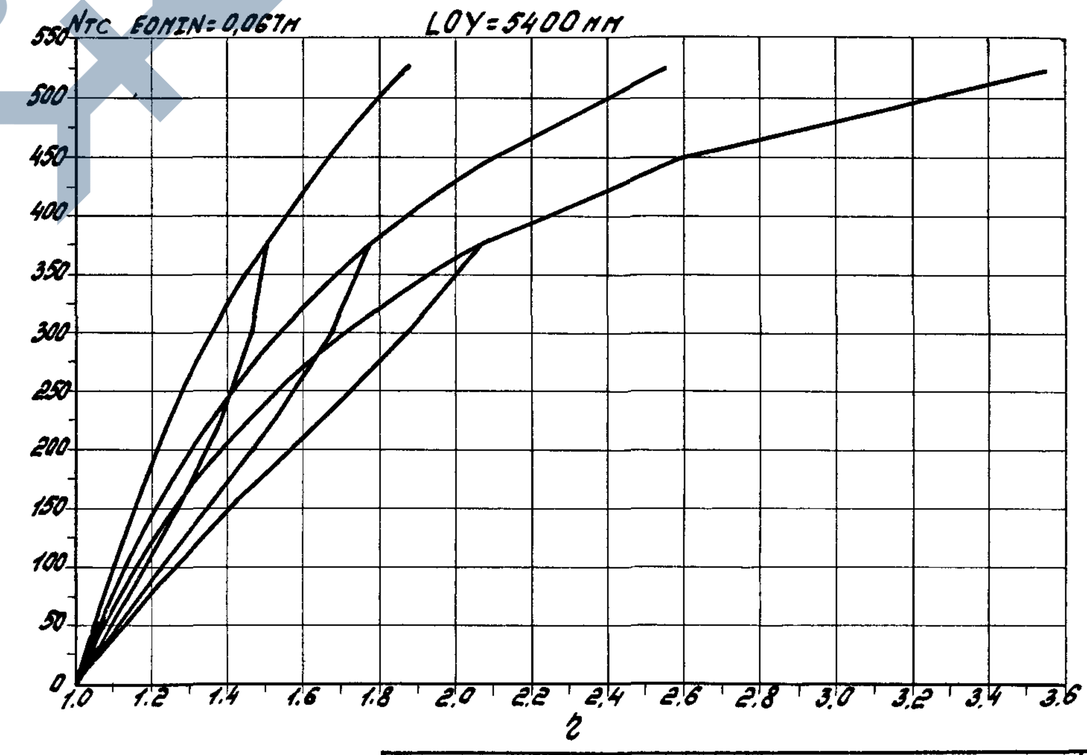
24166-03 55

https://zavodjbi.com/



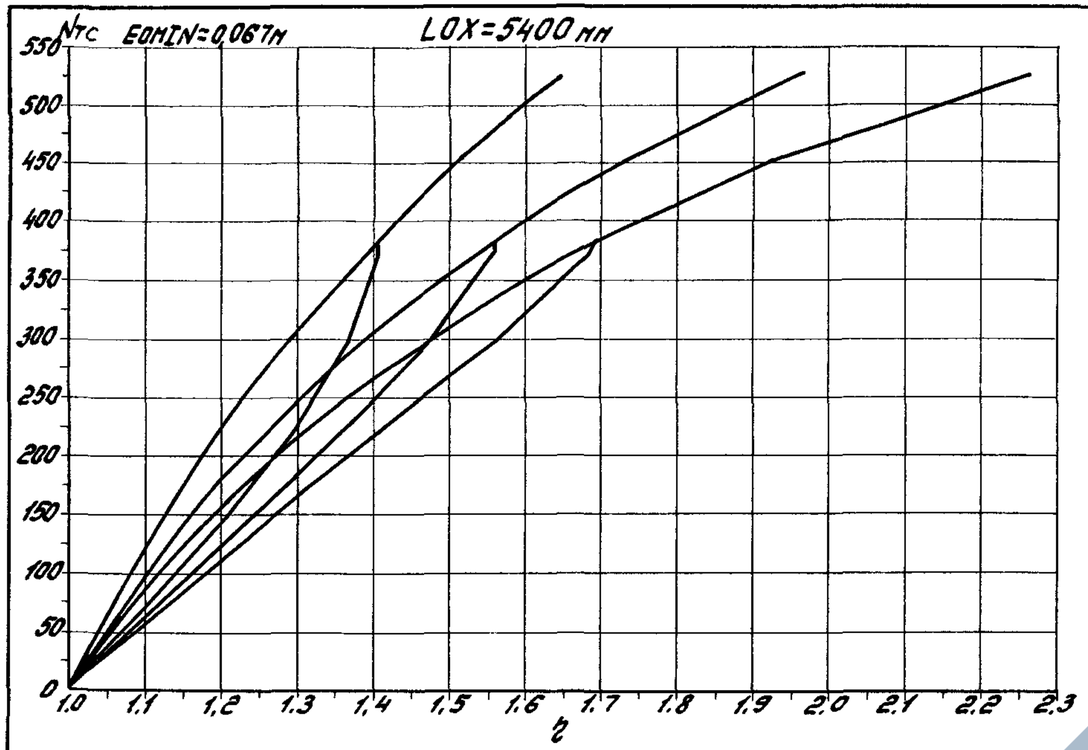


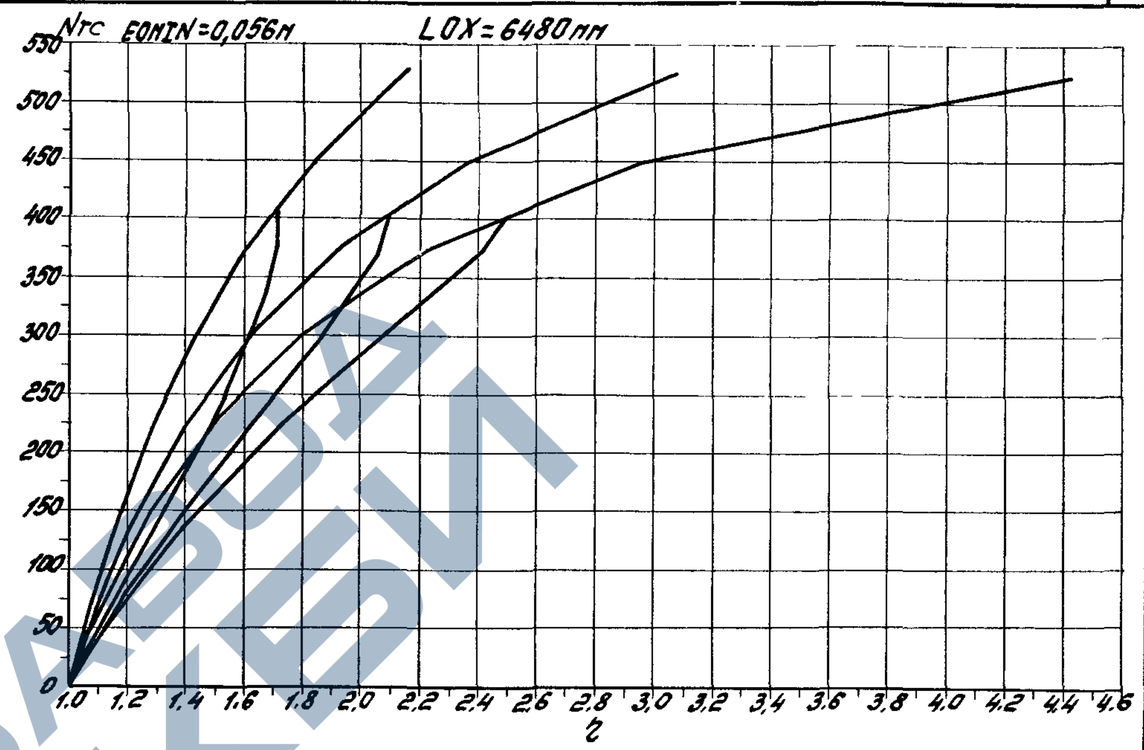


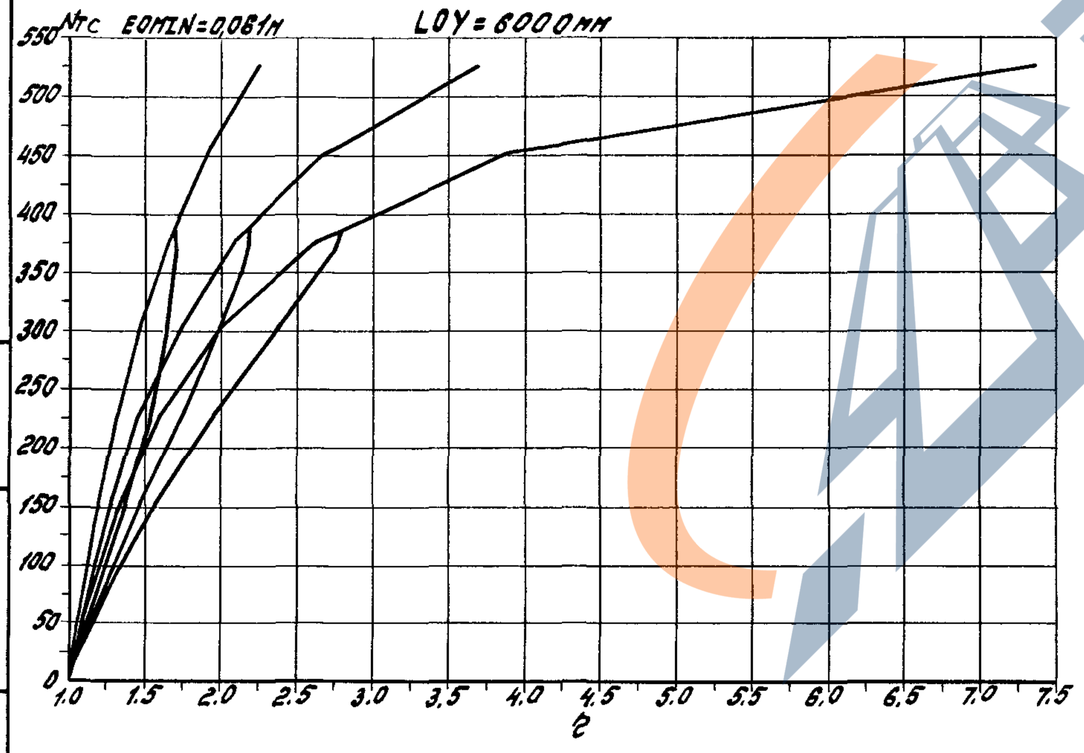


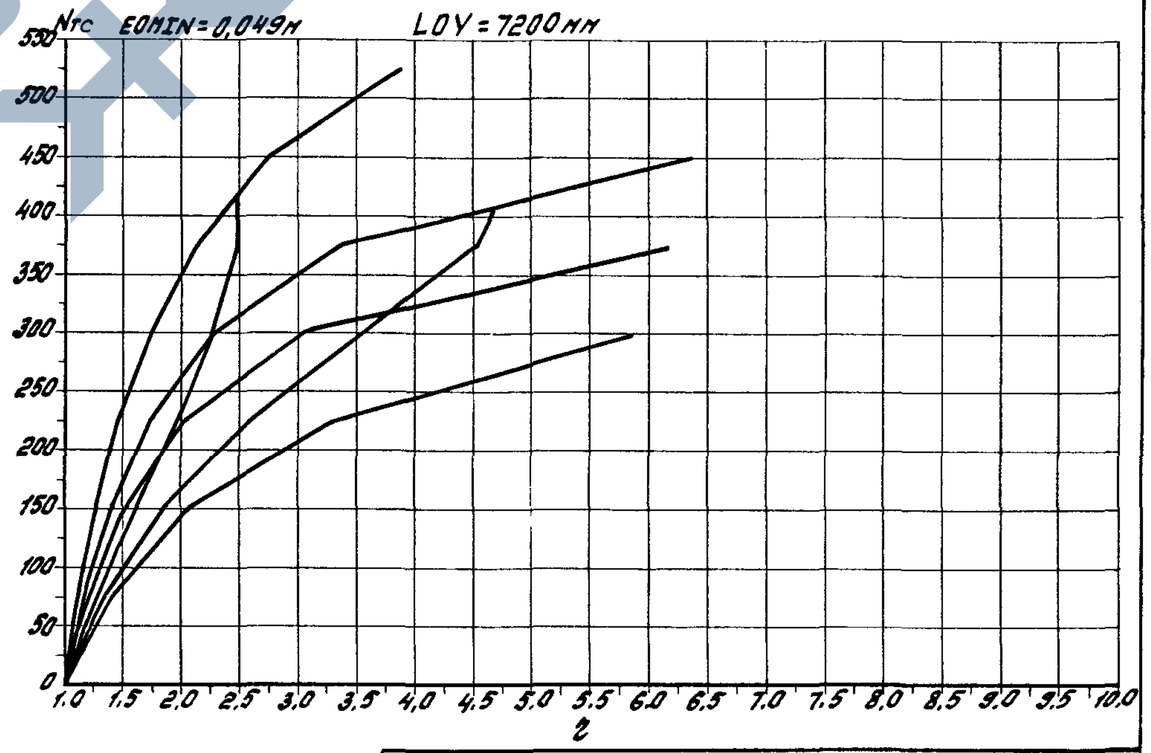
Инв.№ подл. | Подпись и дата | Взам.инв.№

https://zavodjbi.com/









Инв.№ подл. | Подпись и дата | Взам. инв.№

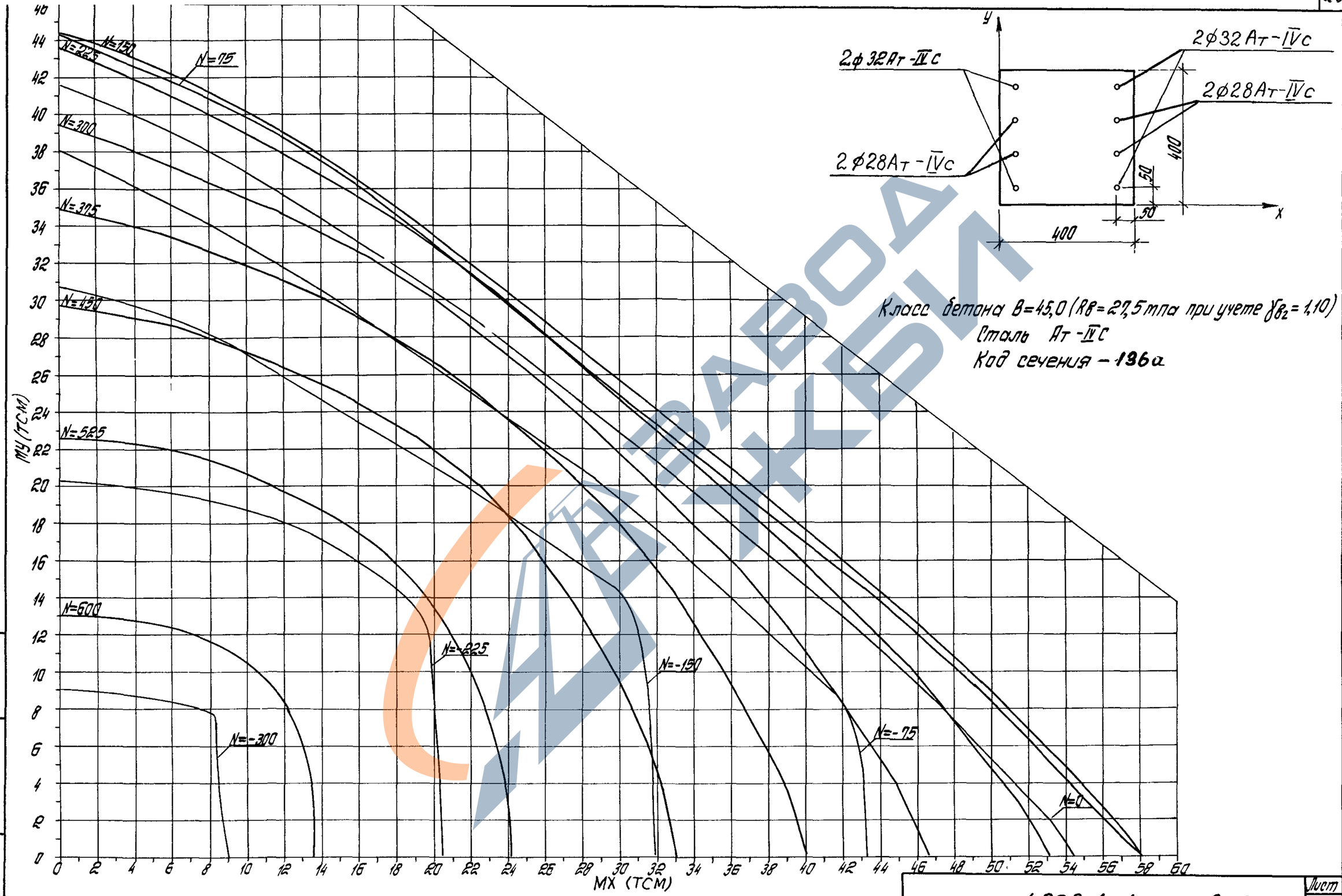
1.020.1-4 0-9 002

Лист 280

24166-03 57

https://zavodjbi.com/

https://zavodjbi.com/



Класс бетона В=45,0 (Rв=27,5 мпа при учете $\gamma_{в2}$=1,10)
Сталь Ат-IVс
Код сечения – 136а

ЗАВОДА ЖБИ

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4 0-9 002 | Лист 281

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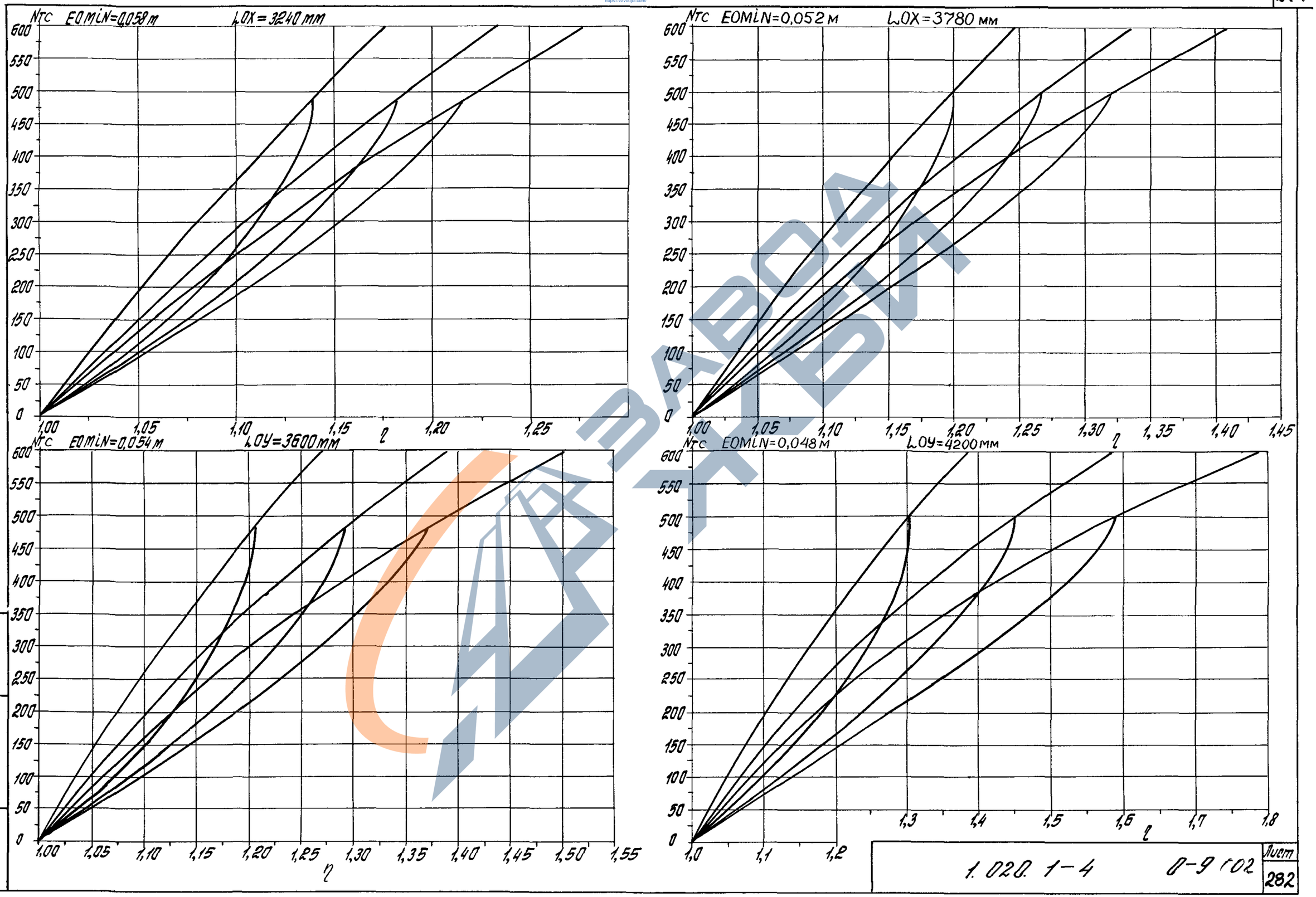
https://zavodjbi.com/



1.020.1-4 0-9 ГОД

Лист 282

24166-03 59

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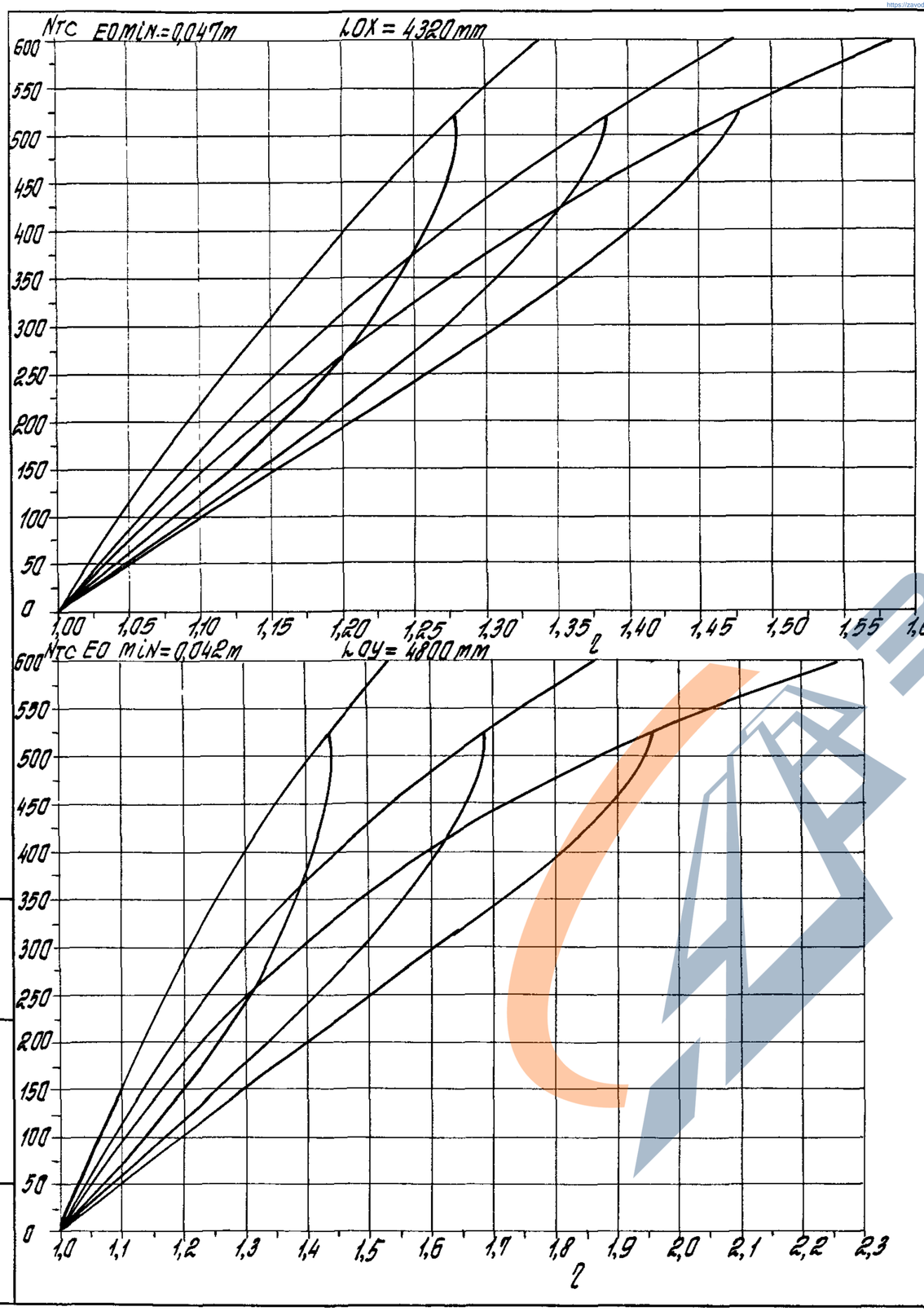

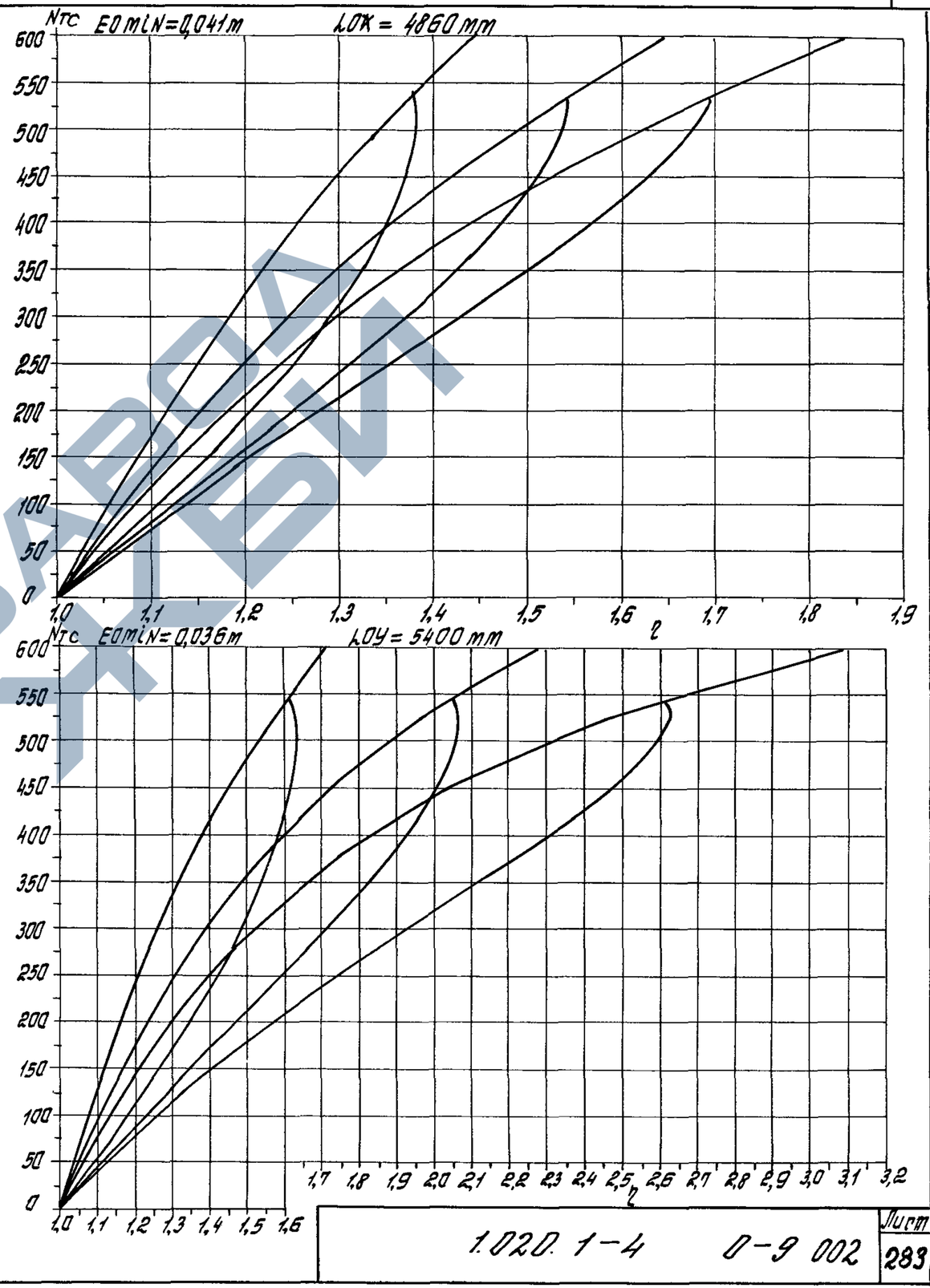

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4 0-9 002

Лист 283

24166-03 60

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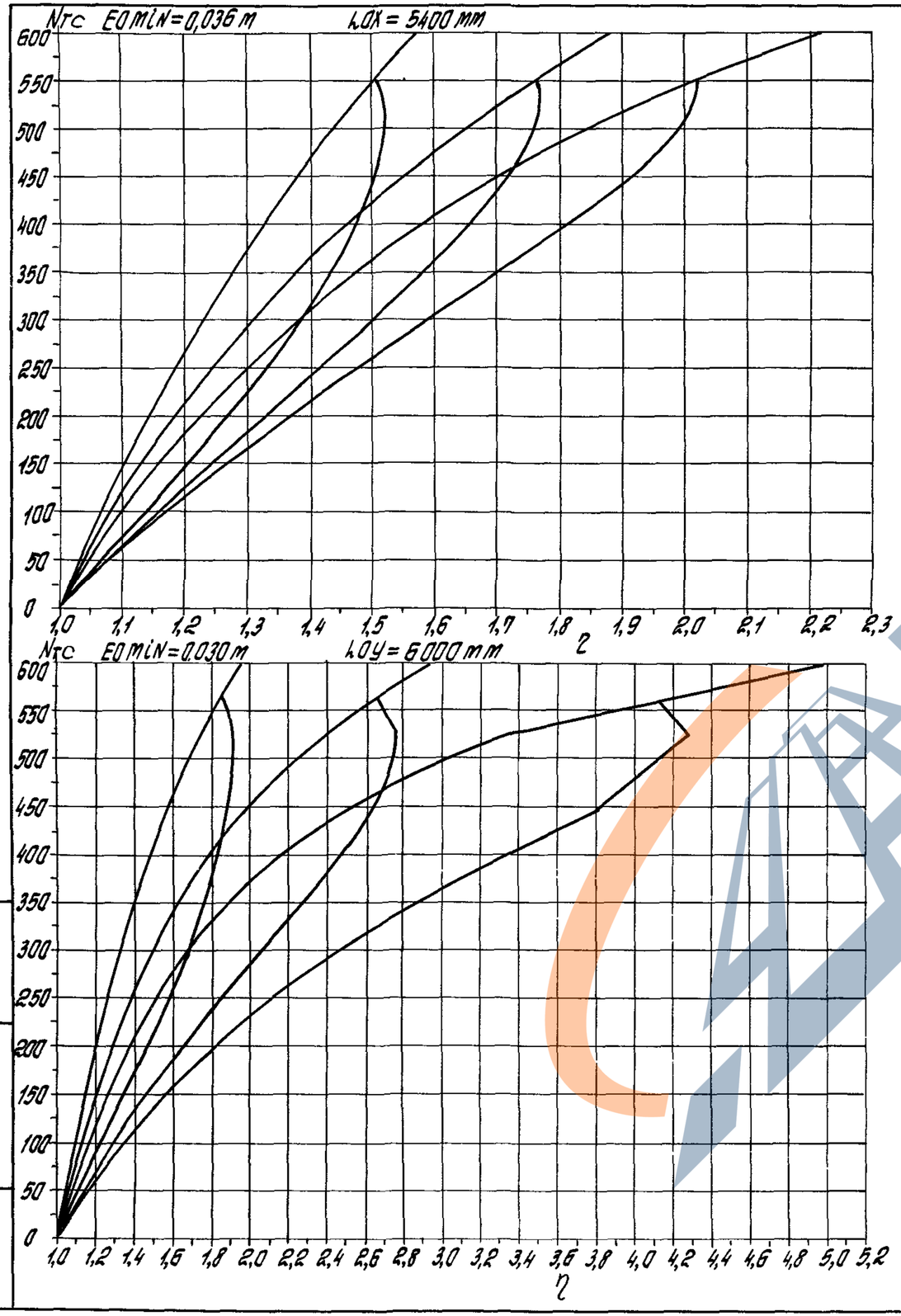
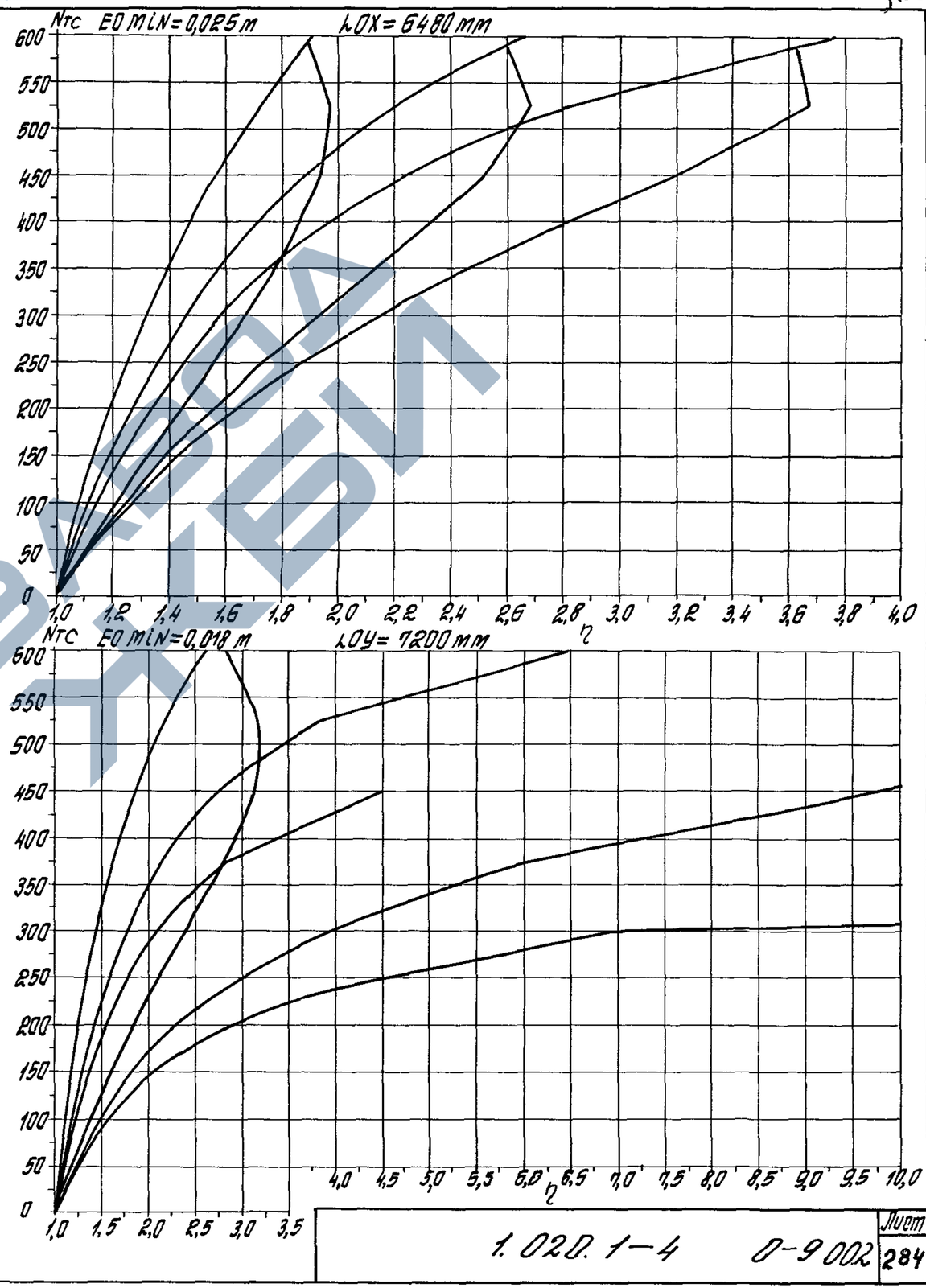
https://zavodjbi.com/





Инв. № подл. | Подпись и дата | Взам. инв. №

1.020.1-4 0-9002

Лист 284

24166-03 61

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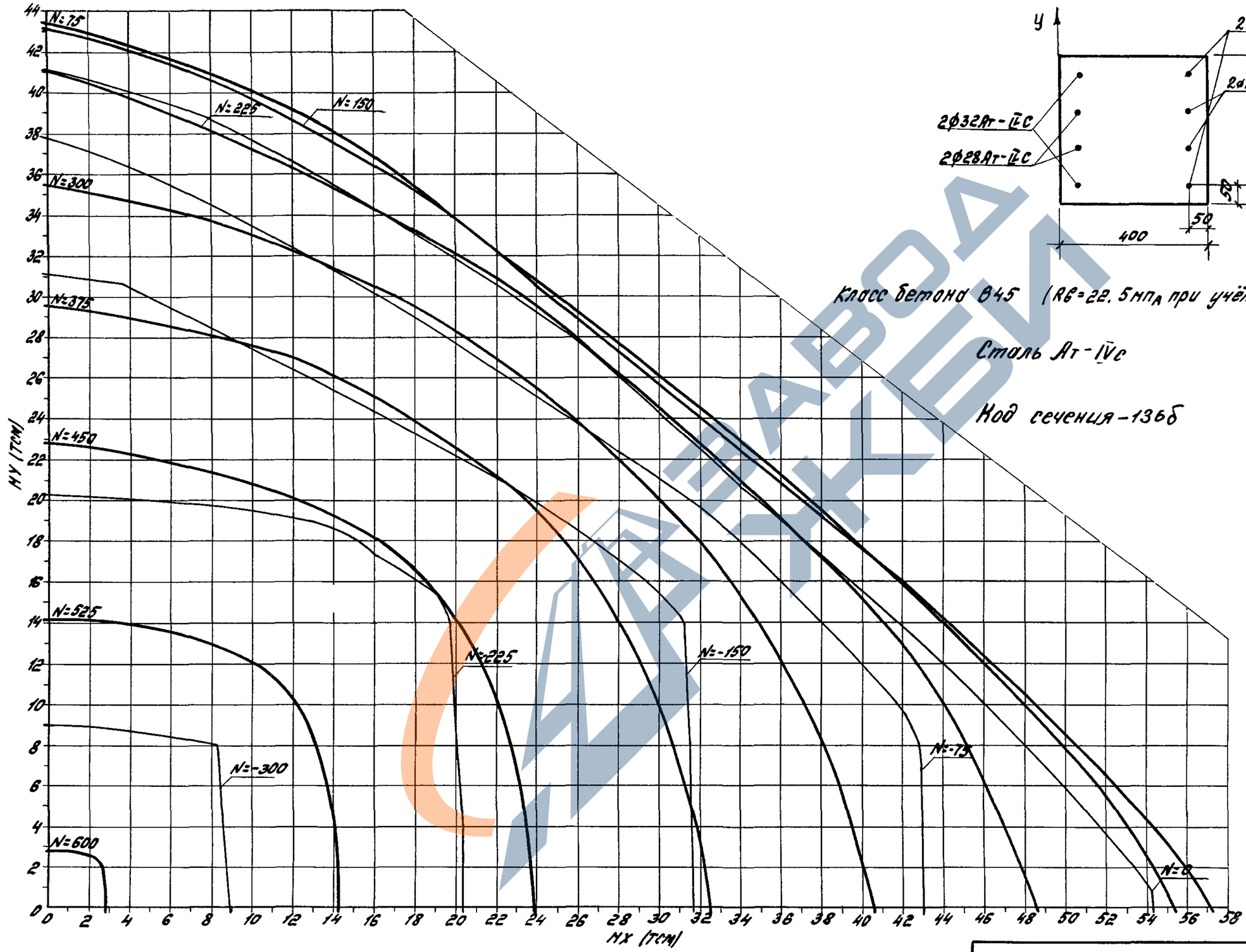

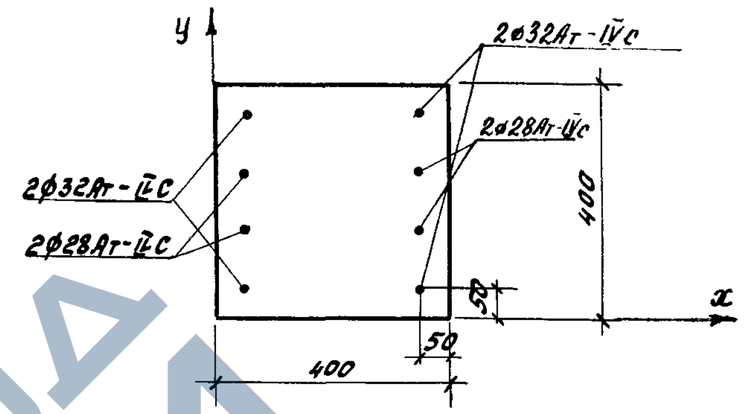

Класс бетона В45 (Rв=22.5 МПа при учёте γ_{B_2} = 0.90)

Сталь Ат-IVс

Код сечения-136б

Инв.№ подл.	Подпись и дата	Взам. инв.№		

24166-03 62

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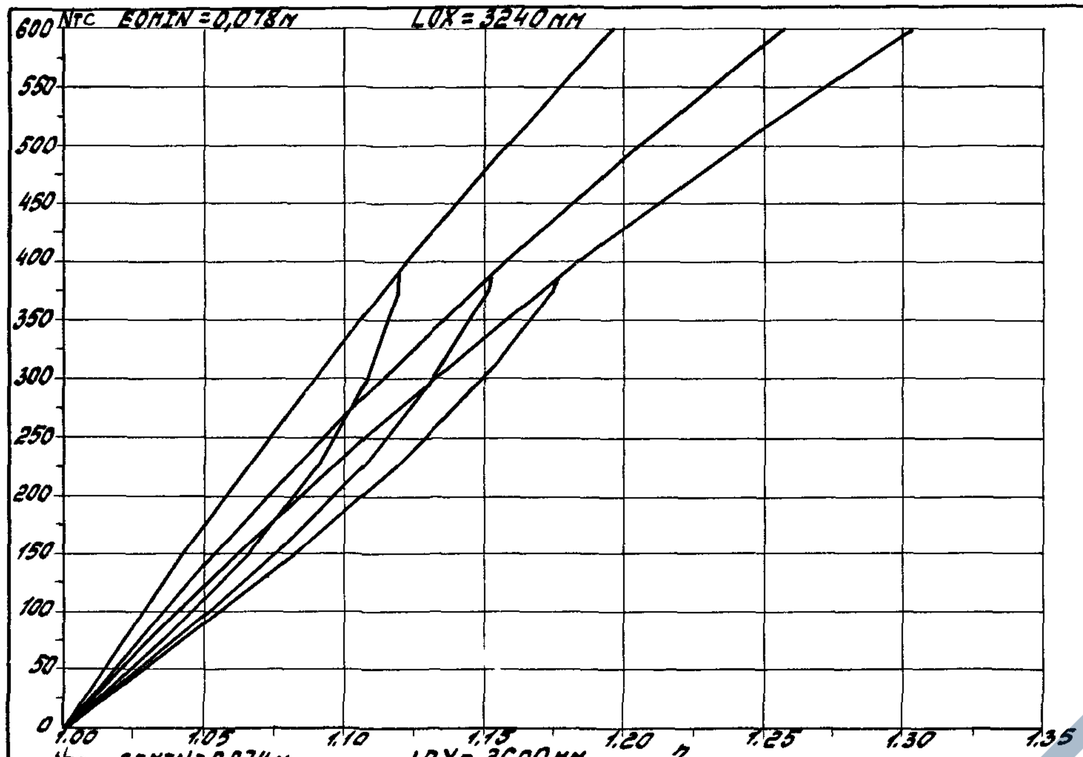

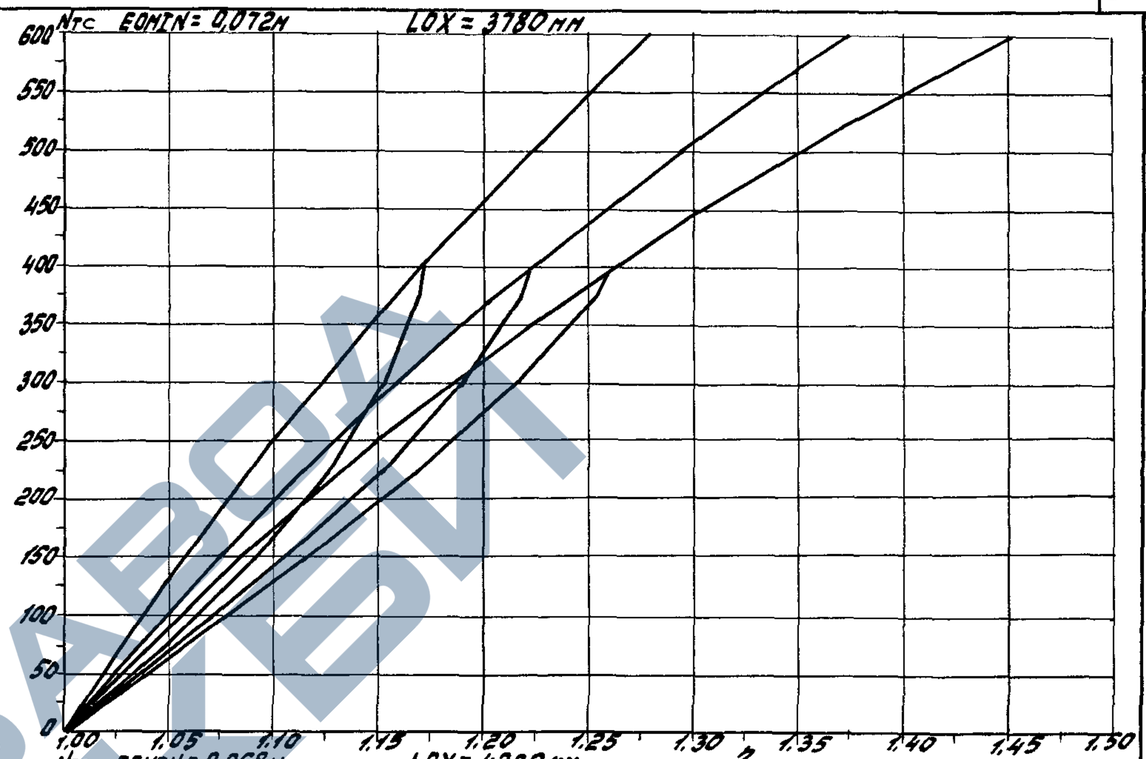

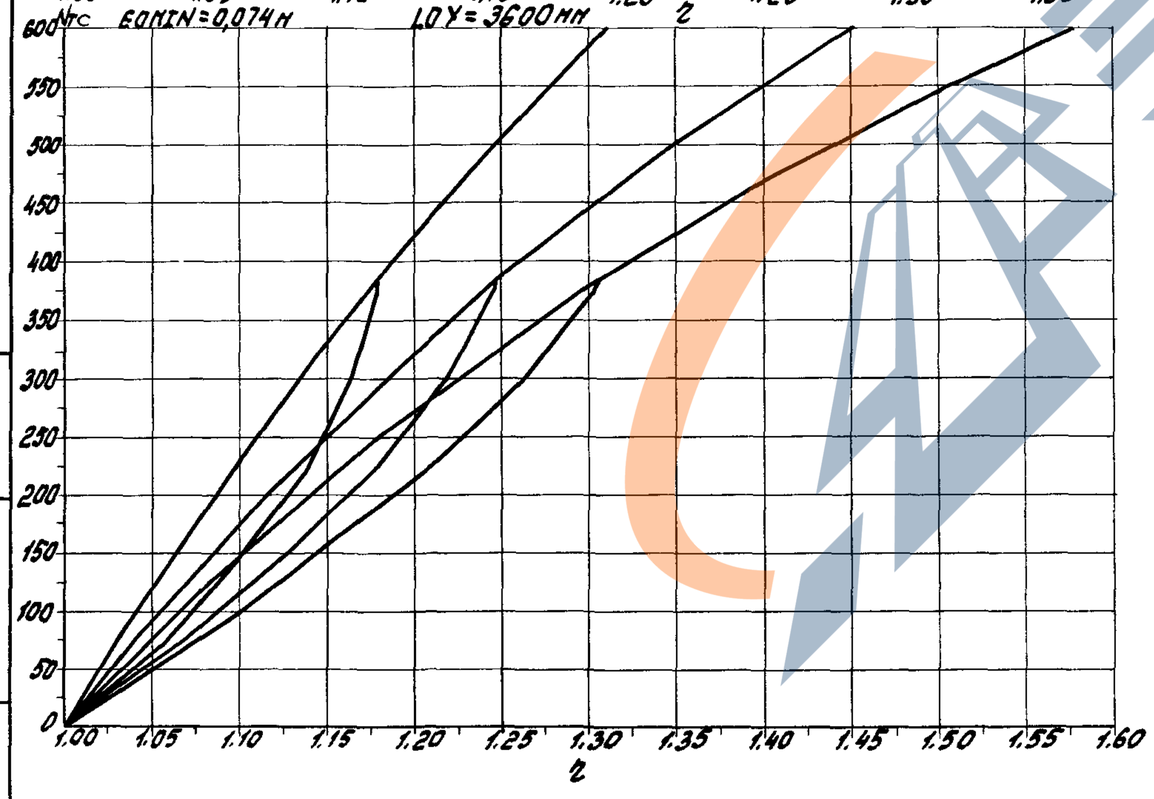

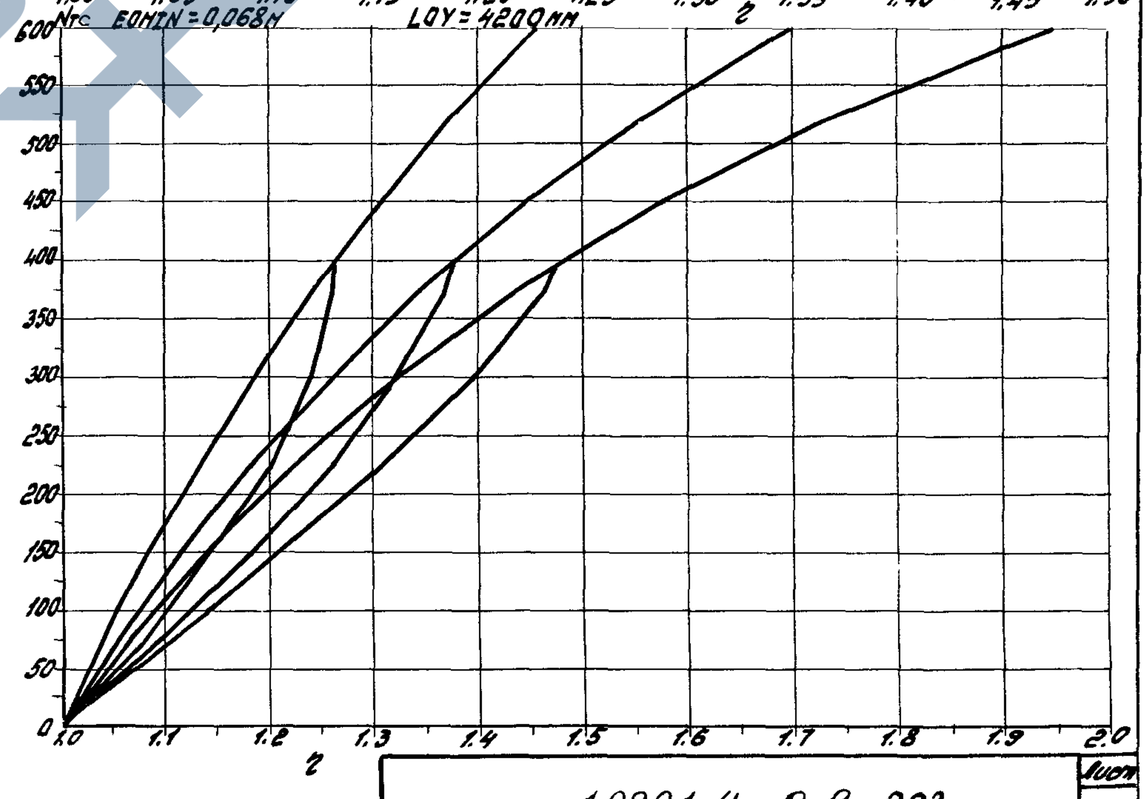

Инв.№ подл. | Подпись и дата | Взам. инв.№

1.020.1-4 0-9 002

Лист 286

24166-03 63

https://zavodjbi.com/

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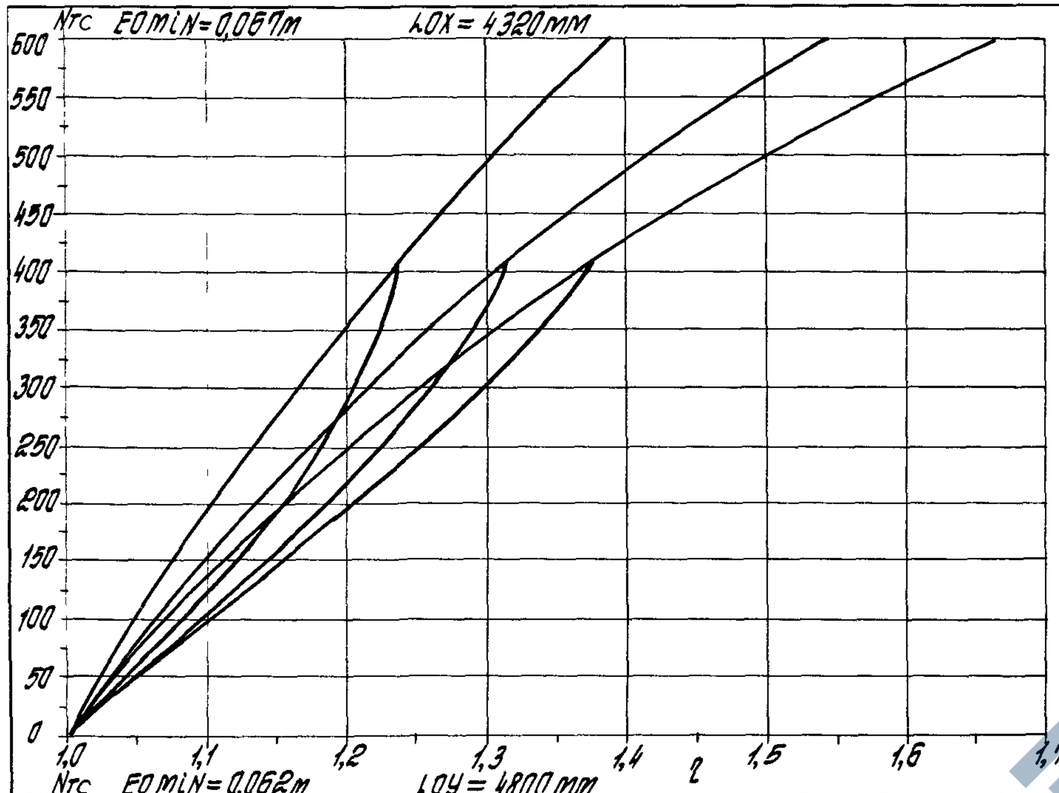
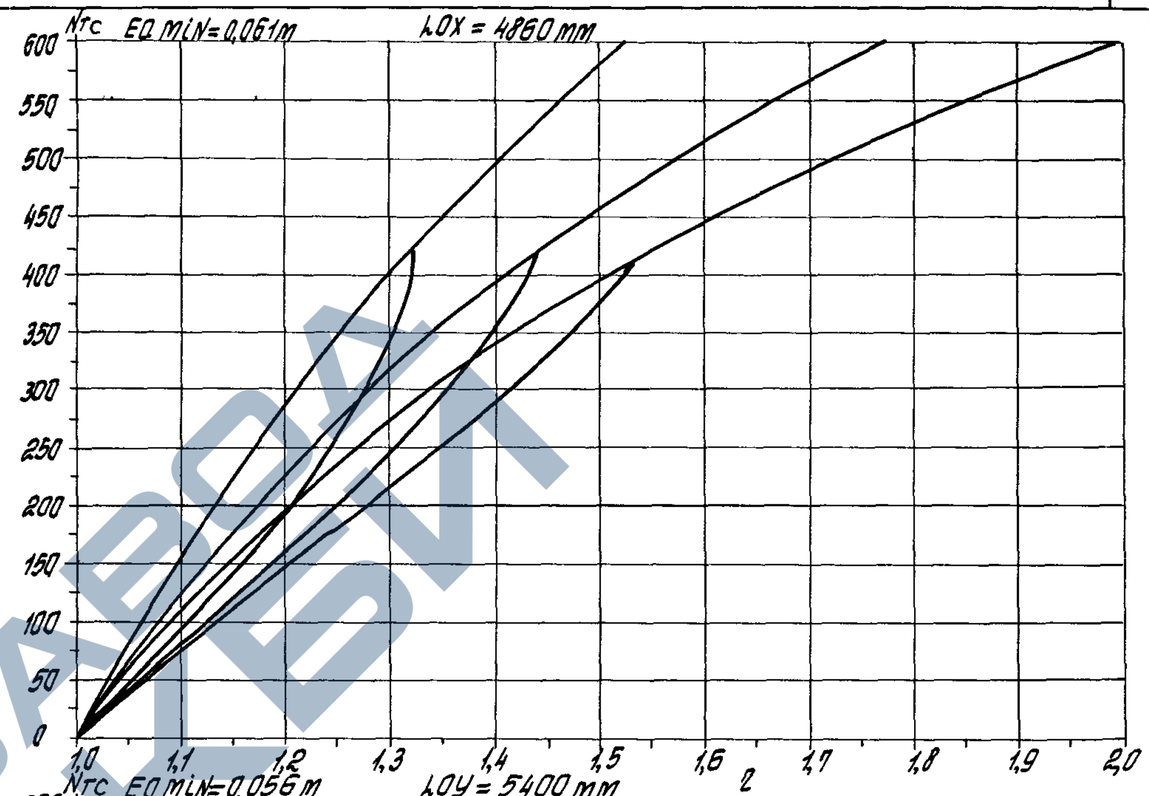
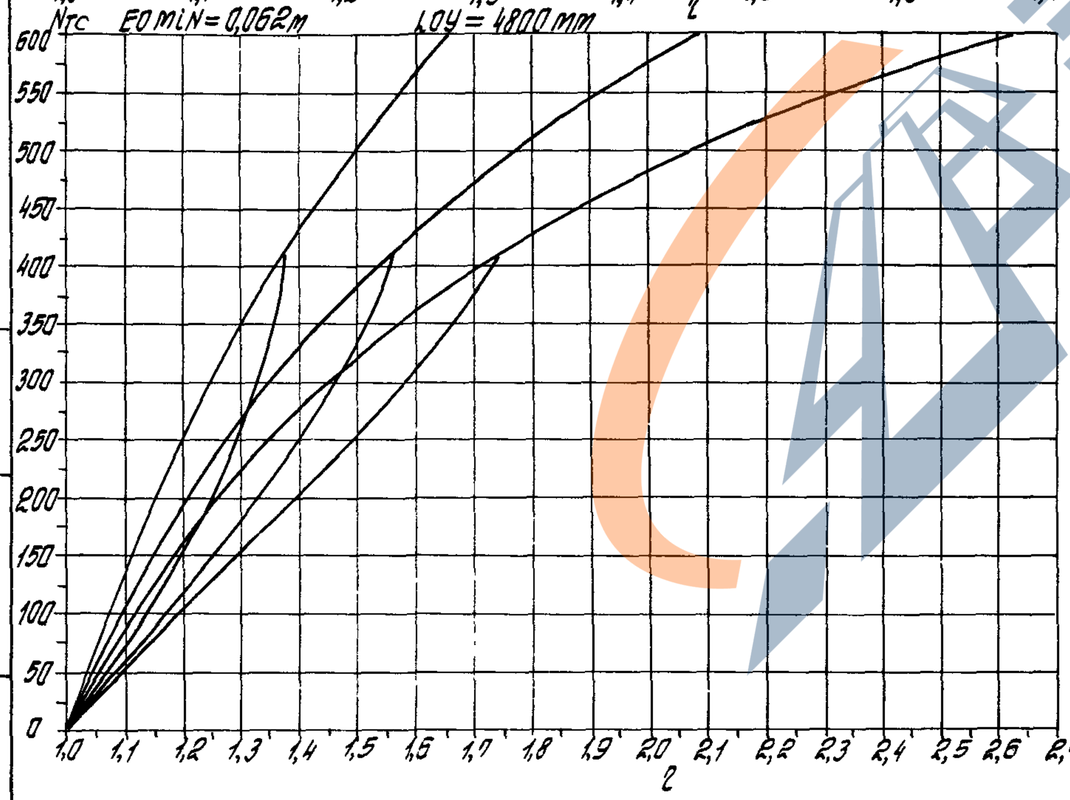
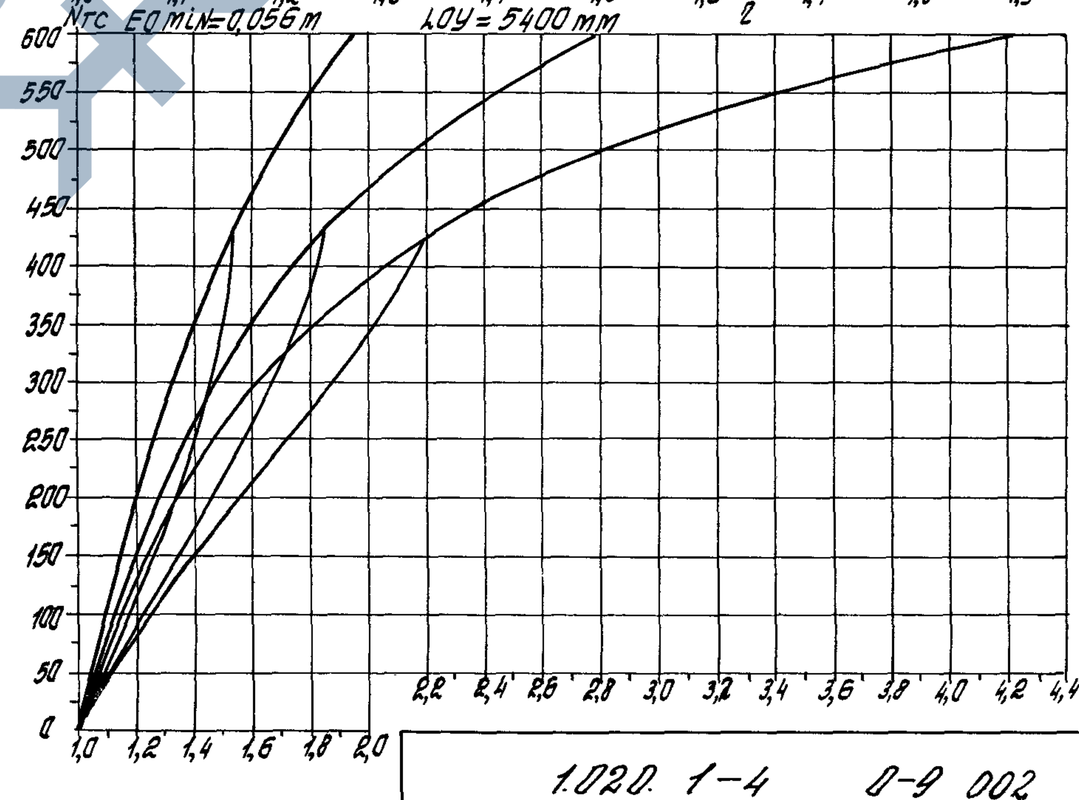






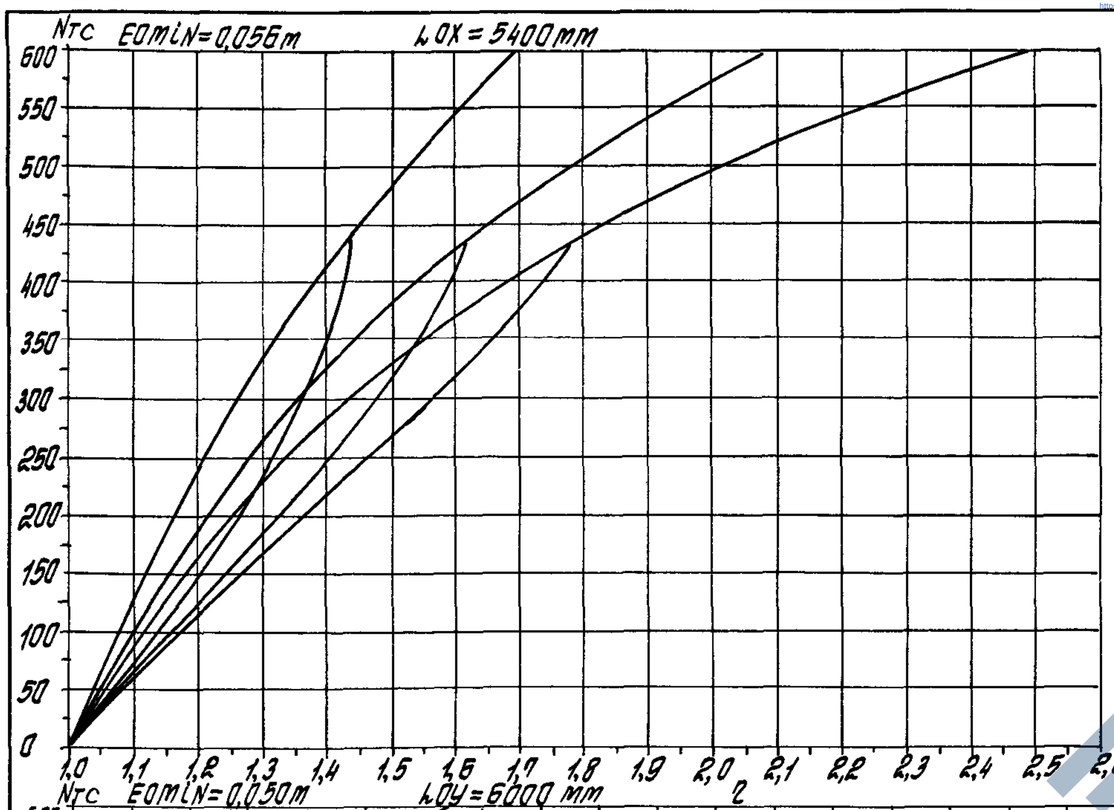


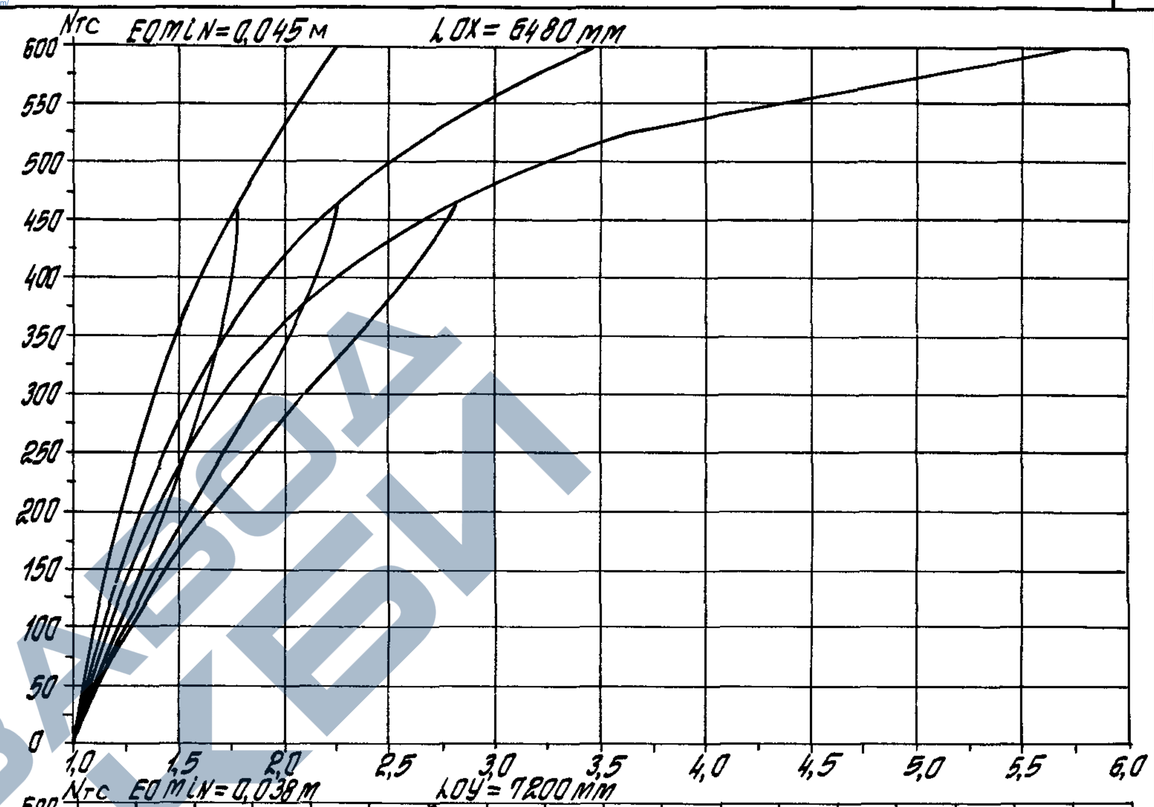
Инв.№ подл. | Подпись и дата | Взам. инв.№

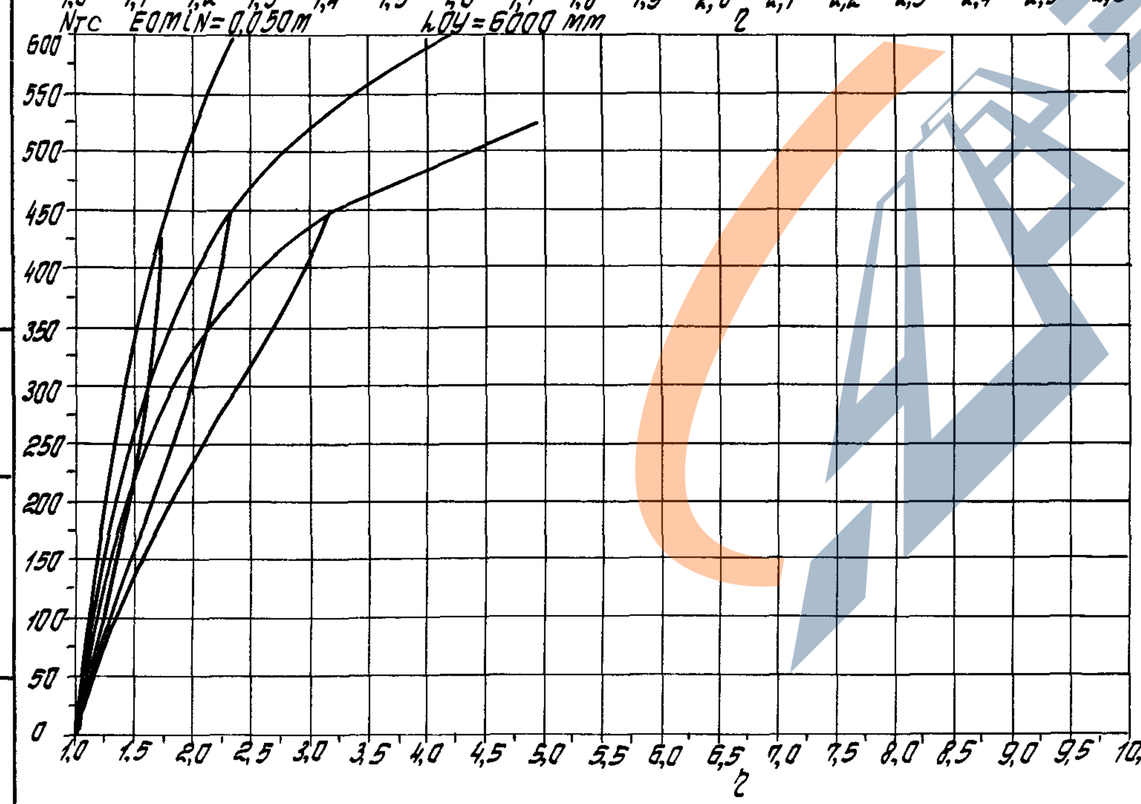
1.020.1-4 0-9 002

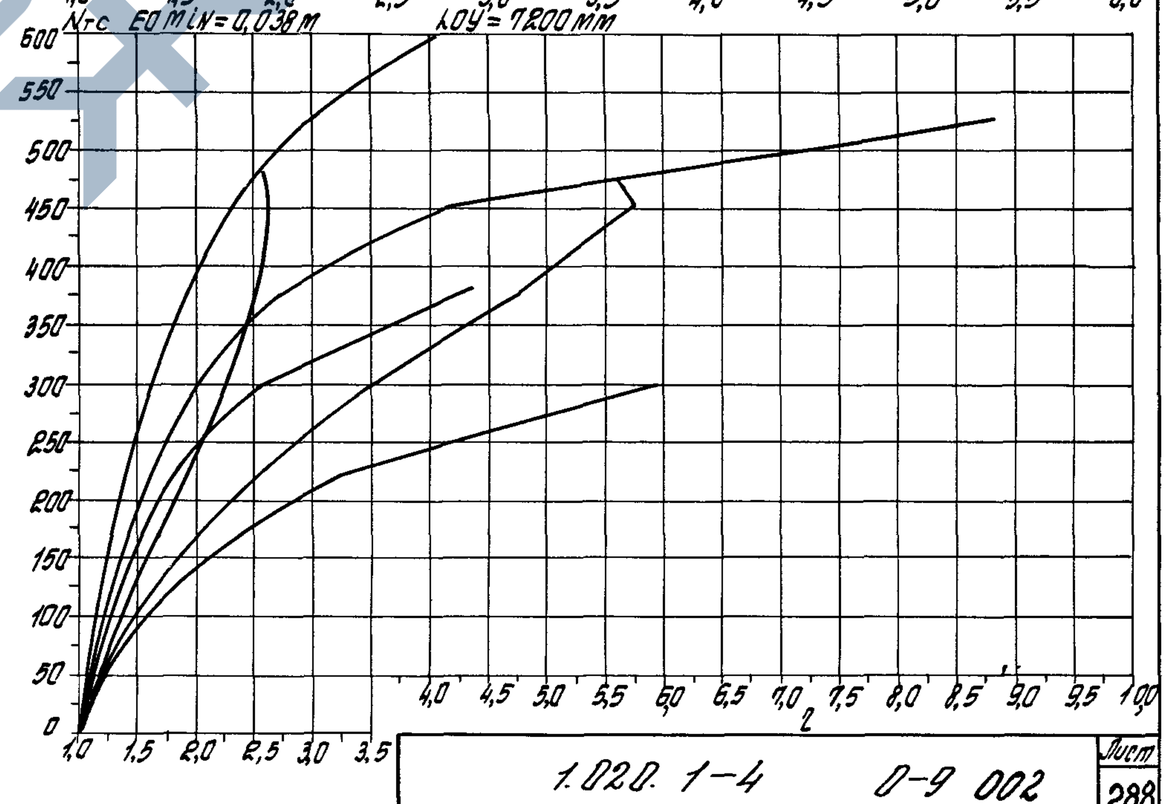
Лист 287

https://zavodjbi.com/









Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4 0-9 002

Лист 288

24166-05 65

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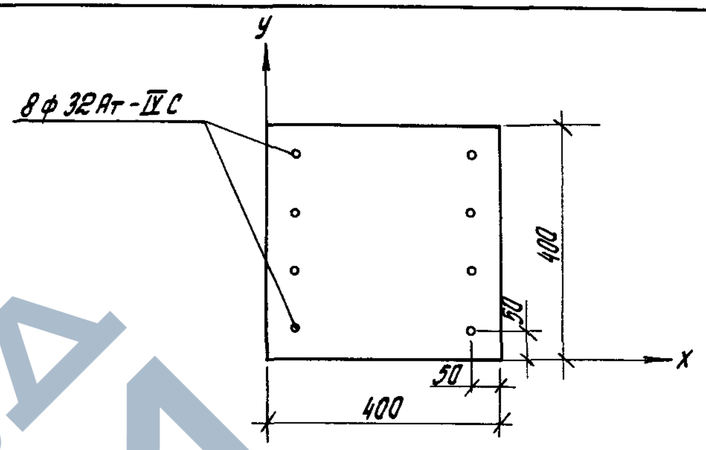
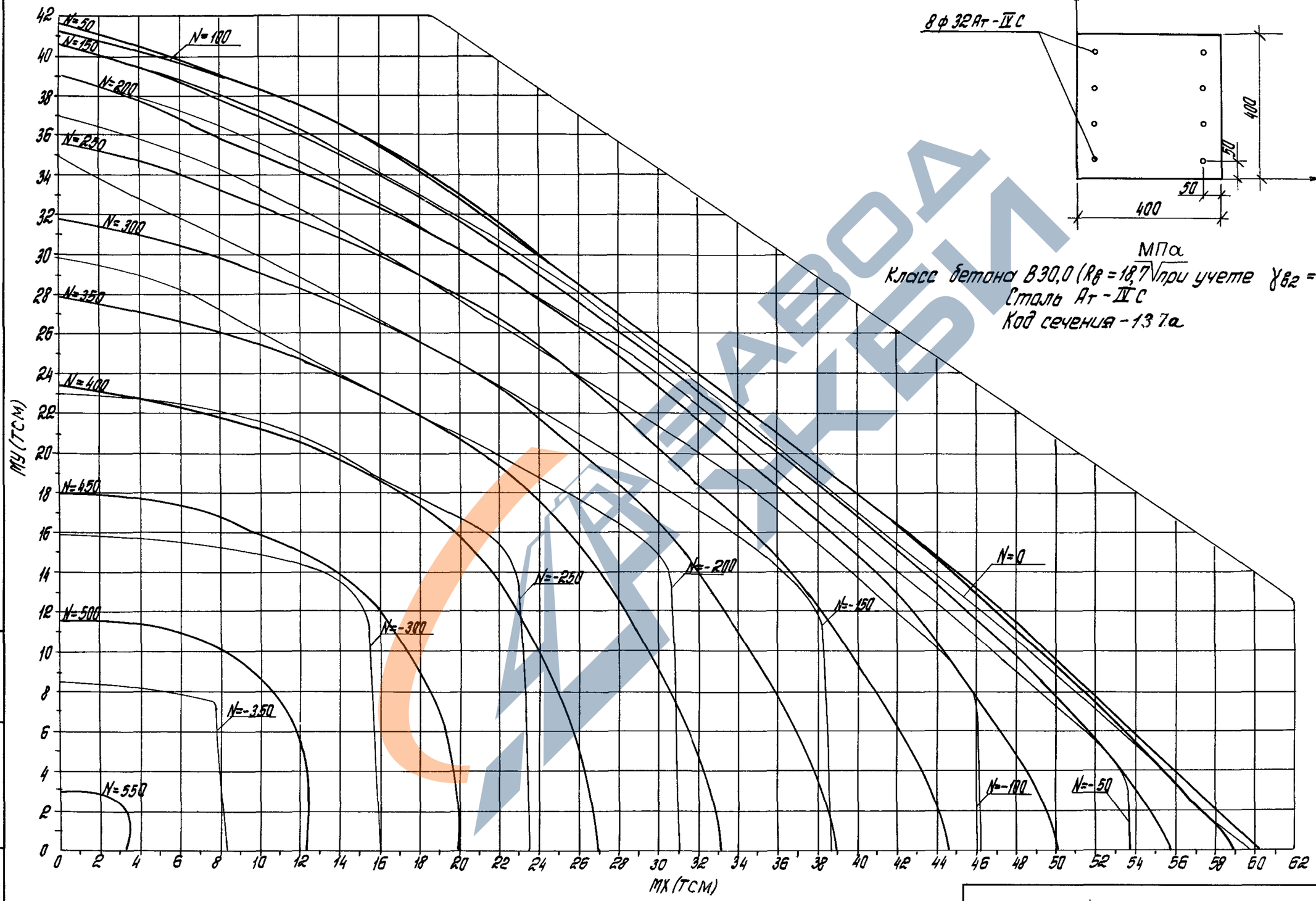


МПа

Класс бетона В30,0 ($R_в = 18,7\sqrt{}$ при учете $\gamma_{в2} = 1,10$)

Сталь Ат-IVС

Код сечения - 137а



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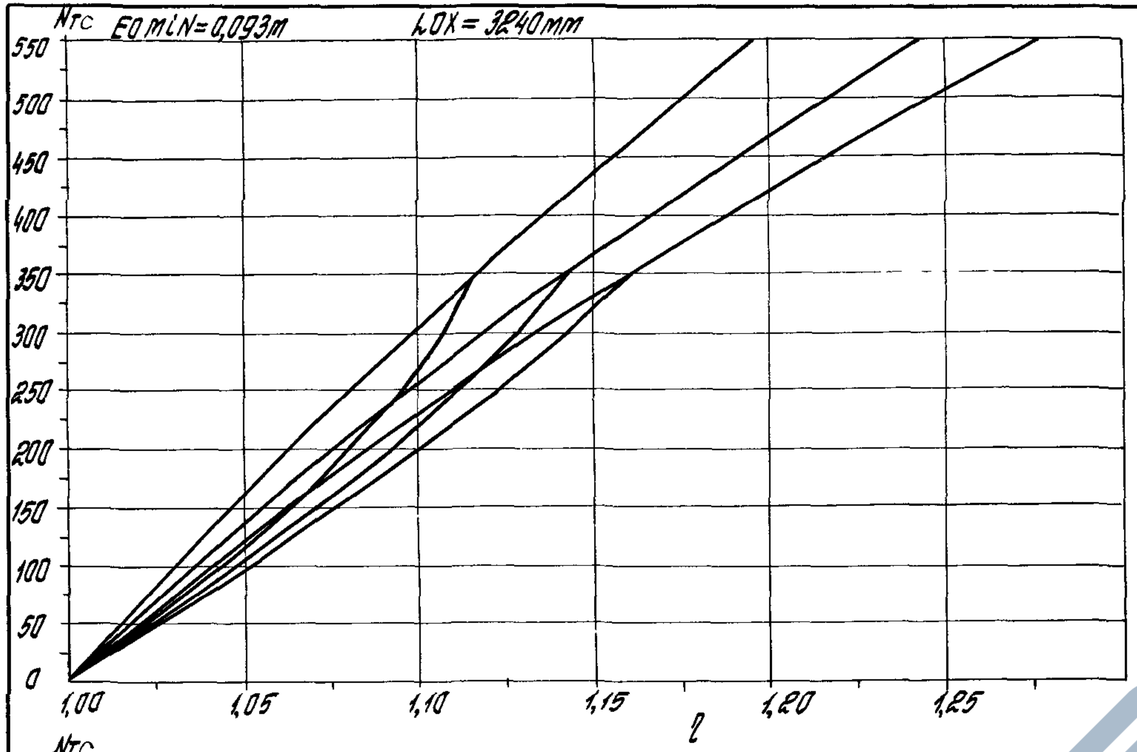

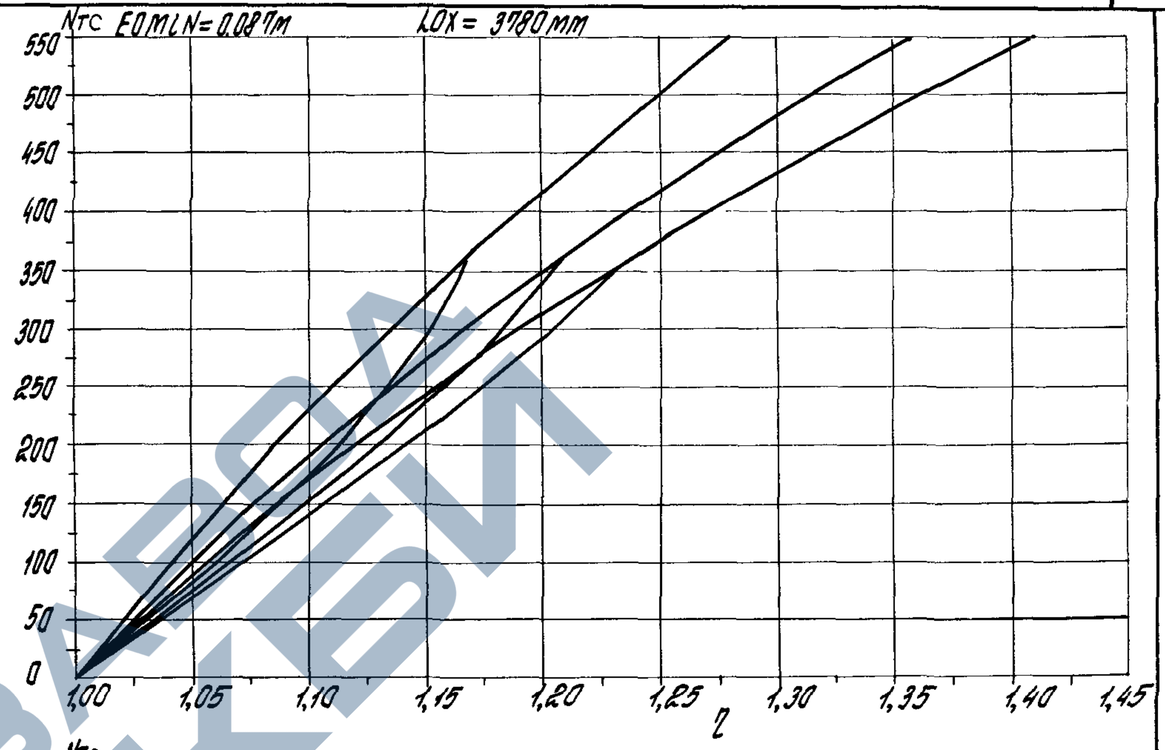

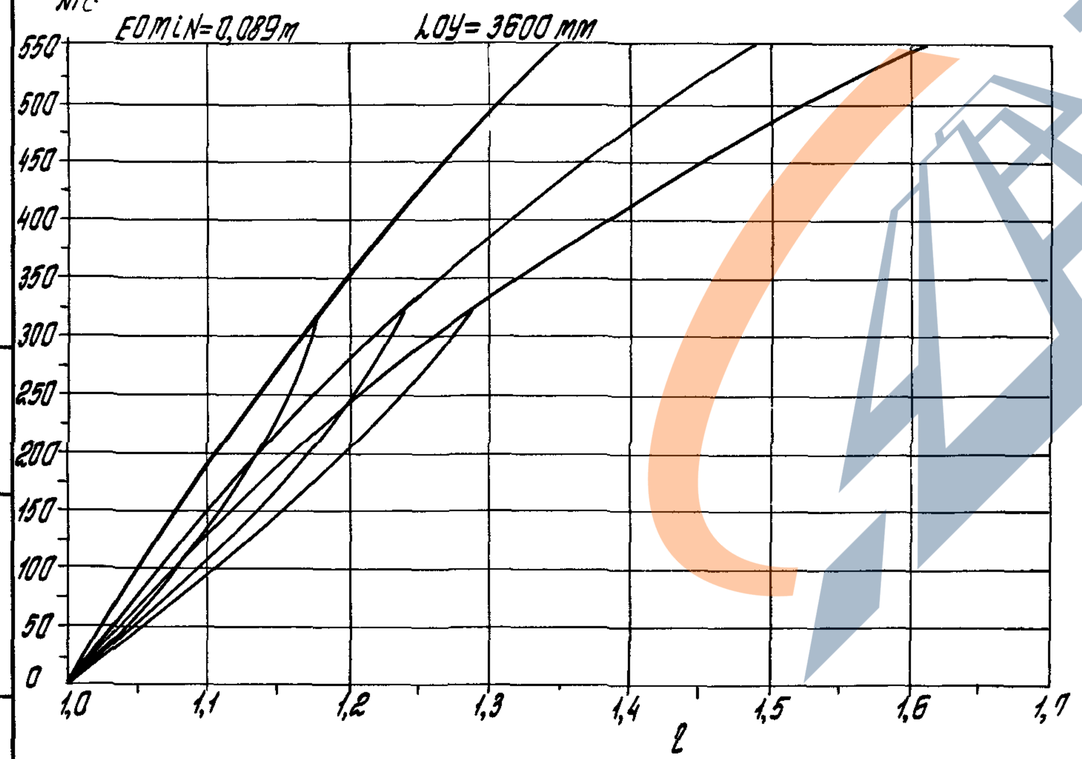

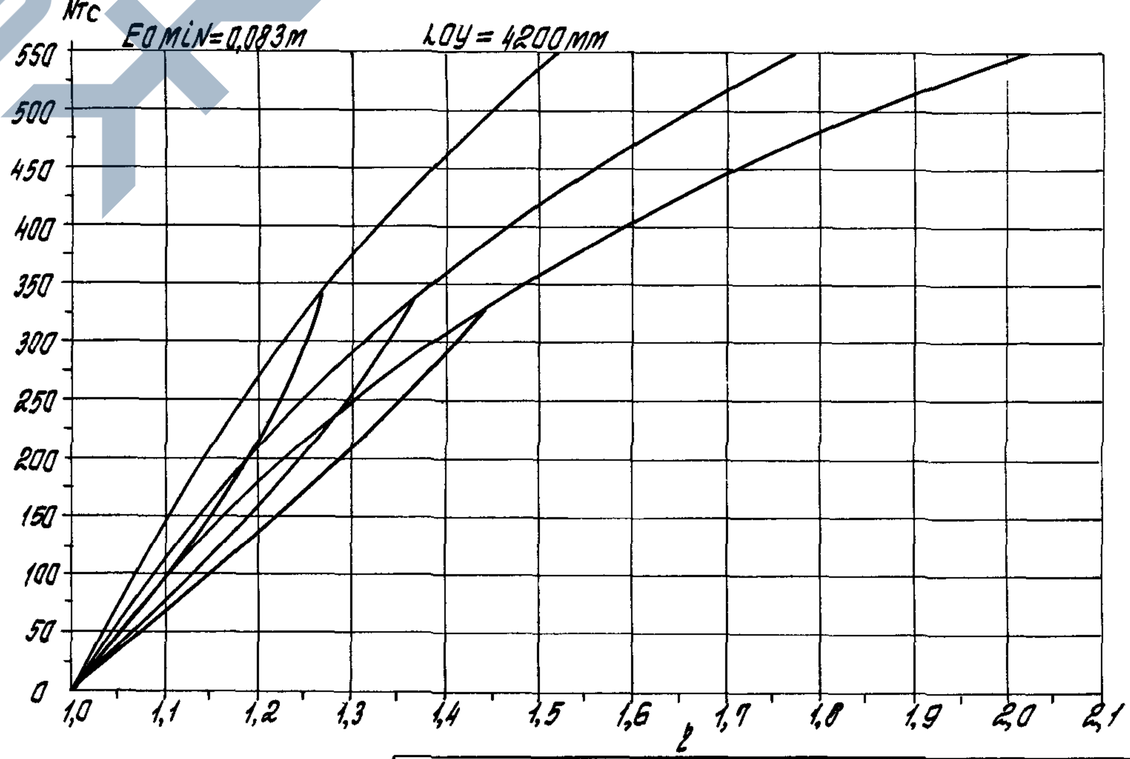

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4 0-900	Лист 290

24166-03 67

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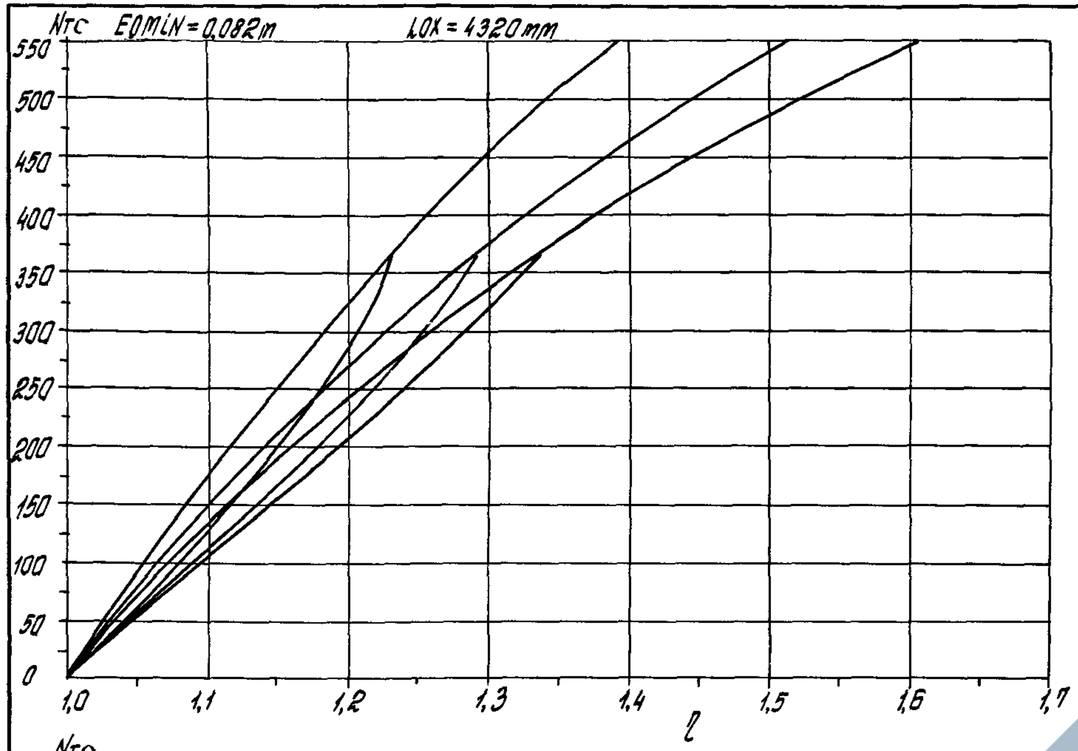

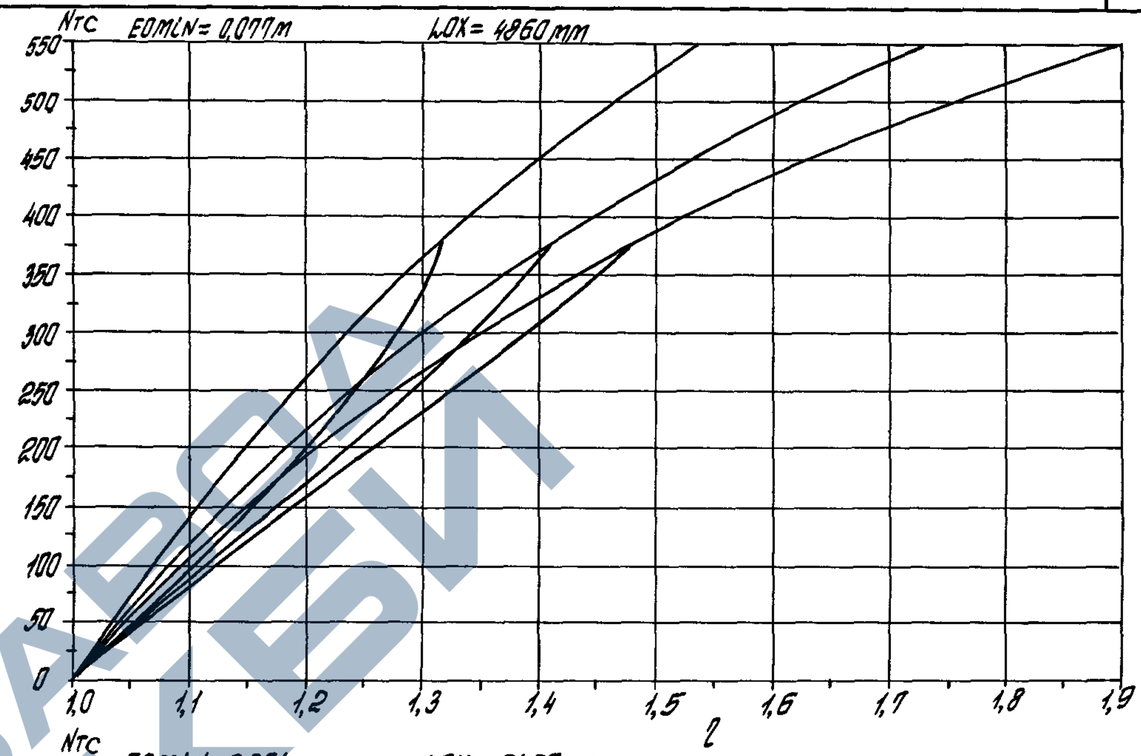

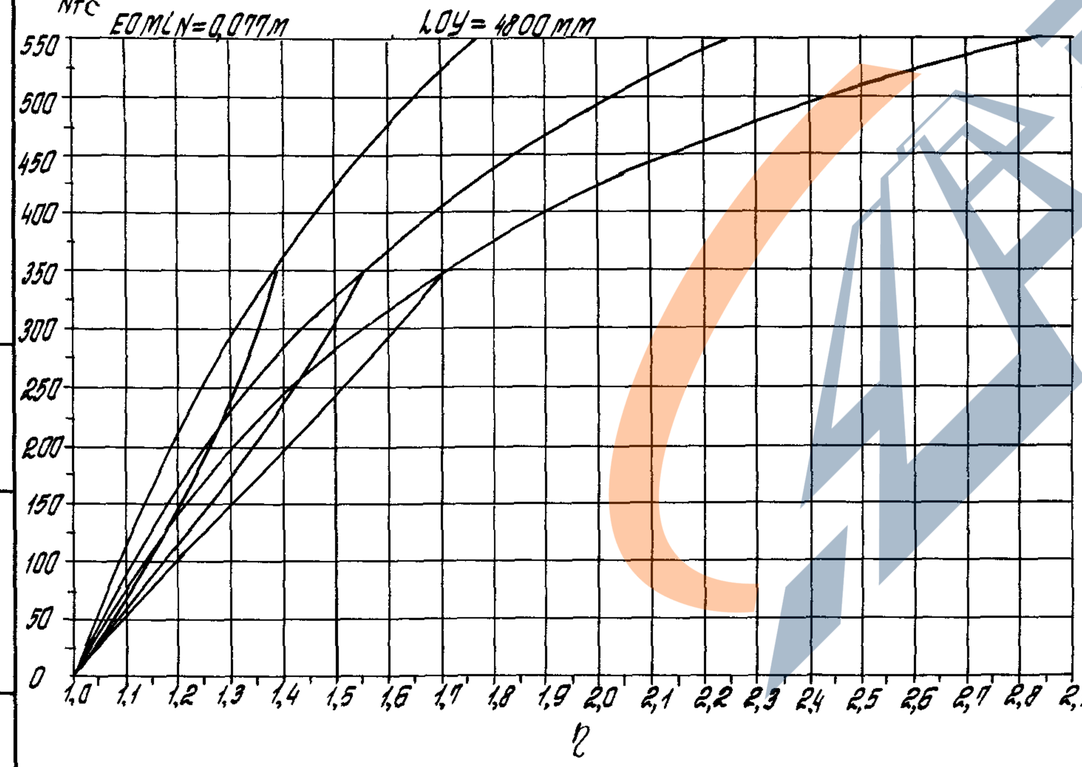

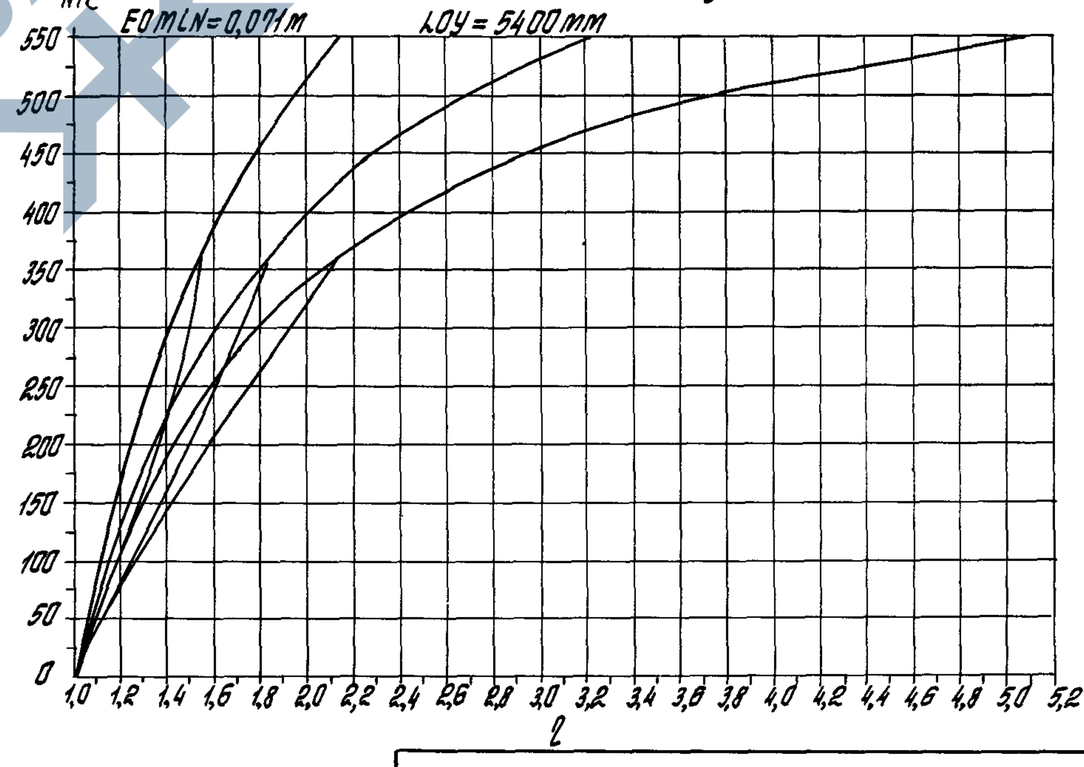

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4 0-9 002

Лист 291

24166-03 68

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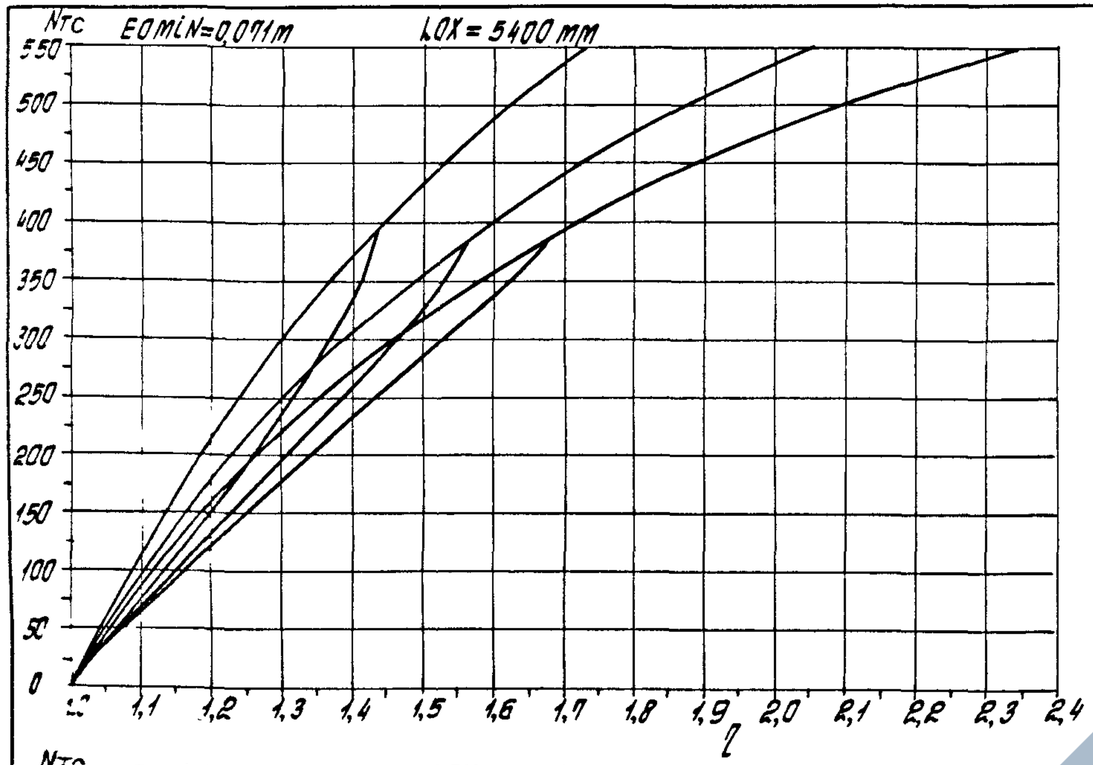
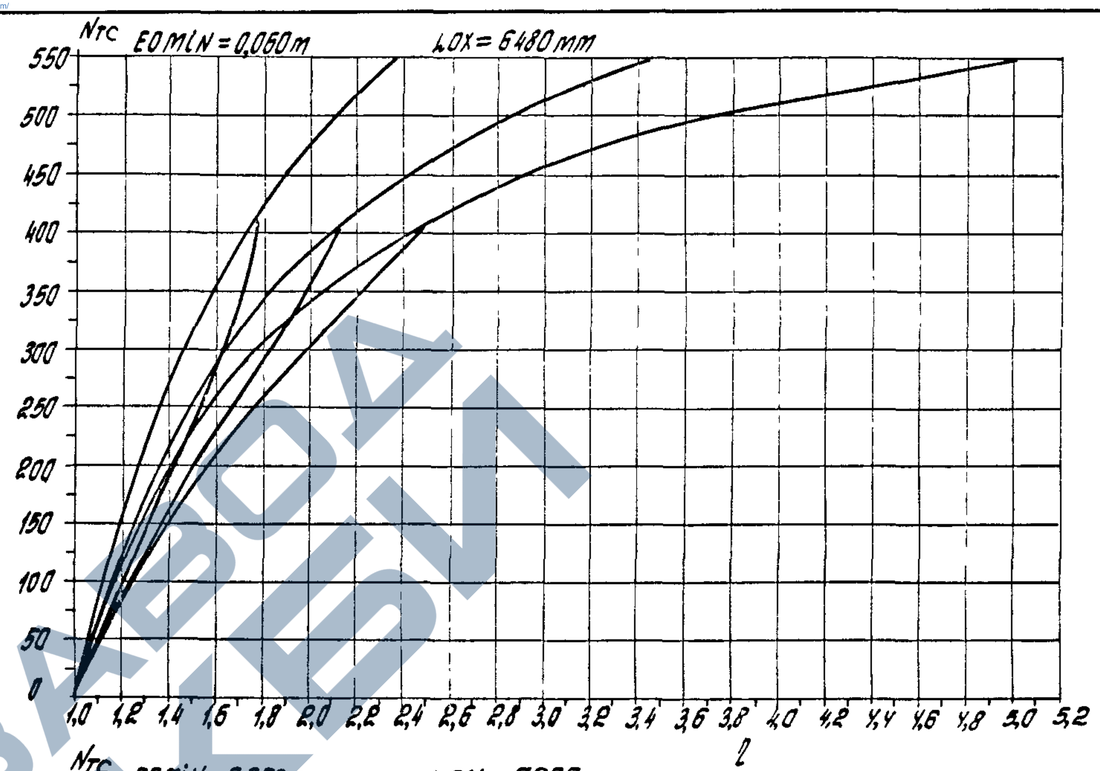
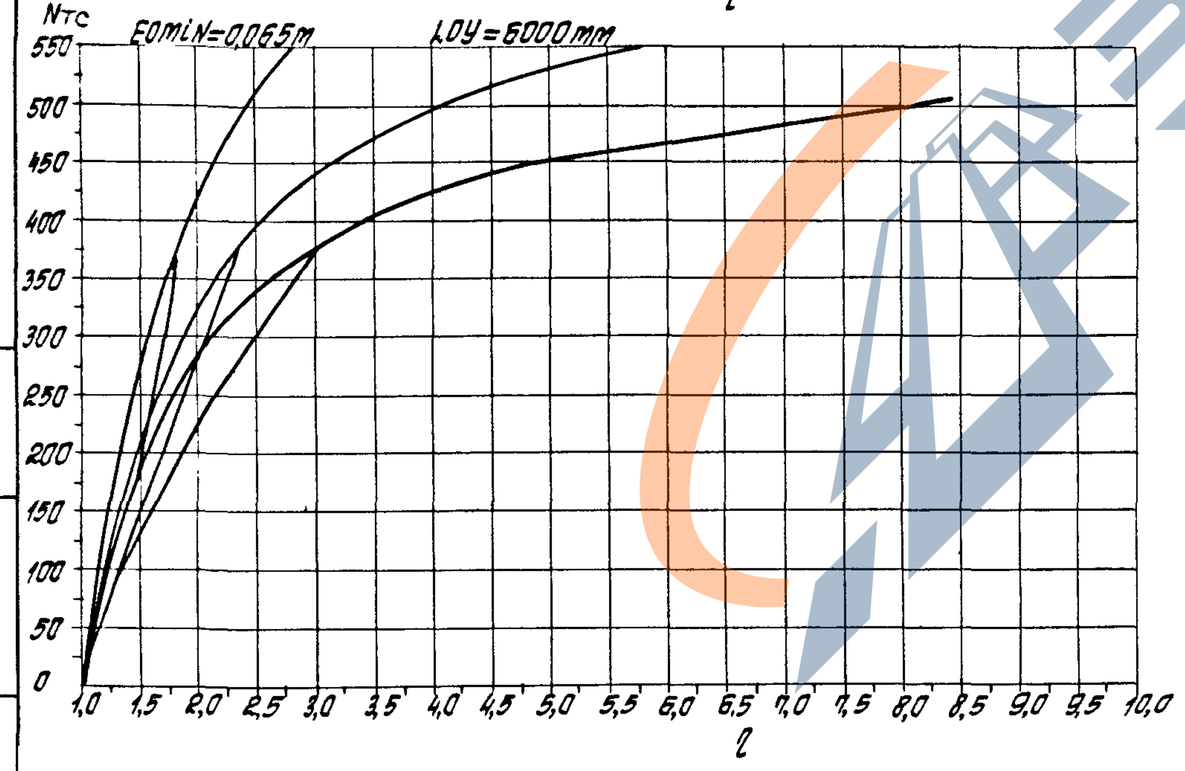
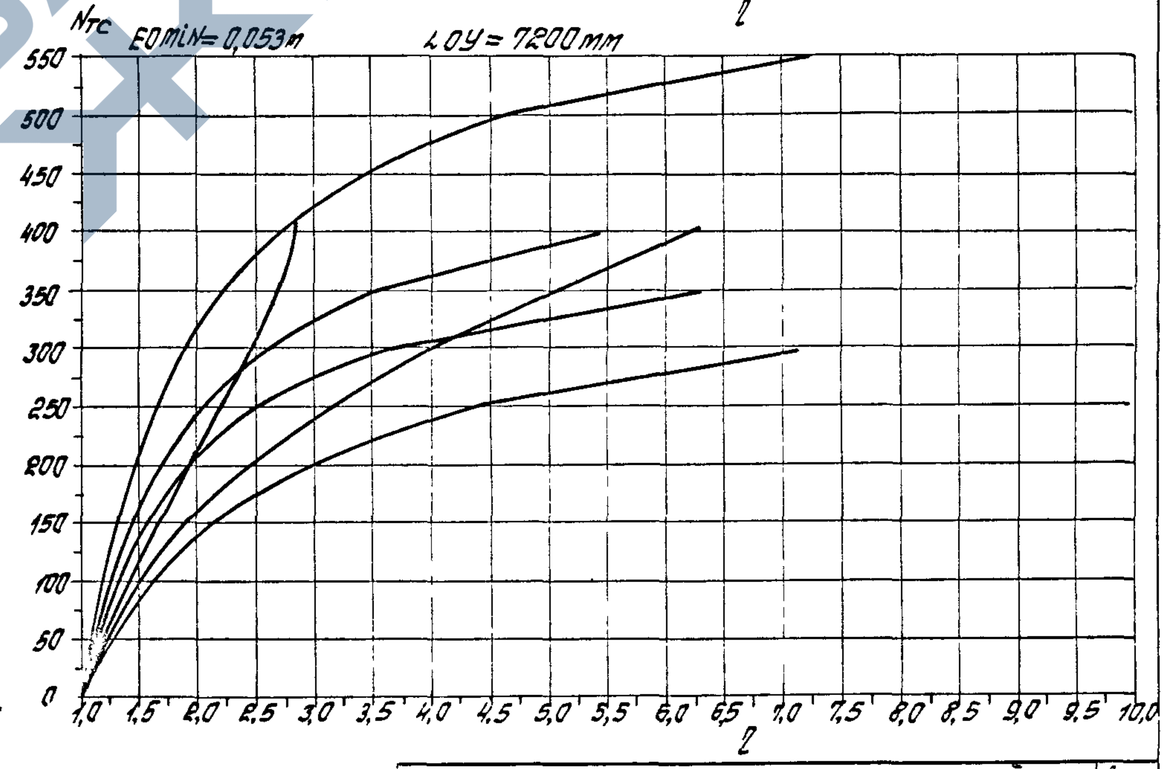
https://zavodjbi.com/









Инв. № подл. | Подпись и дата | Взам. инв. №

1.020. 1-4. 0-9-002

Лист 292

24166-03 69

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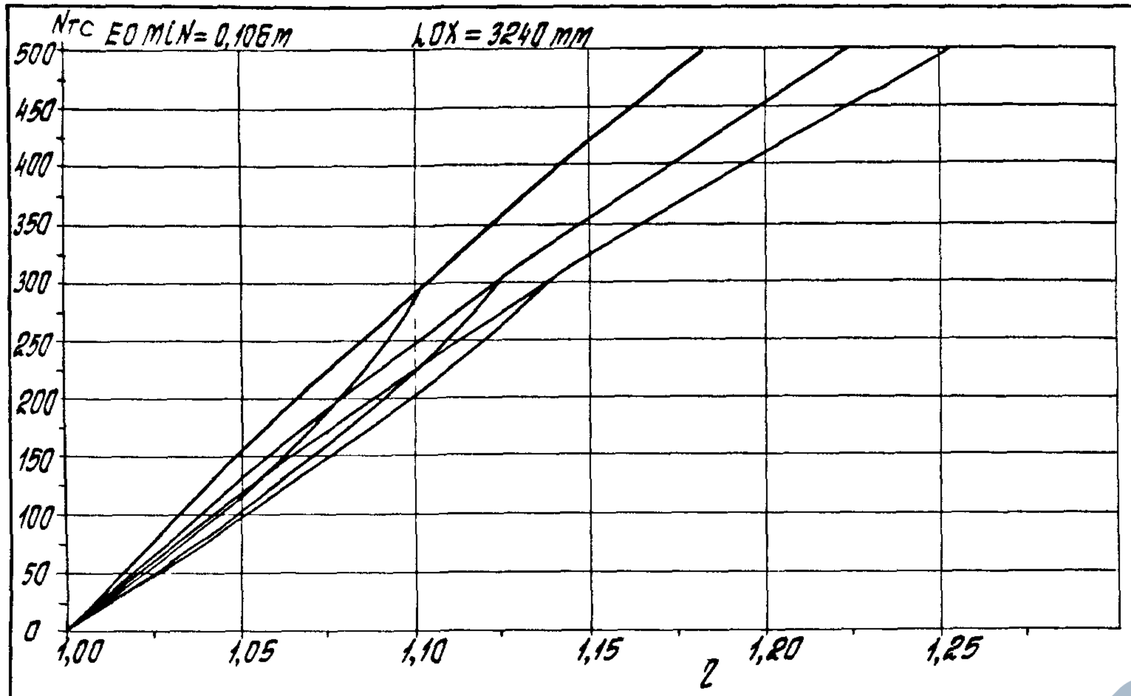

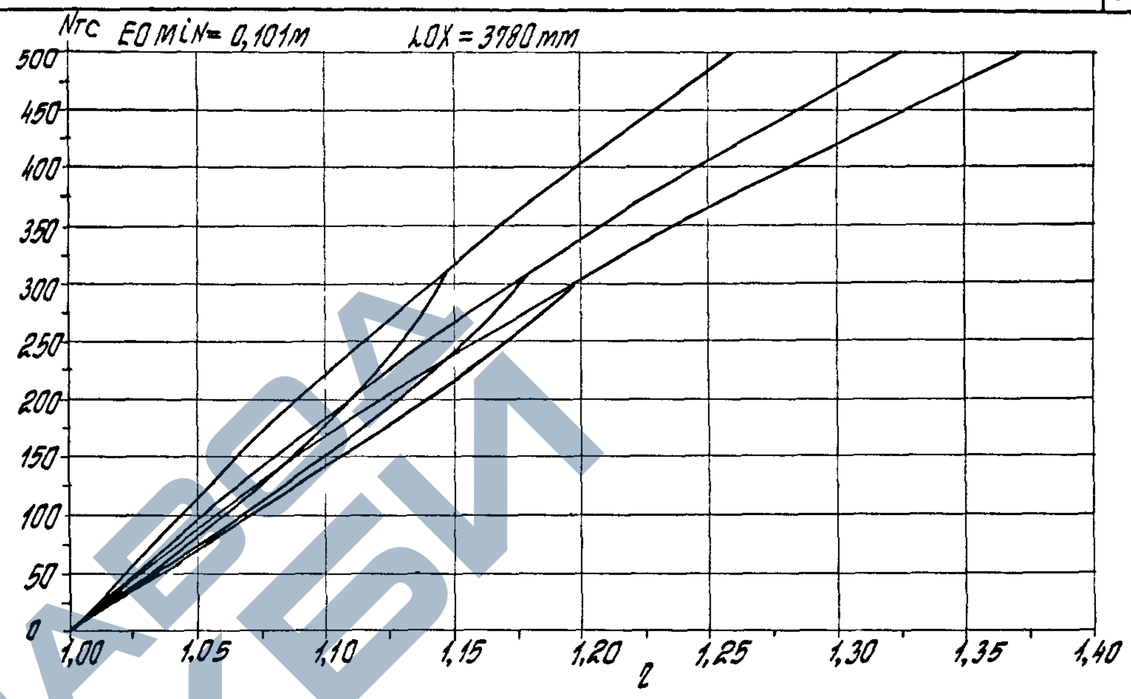

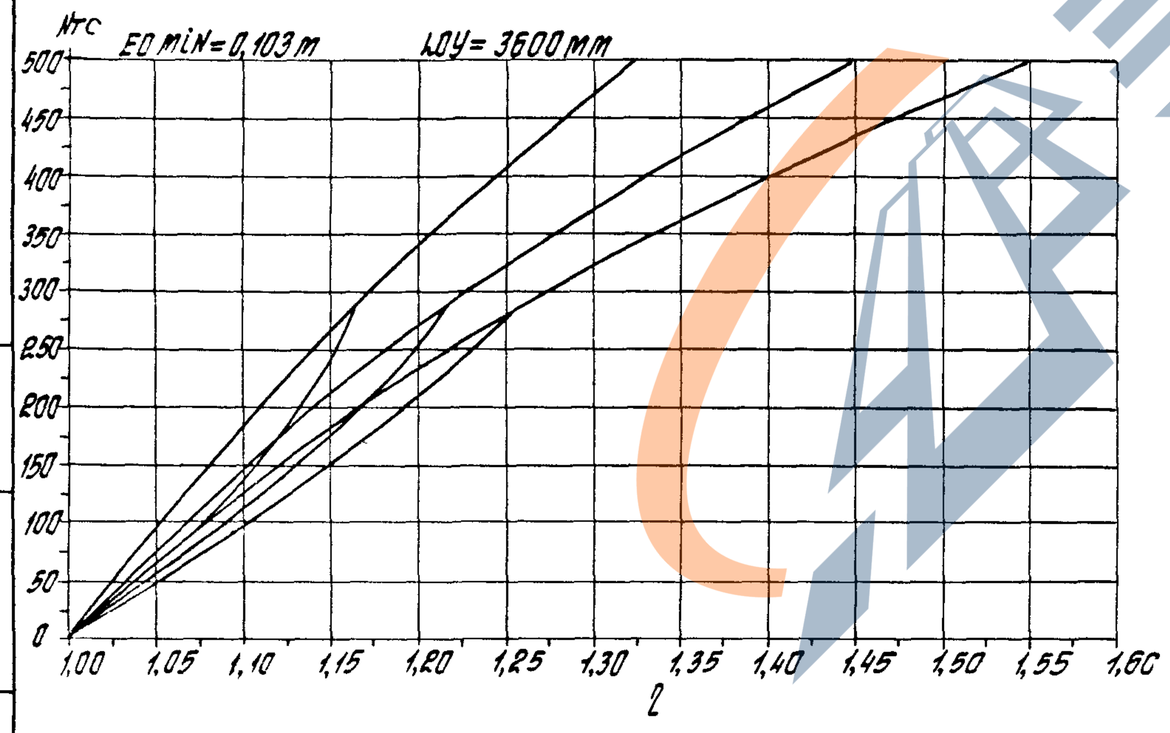

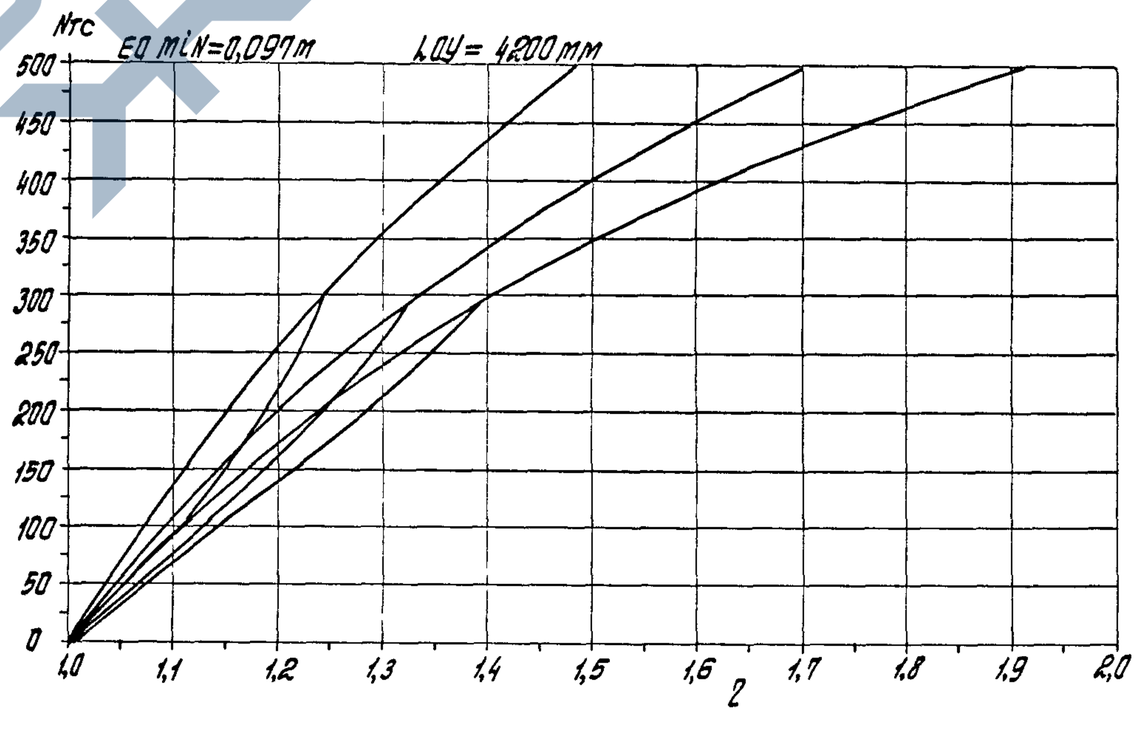

Инв. № подл. | Подпись и дата | Взам. инв. №

1.020.1-4. 0-9-002	Лист 203

24166-03 70

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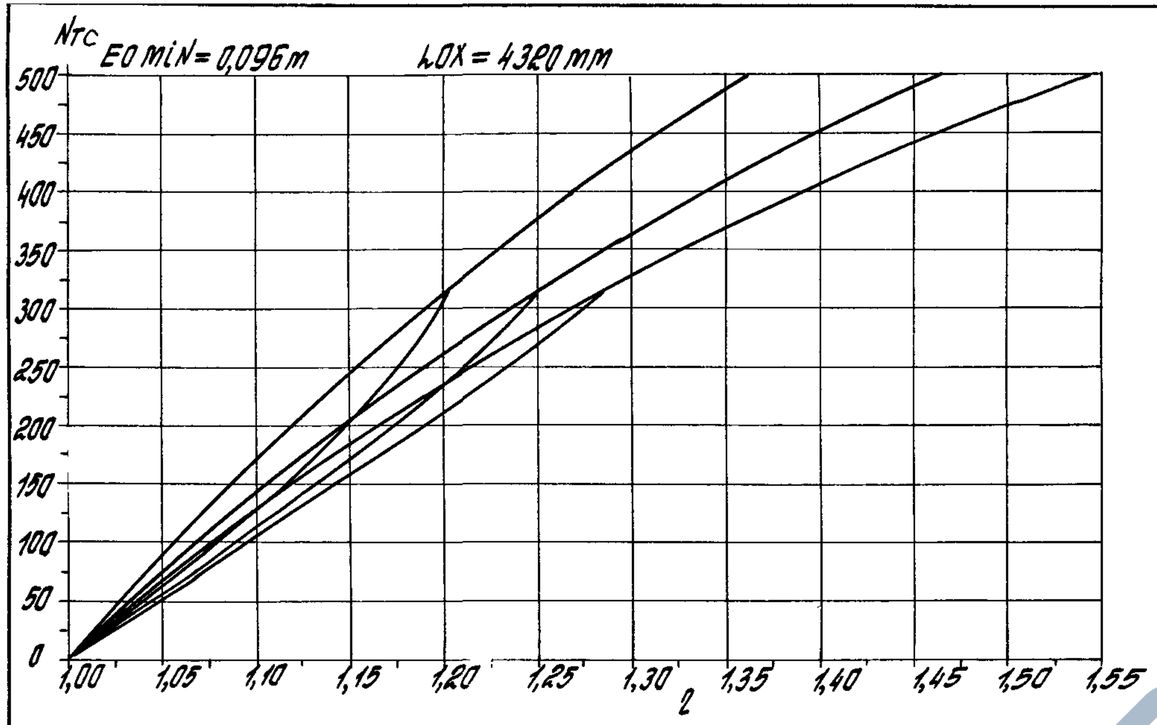

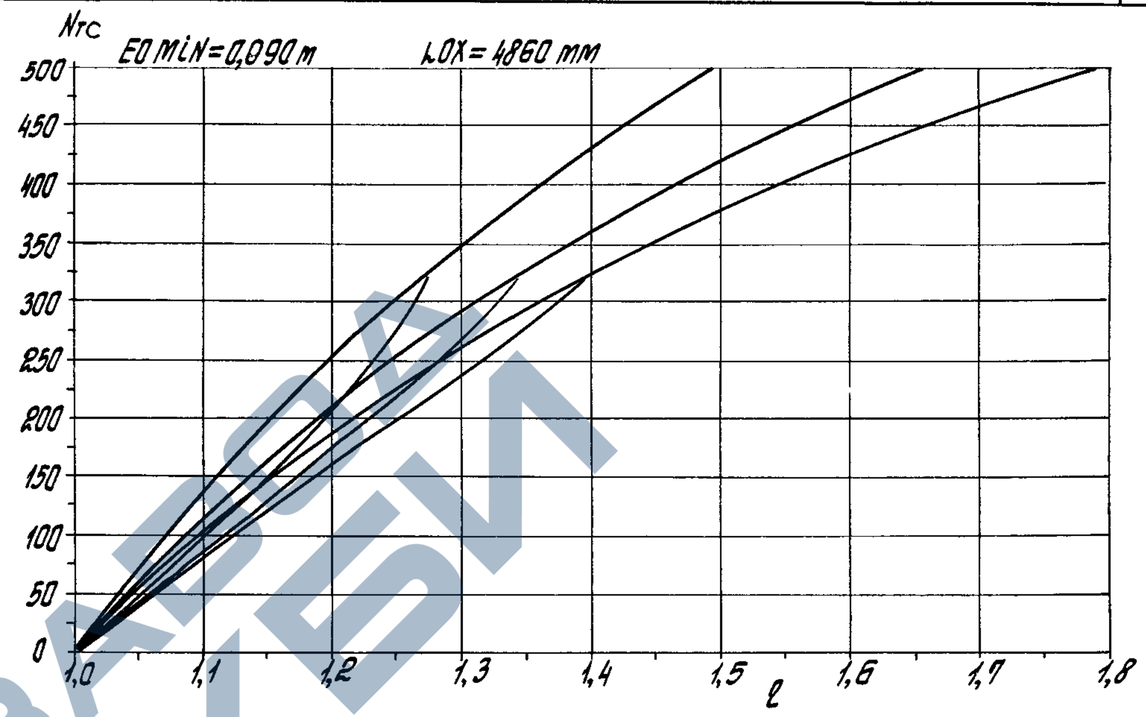

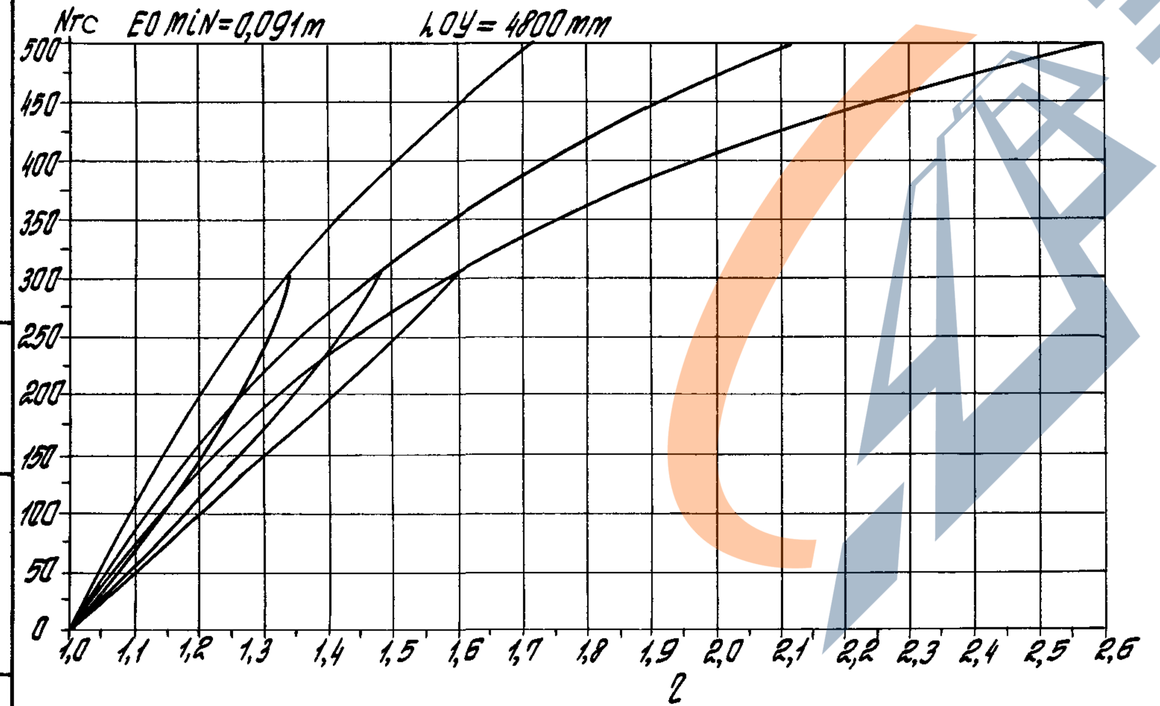

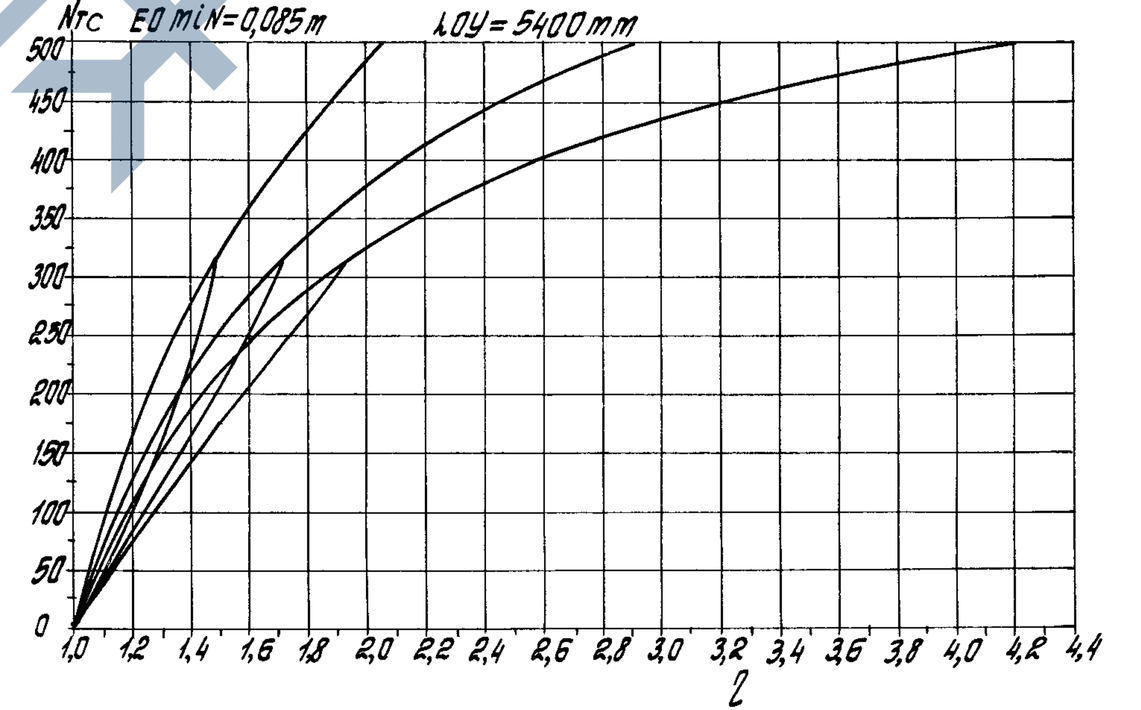

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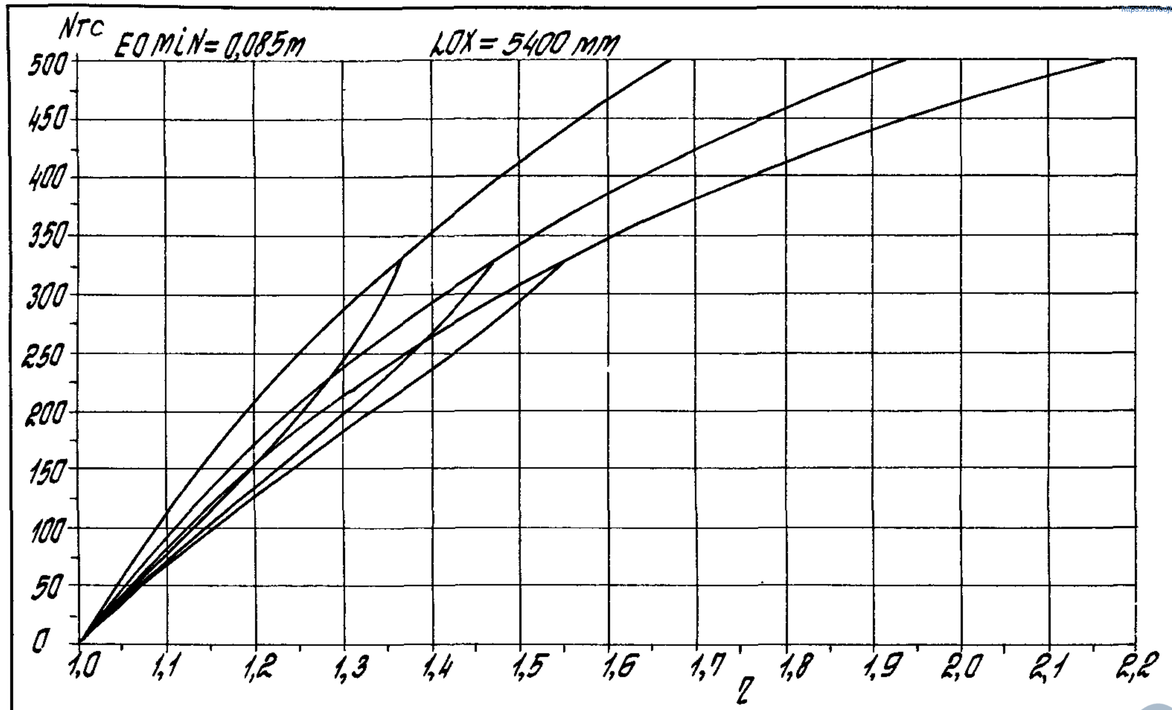

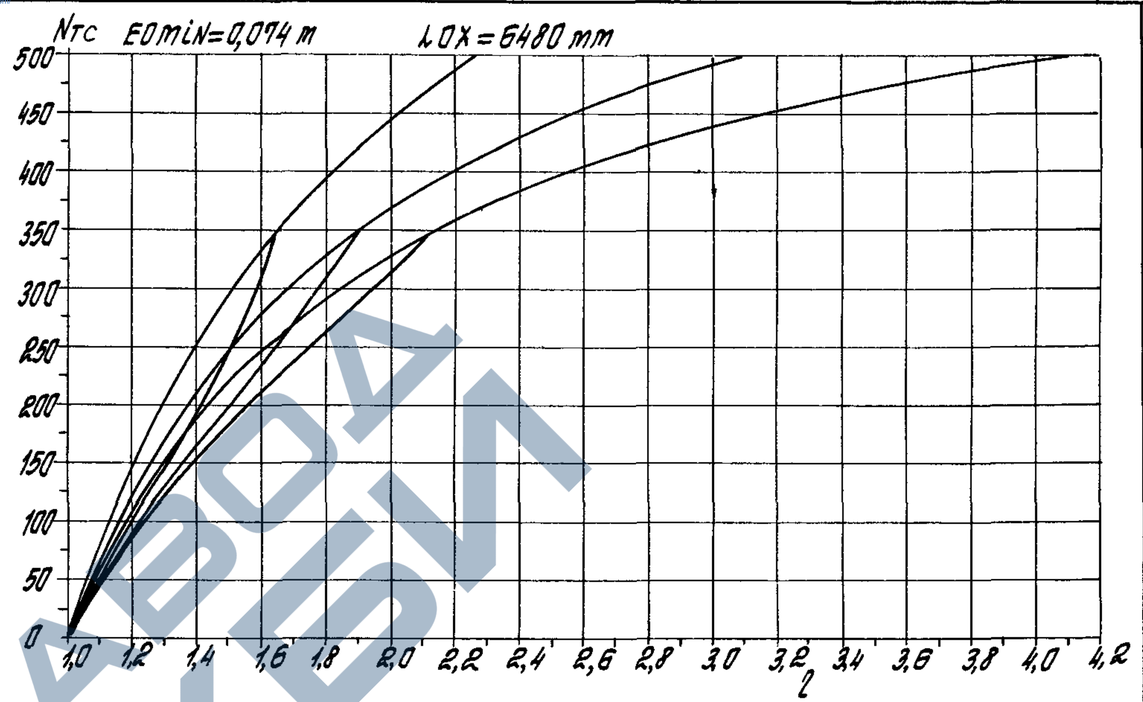

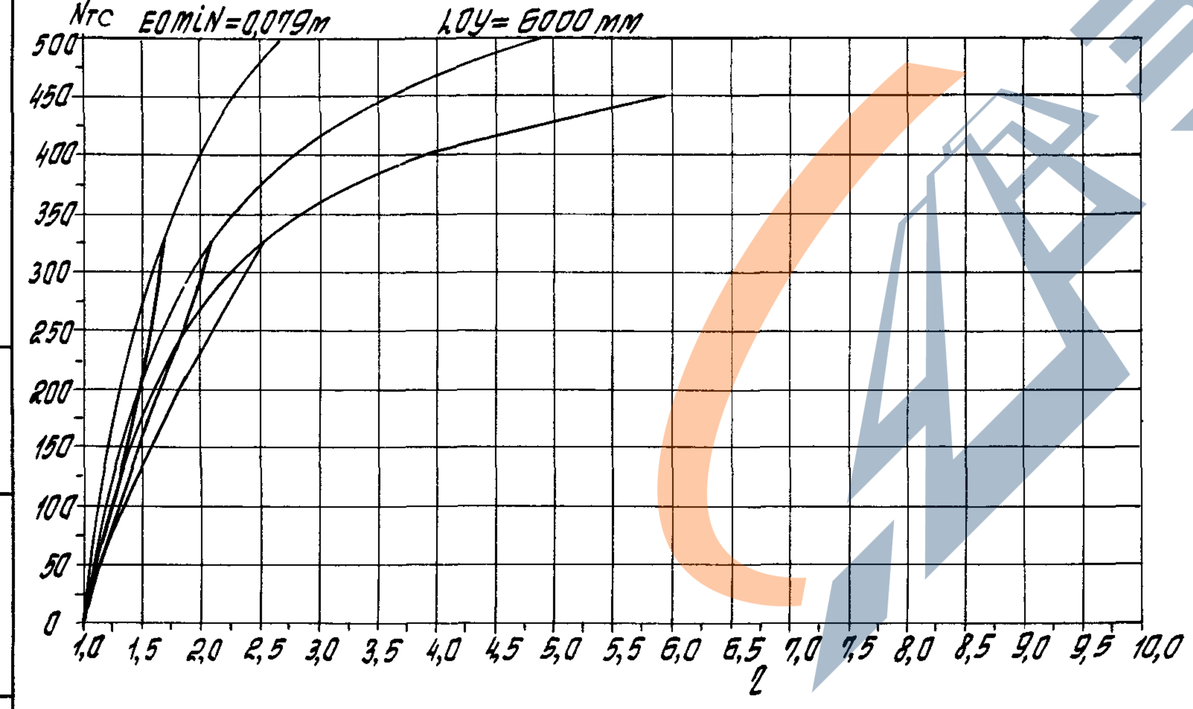

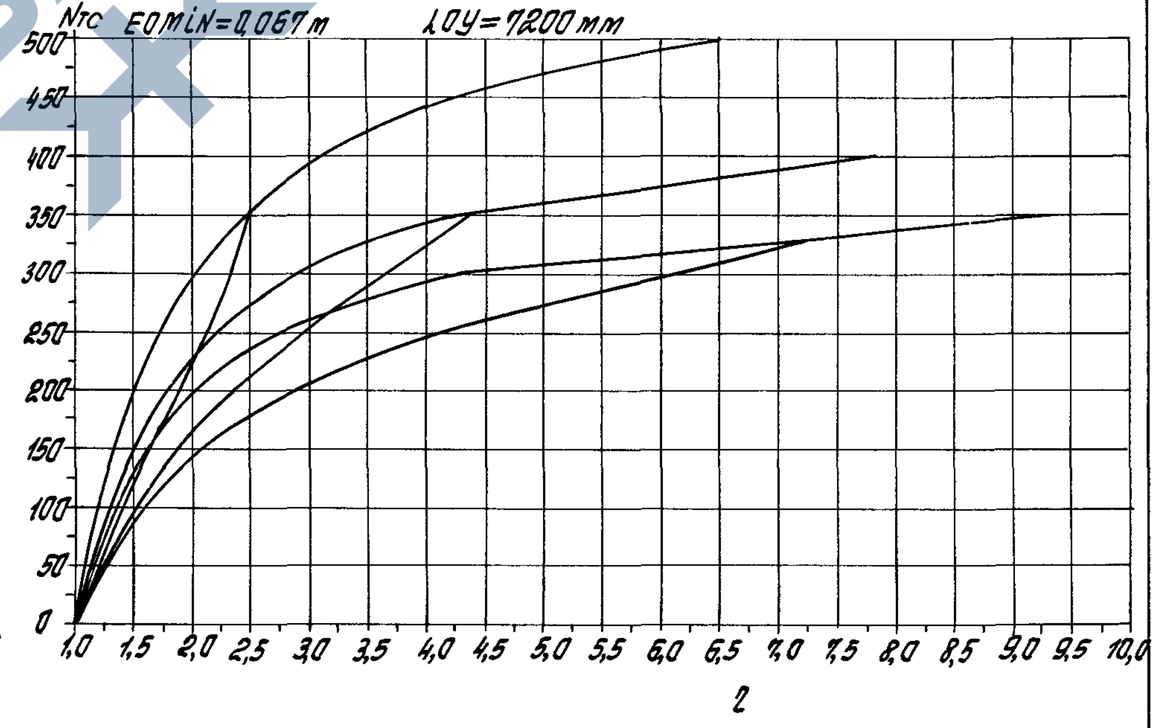

Инв. № подл. | Подпись и дата | Взам. инв. №

1.020.1-4	0-9002	Лист 295

24166-03 72

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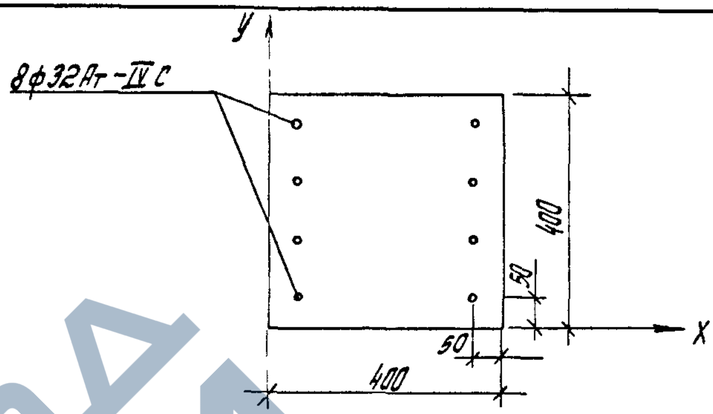
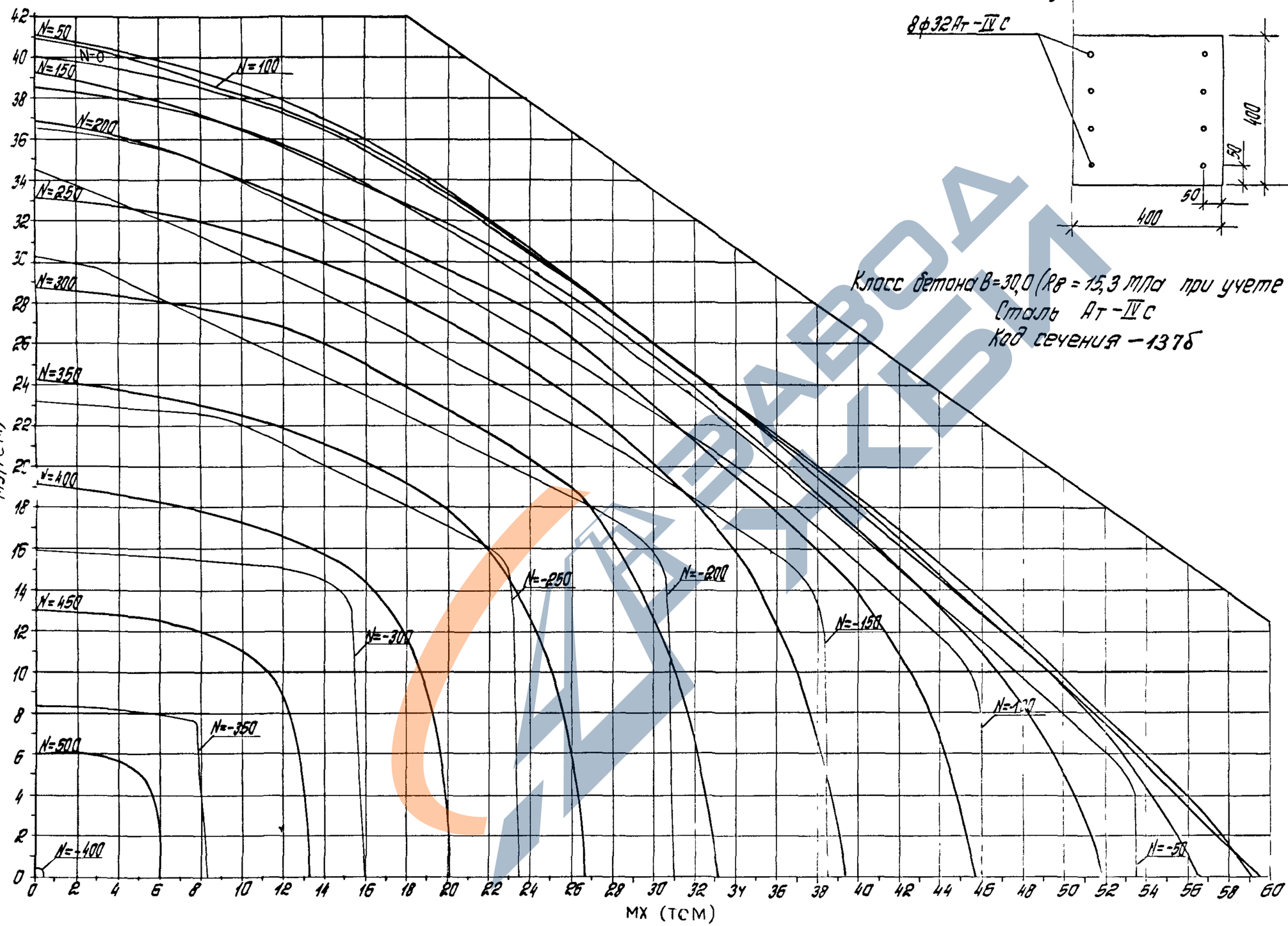


Класс бетона В=30,0 (R_B = 15,3 МПа при учете γ_{B2} = 0,90)
Сталь Ат-IVС
Код сечения – 1378



Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4. 0-9-002	Лист 296

24166-03 73

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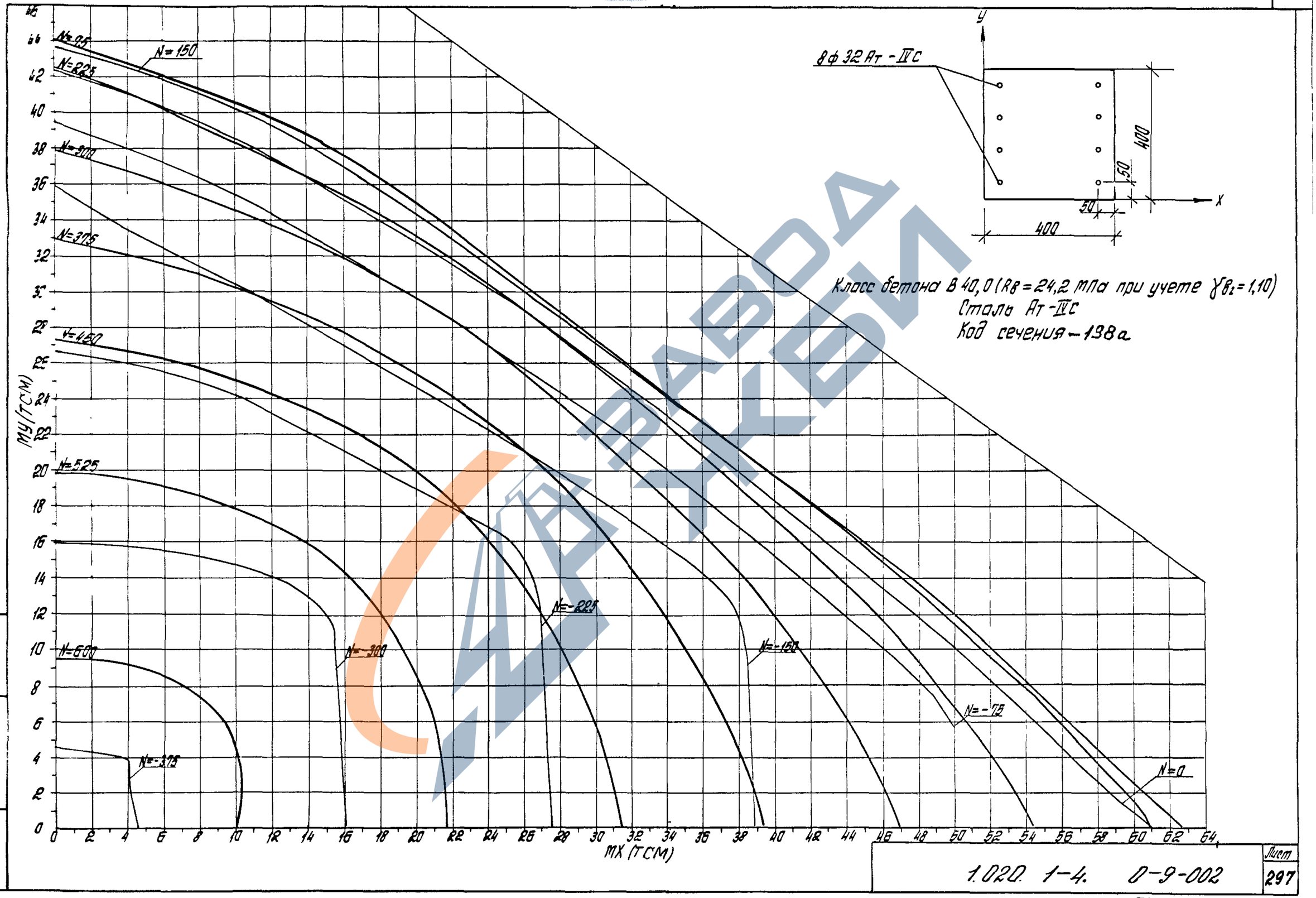

1.020. 1-4. 0-9-002

Лист 297

24166-03 74

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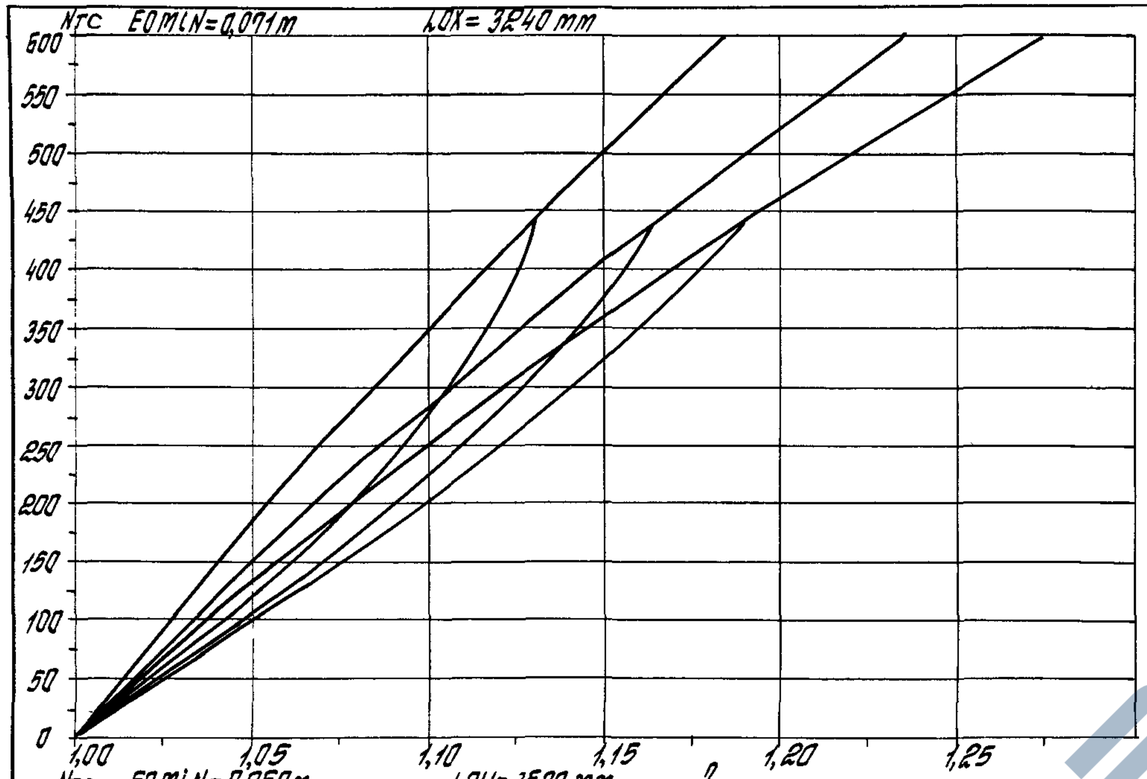

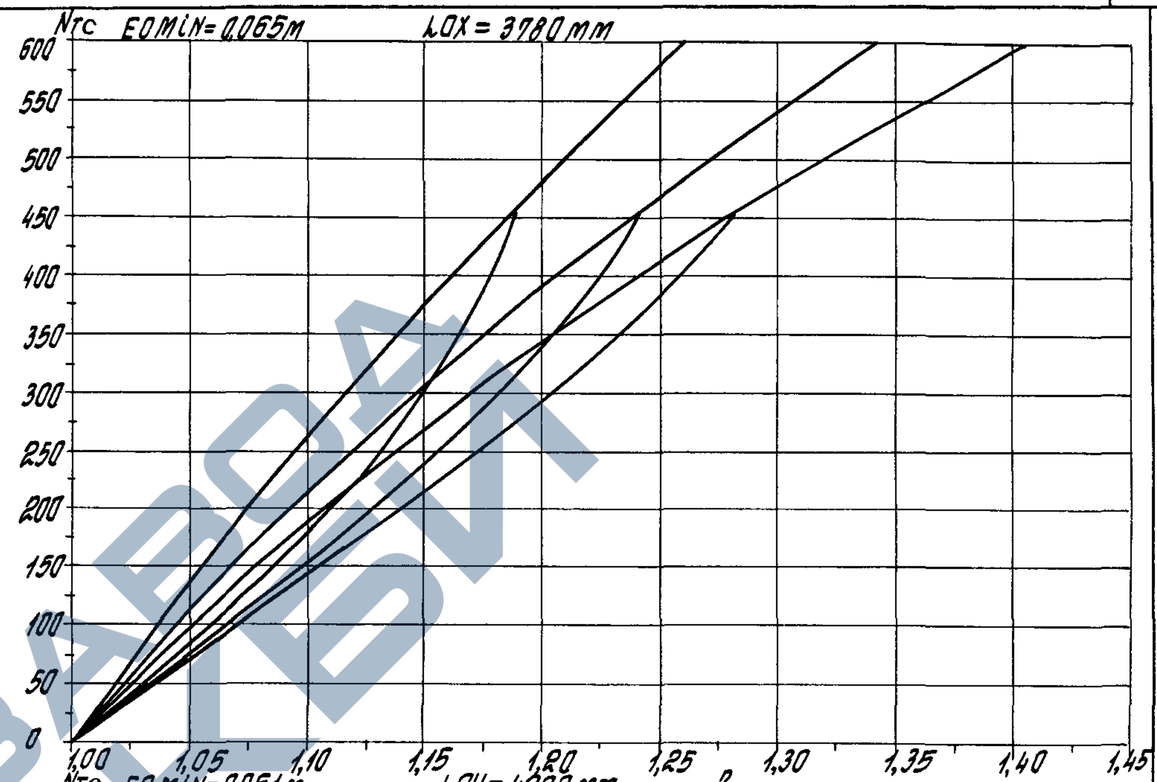

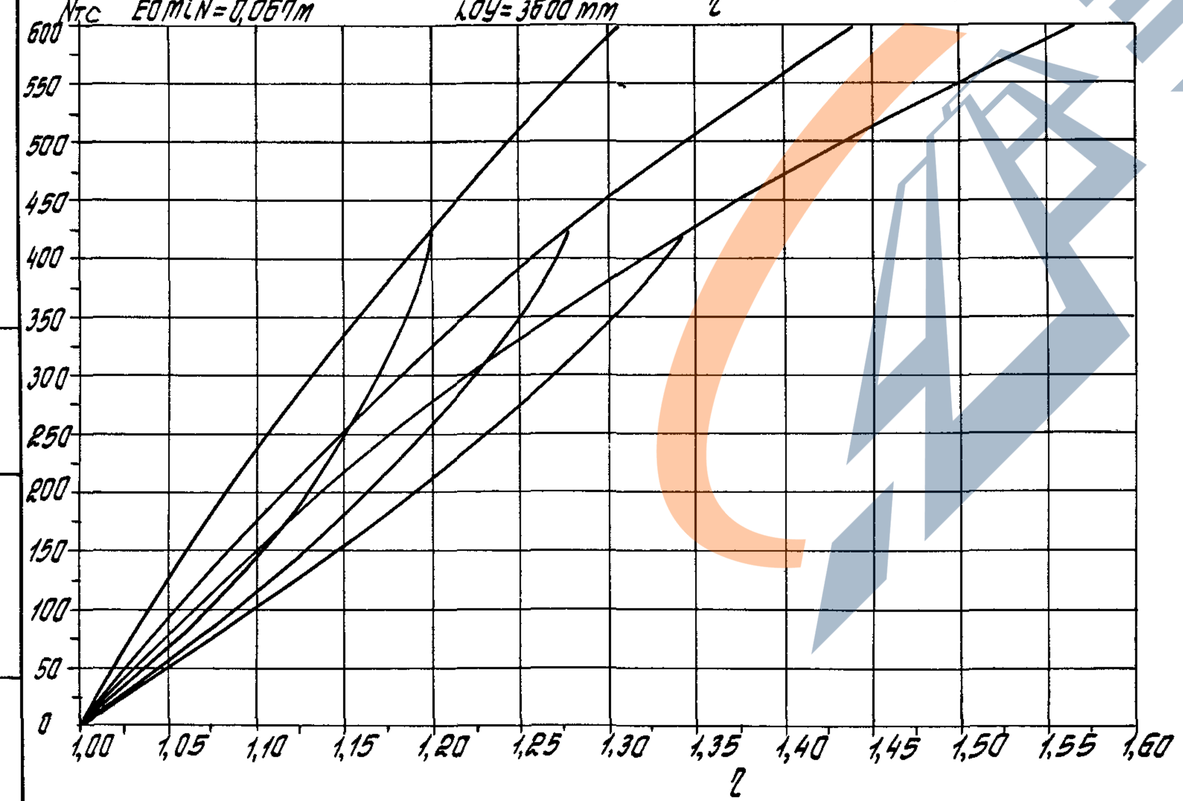

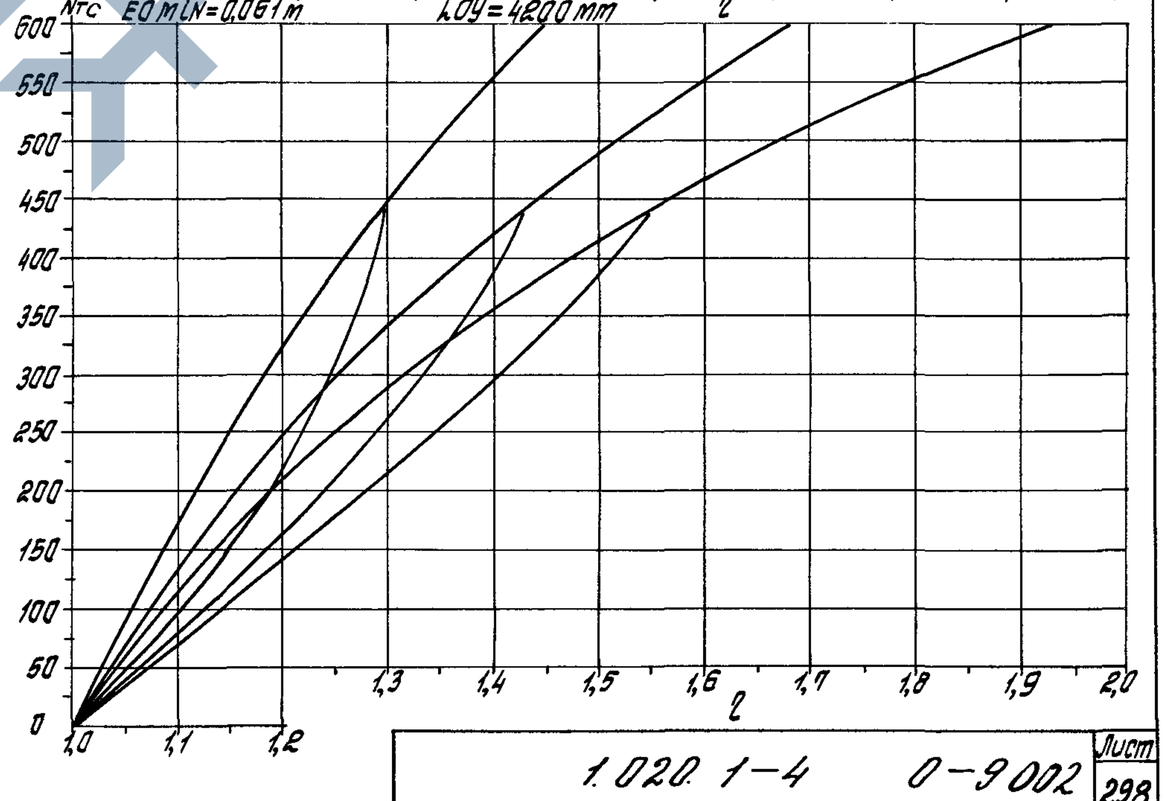

Инв.№ подл. | Подпись и дата | Взам.инв.№

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Лист 298

24166-03 75

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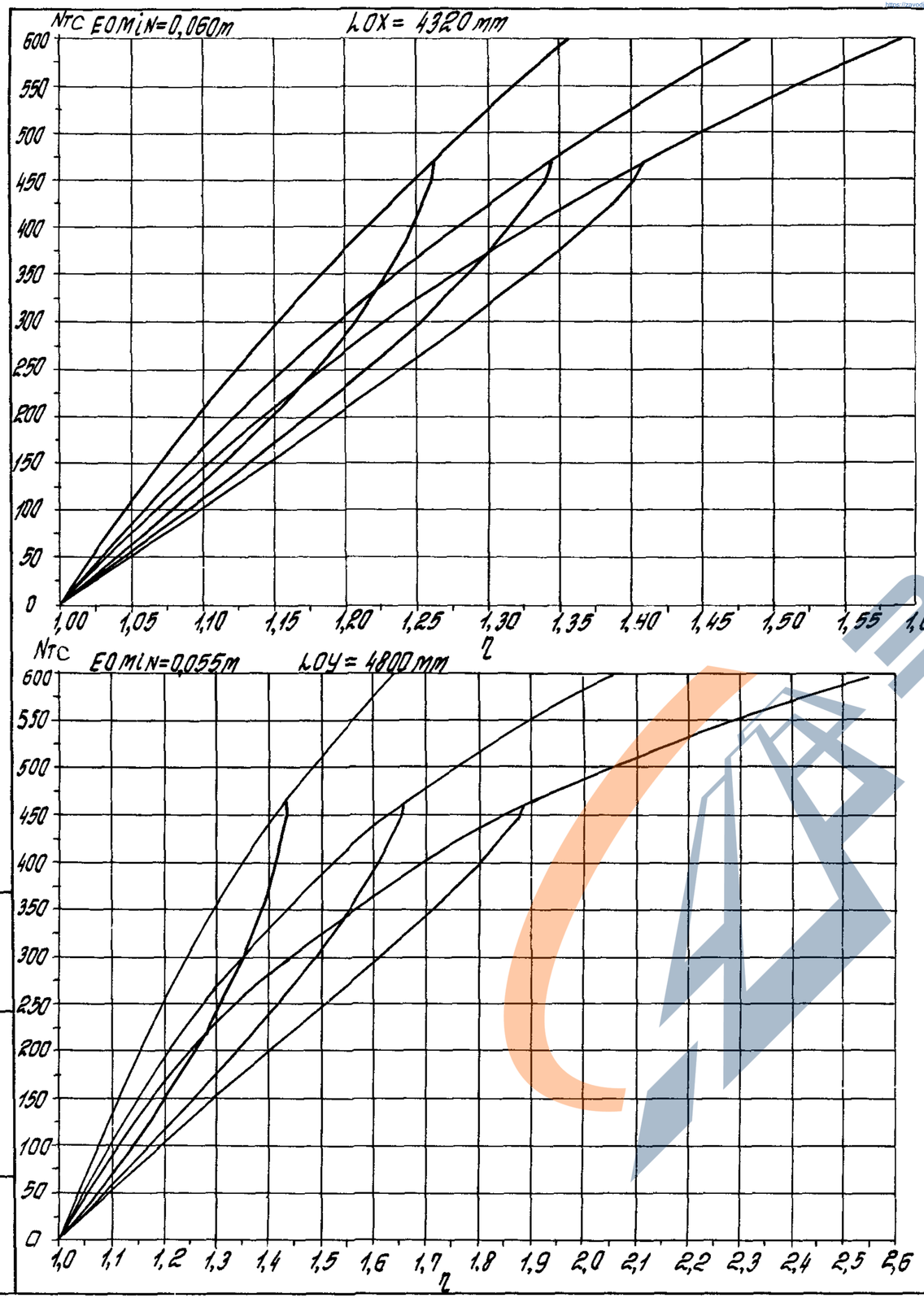

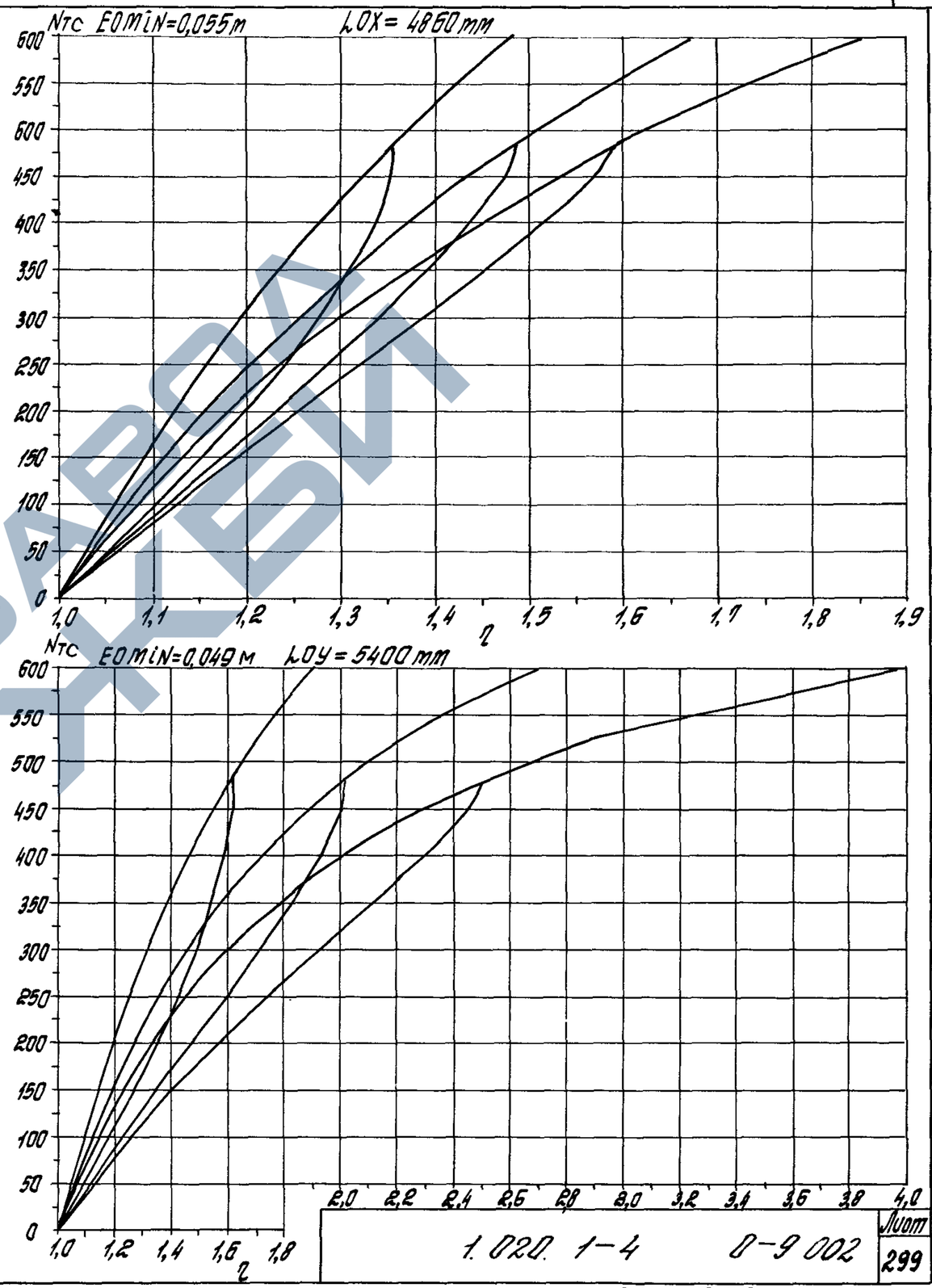

Инв.№ подл. | Подпись и дата | Взам.инв.№

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Лист 299

24166-03 76

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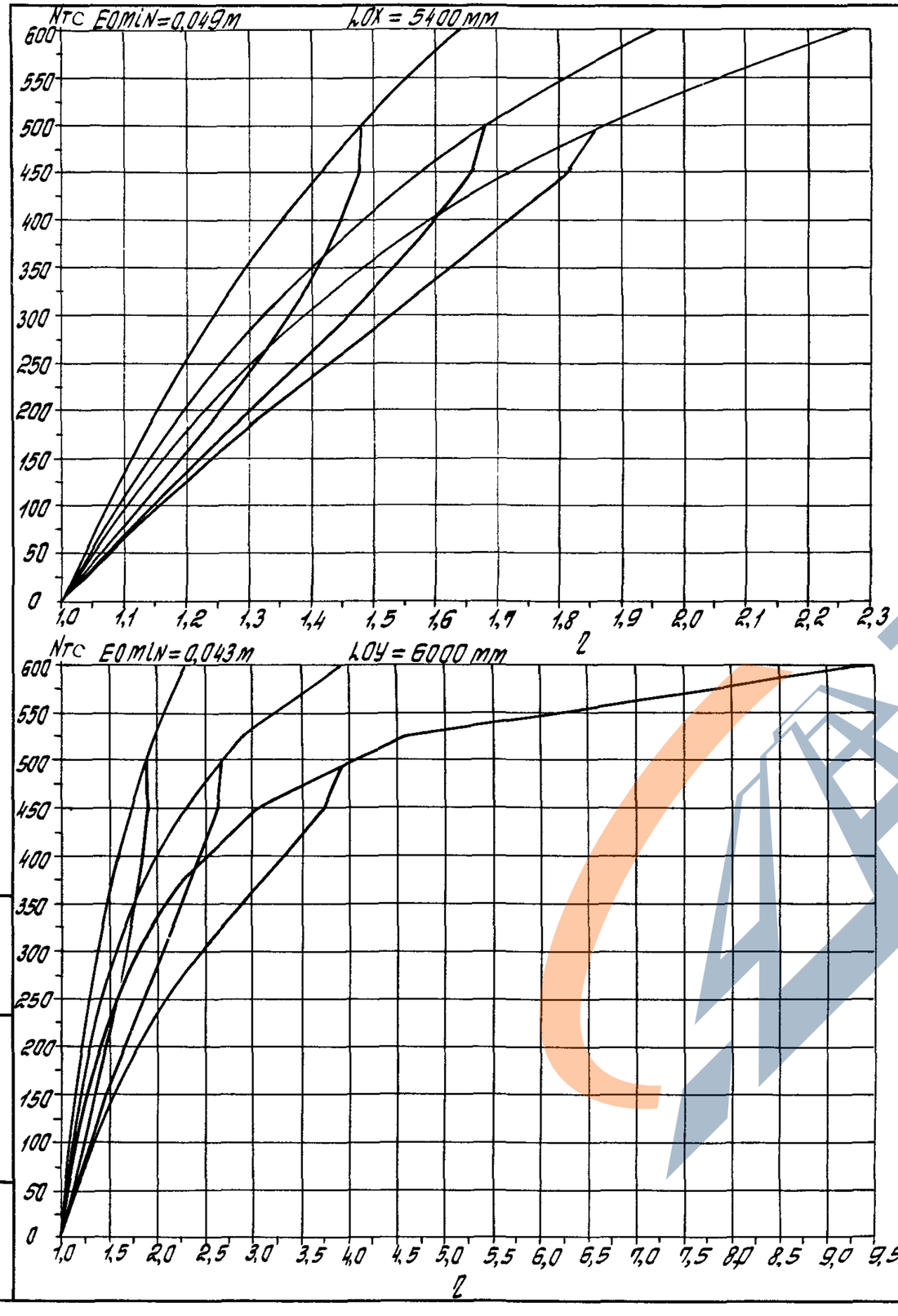

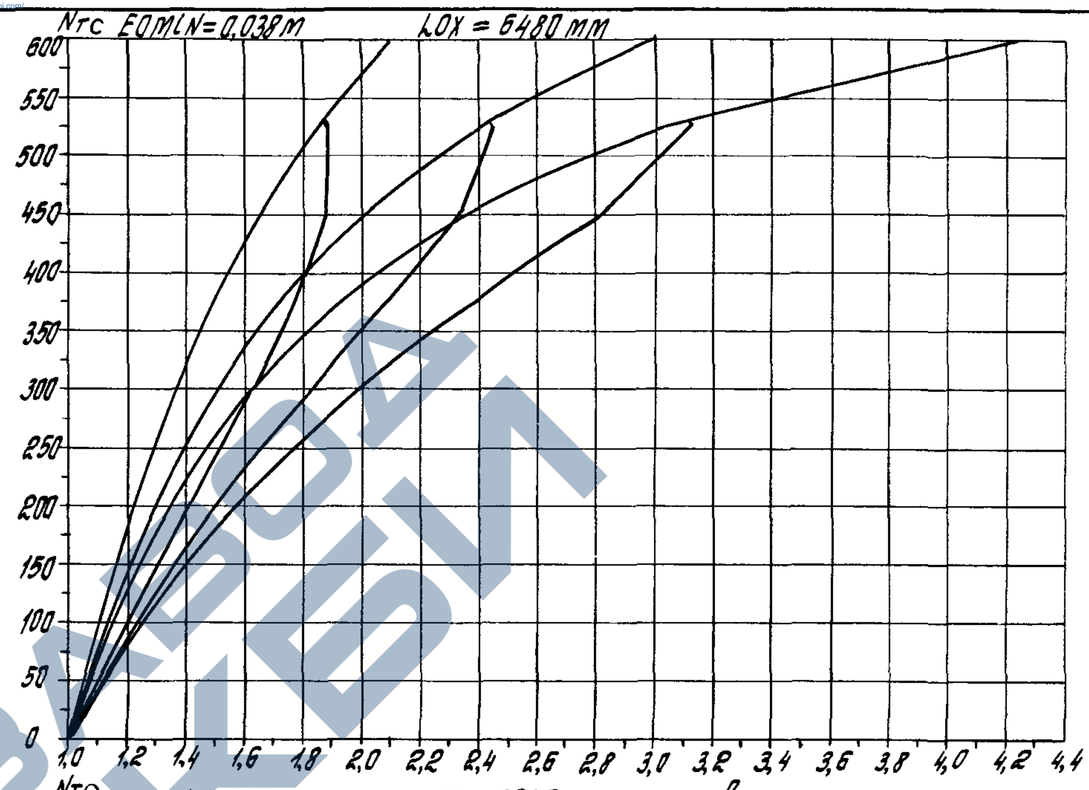

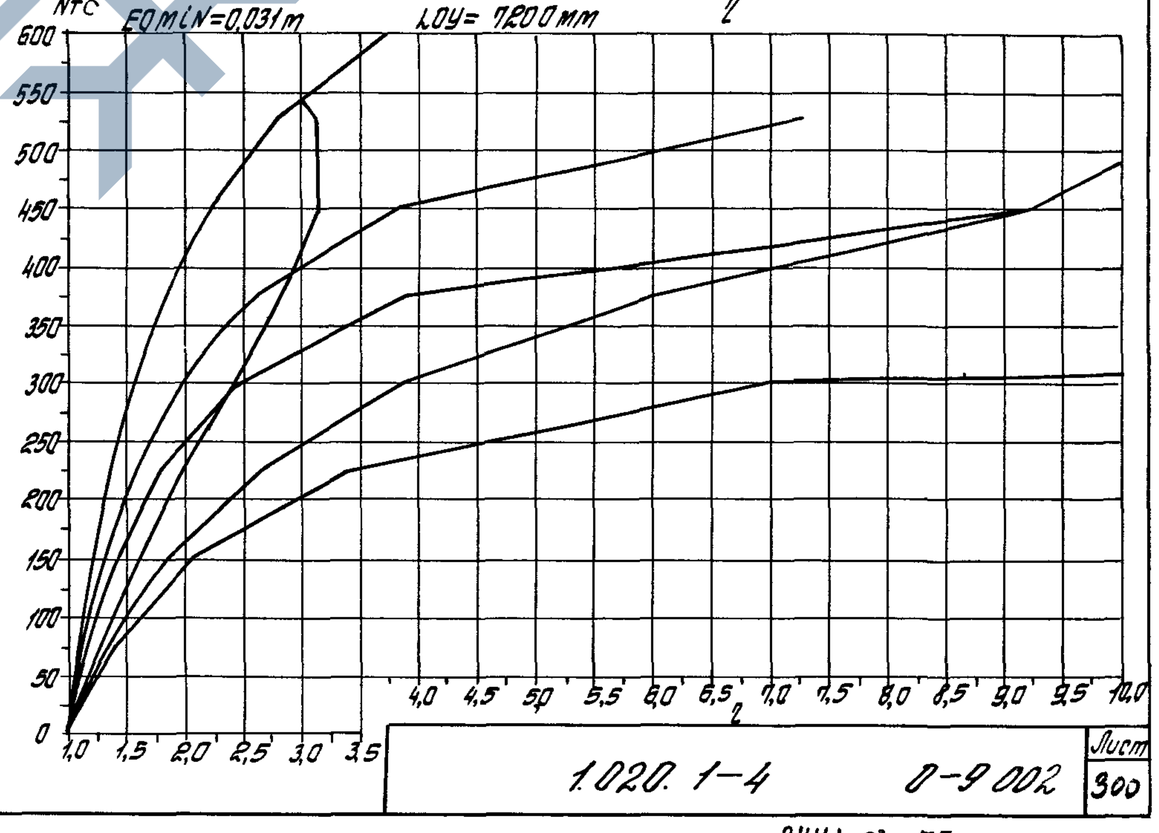

Инв. № подл. | Подпись и дата | Взам. инв. №

1.020.1-4	0-9002	Лист 300

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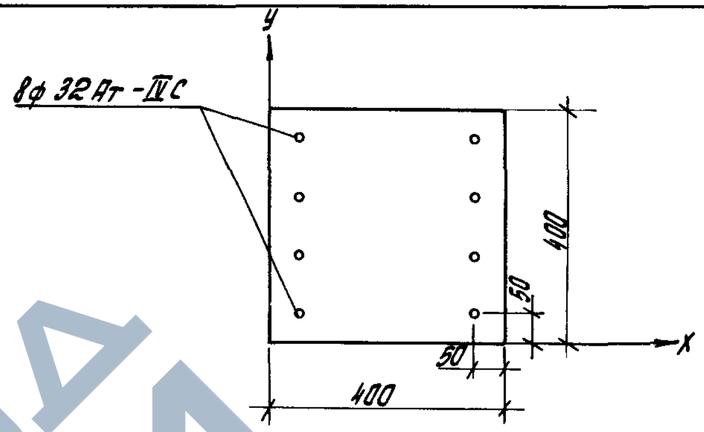
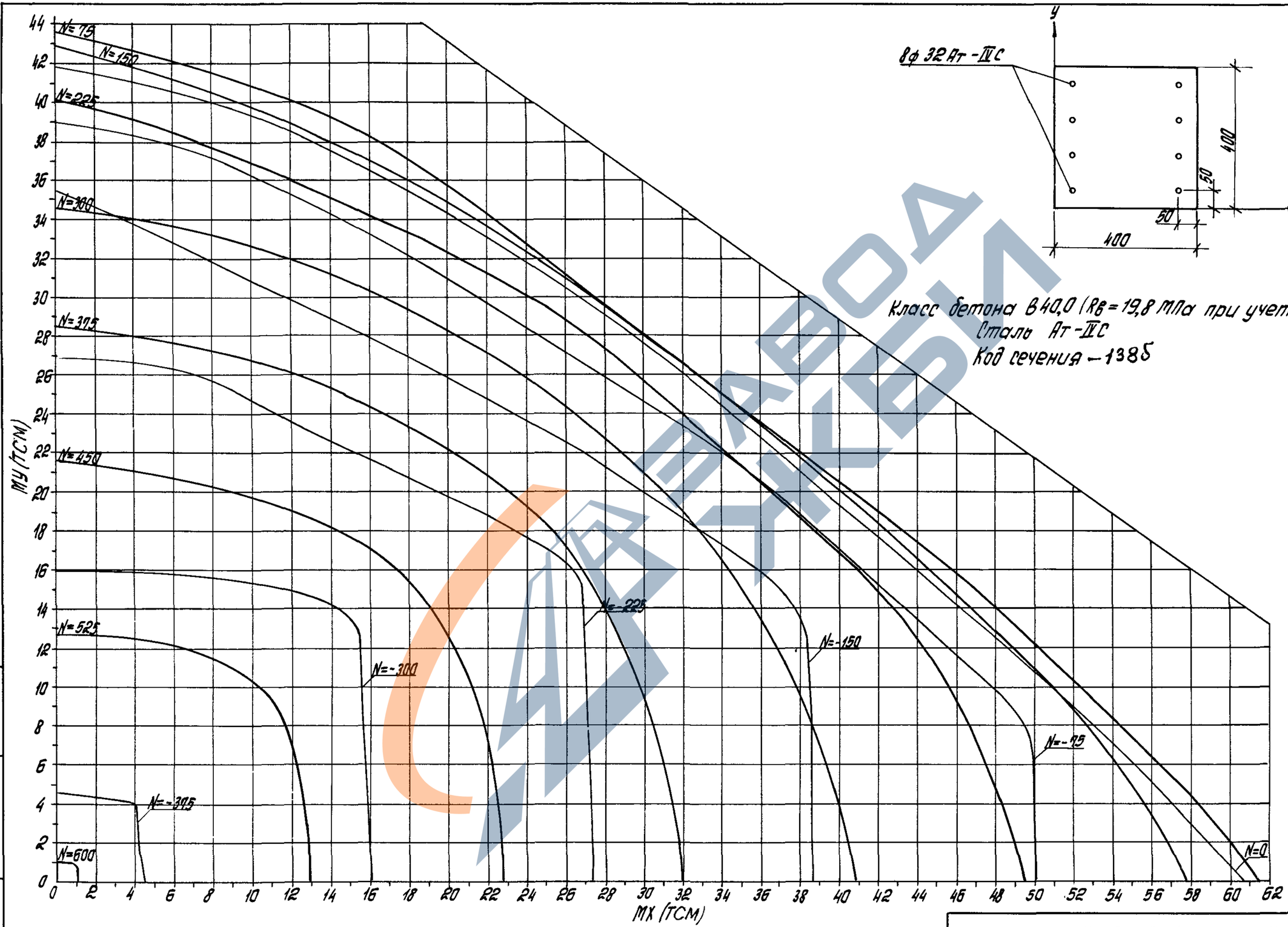


Класс бетона В40,0 ($R_в$ = 19,8 МПа при учете $\gamma_{в2}$=0,90)
Сталь Ат-IVС
Код сечения – 1385



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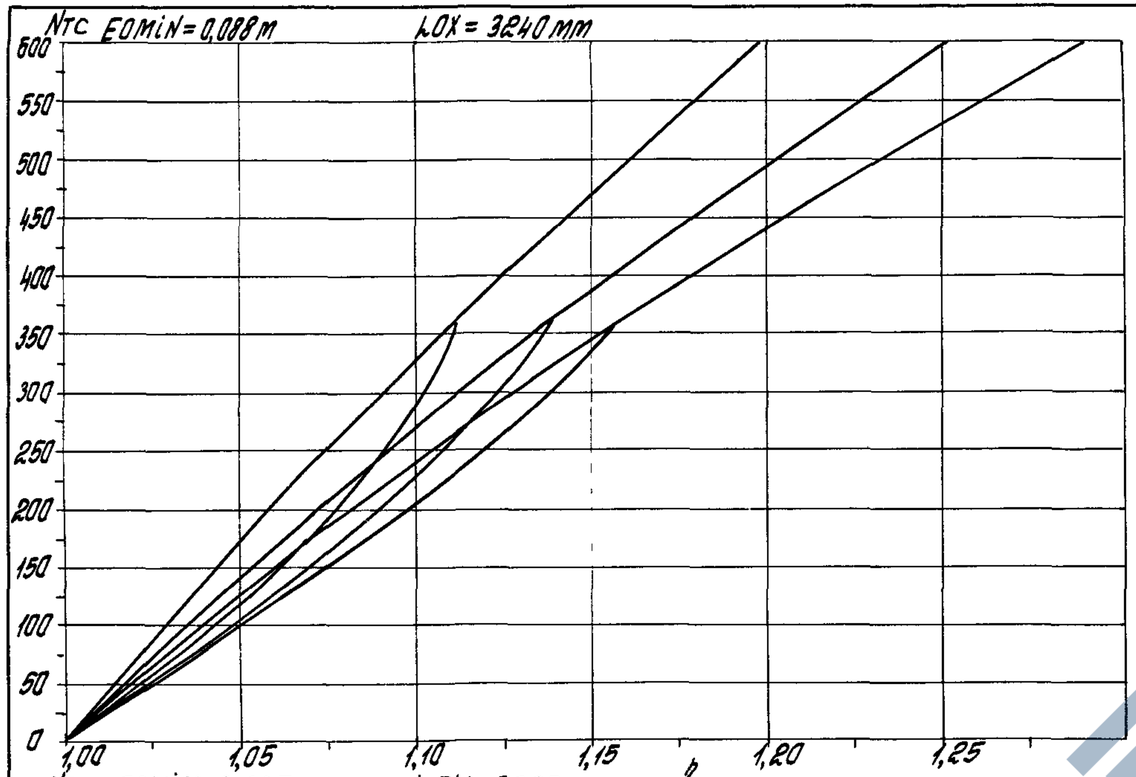

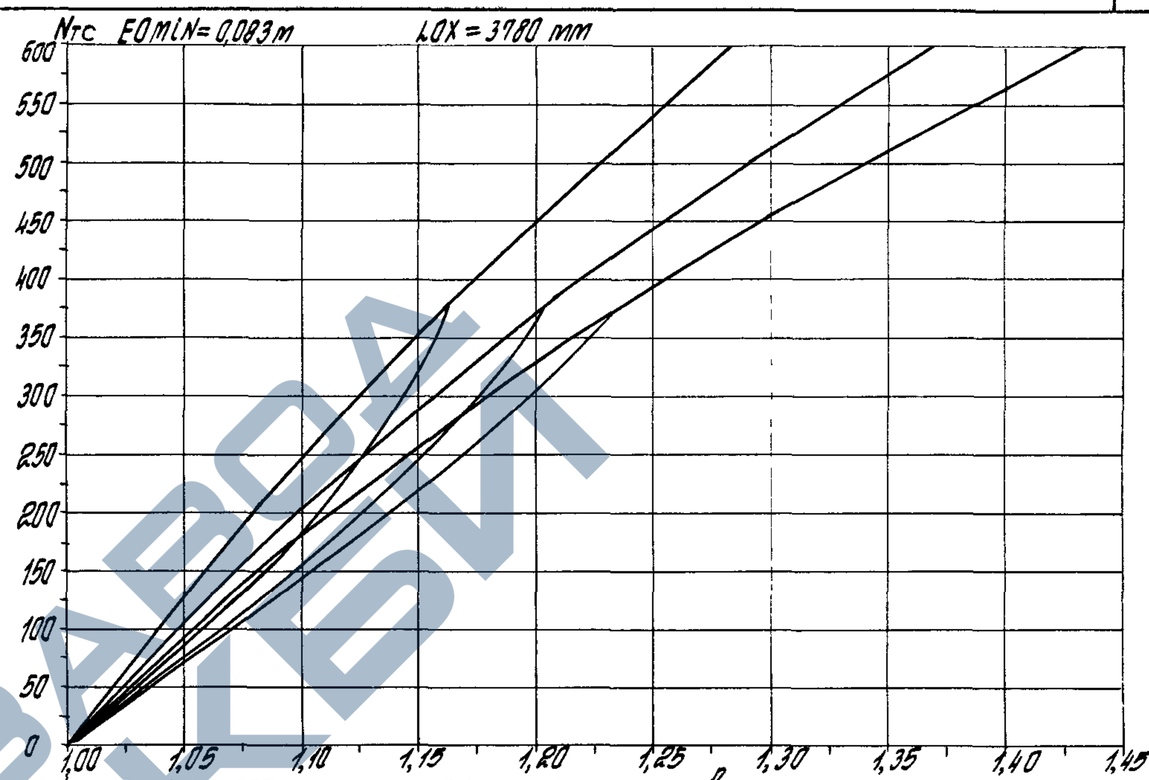

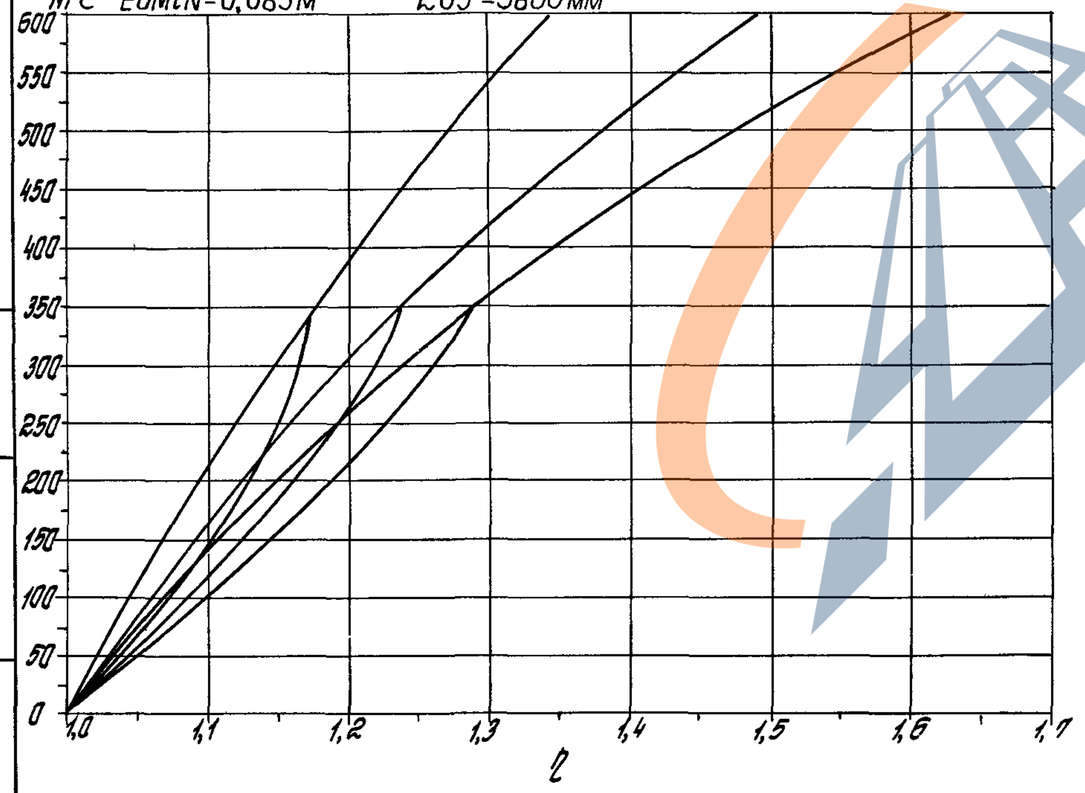

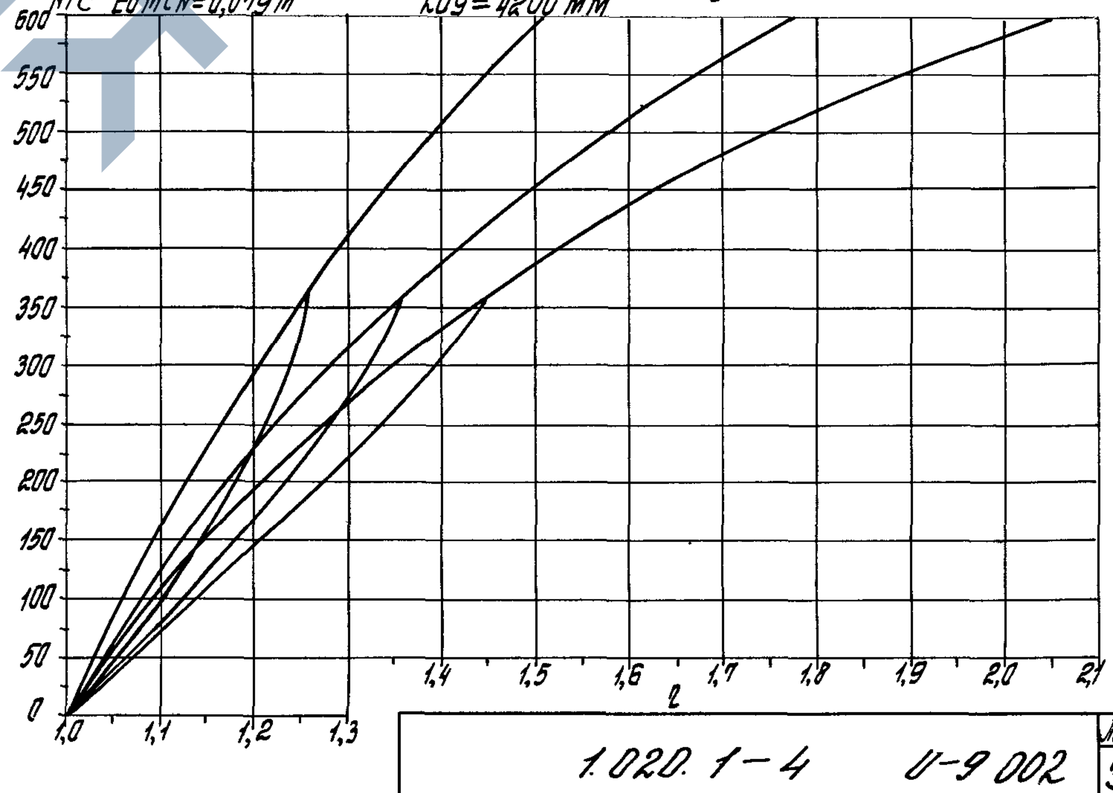

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Лист 302

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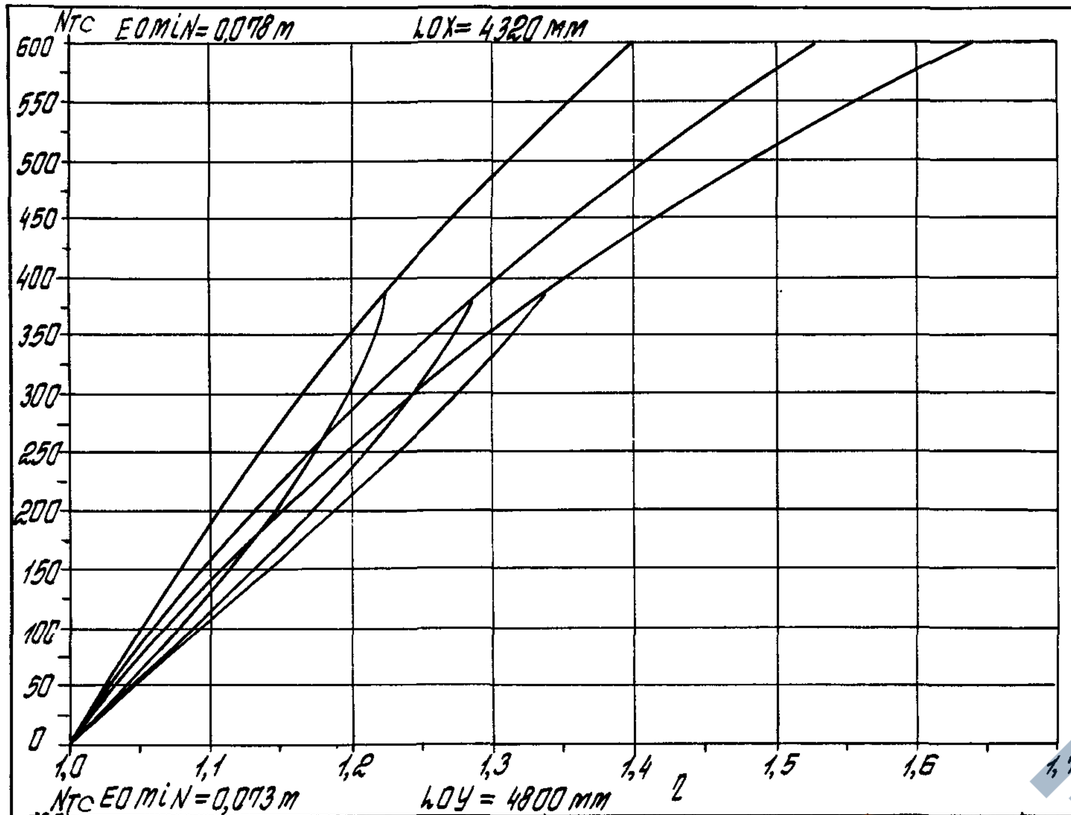

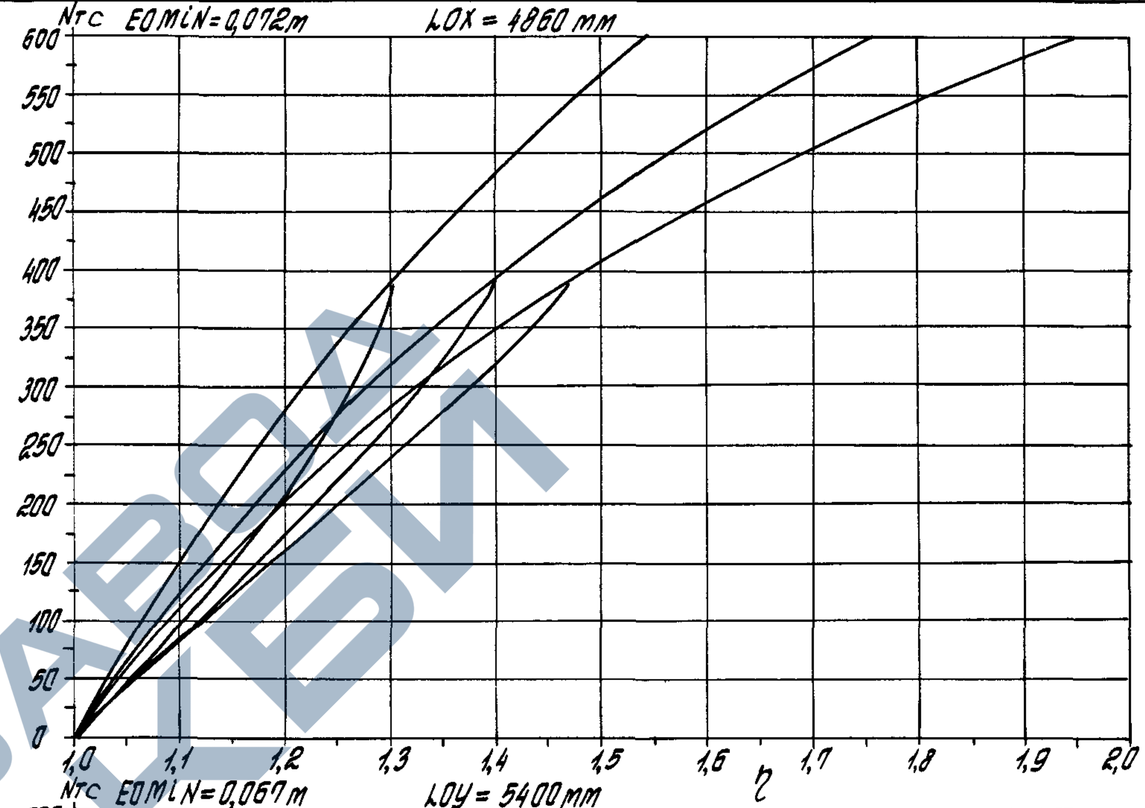

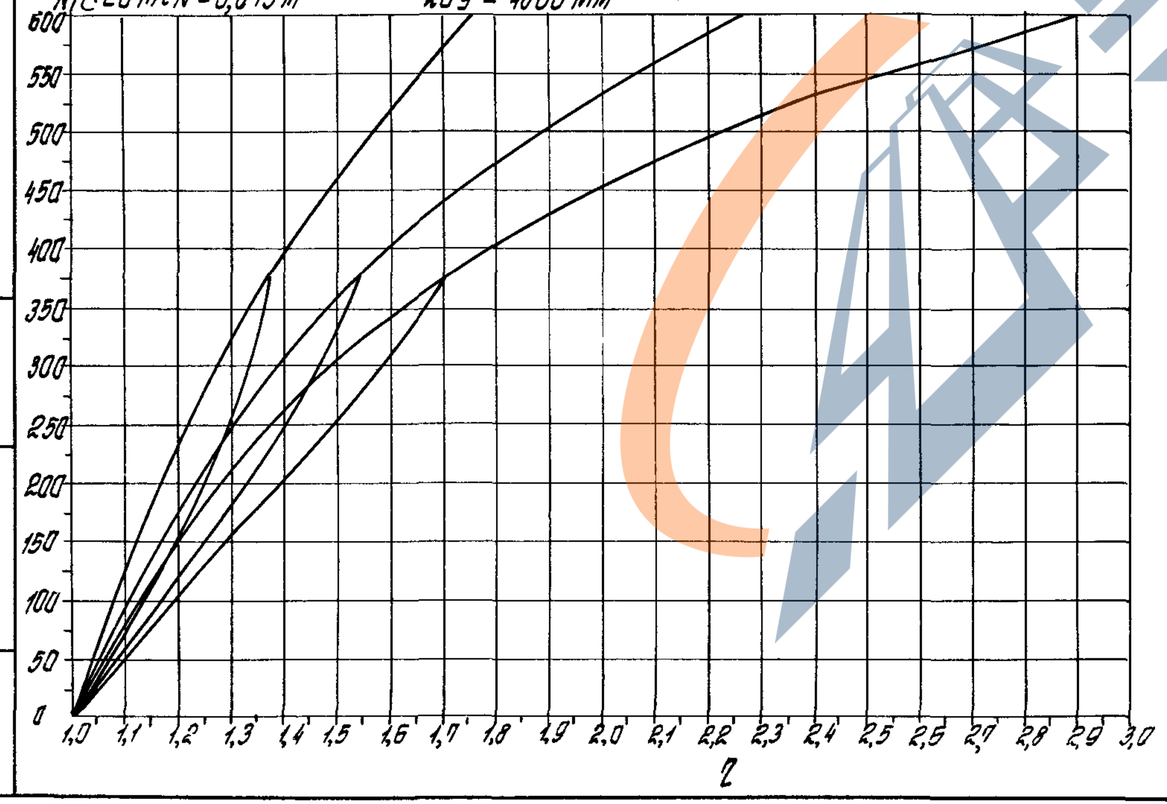

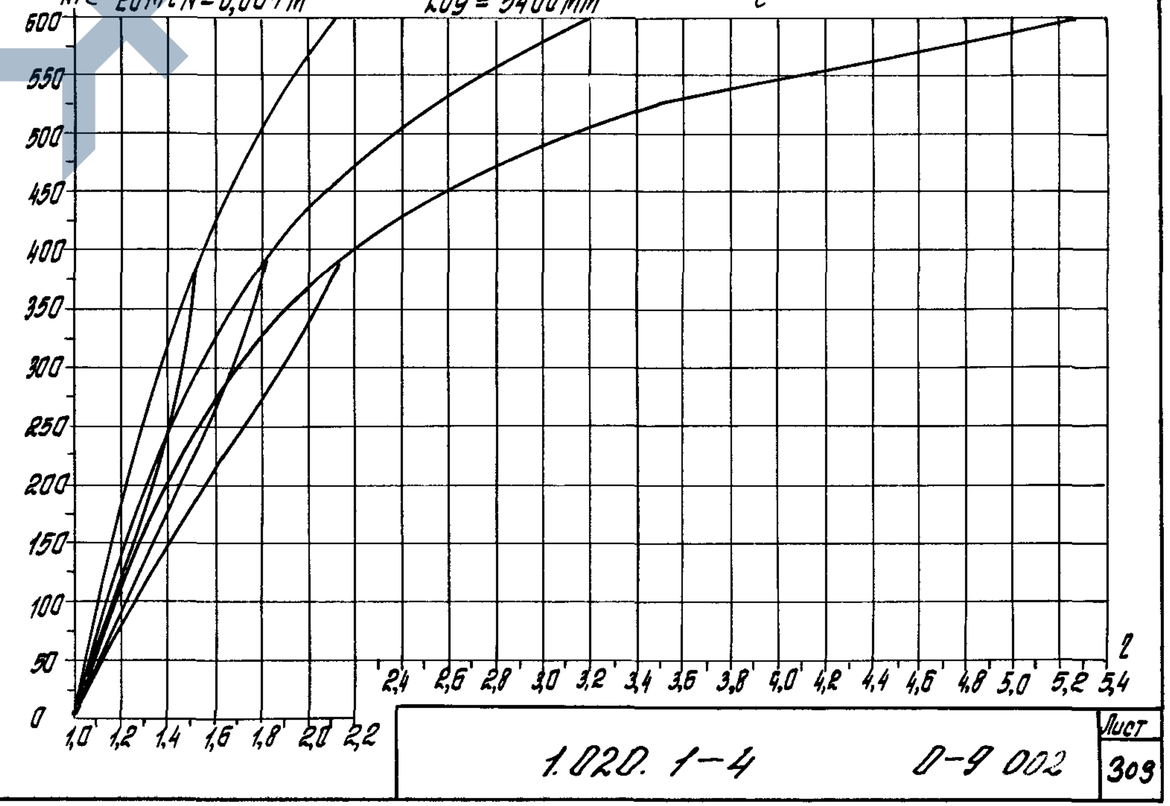

Инв.№ подл. | Подпись и дата | Взам.инв.№

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Лист 309

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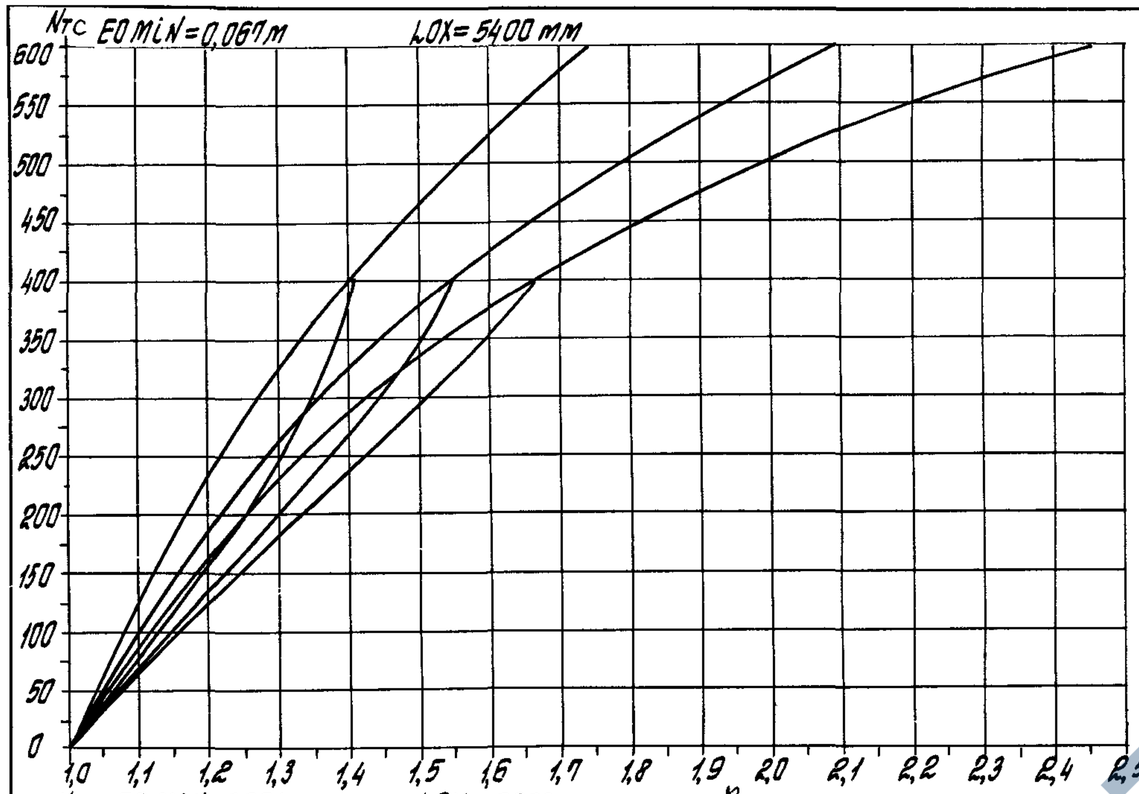

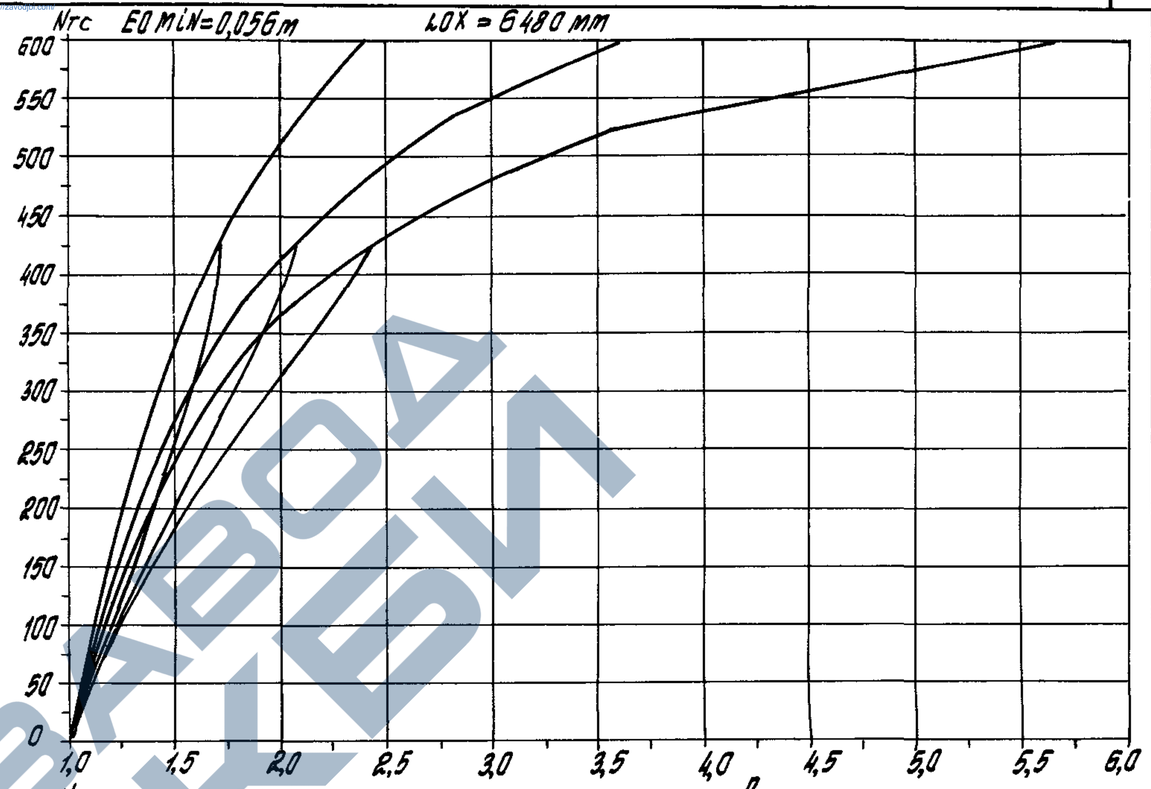

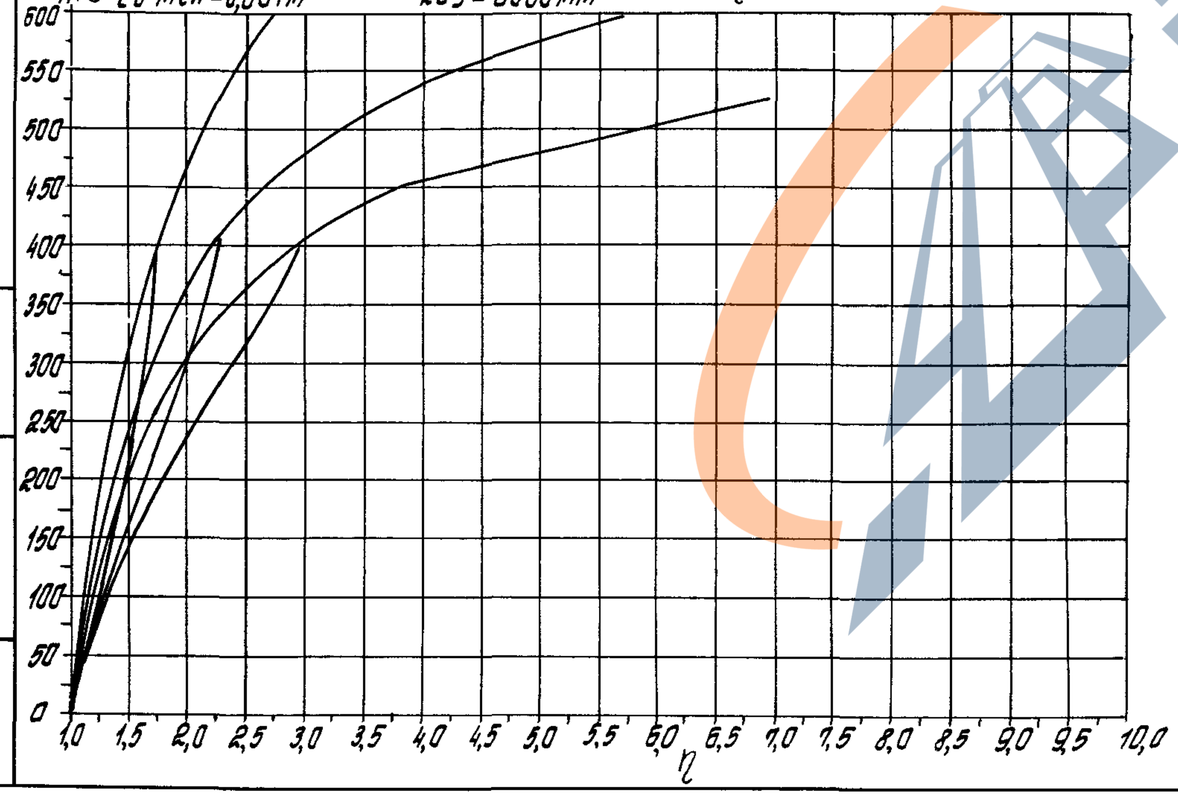

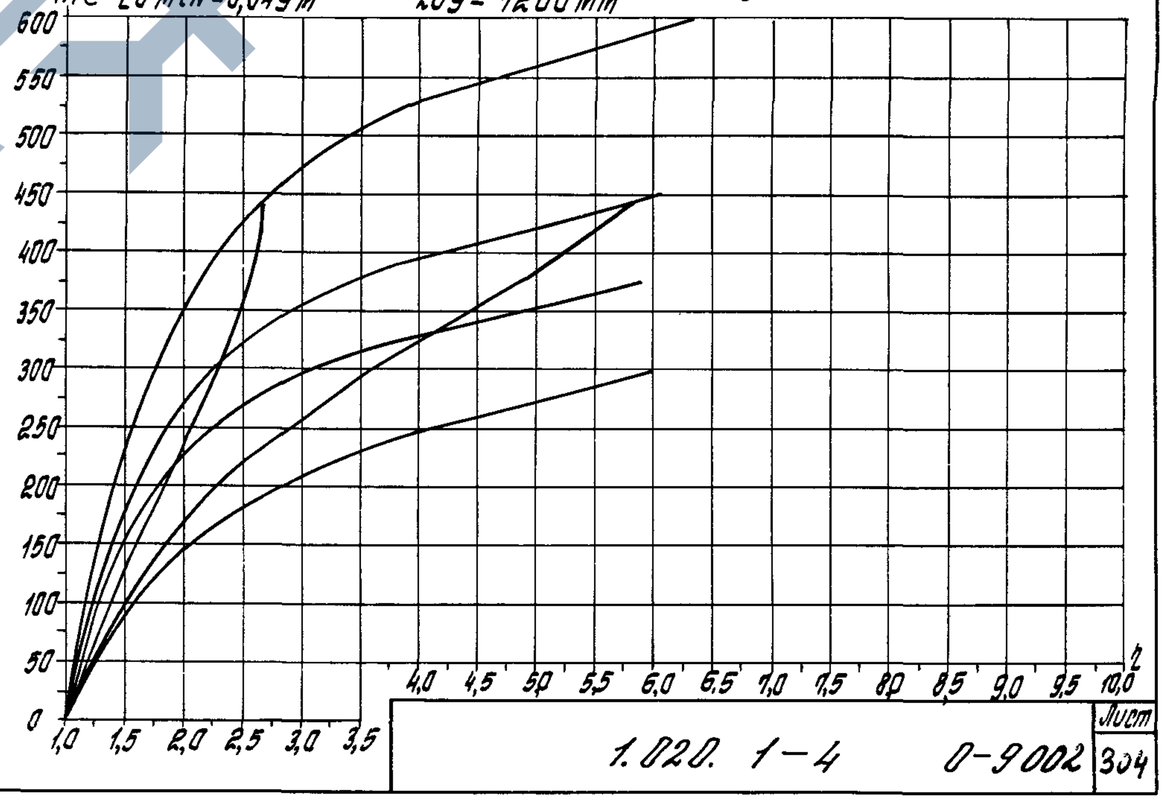

Инв.№подл. | Подпись и дата | Взам.инв.№

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24166-03 81

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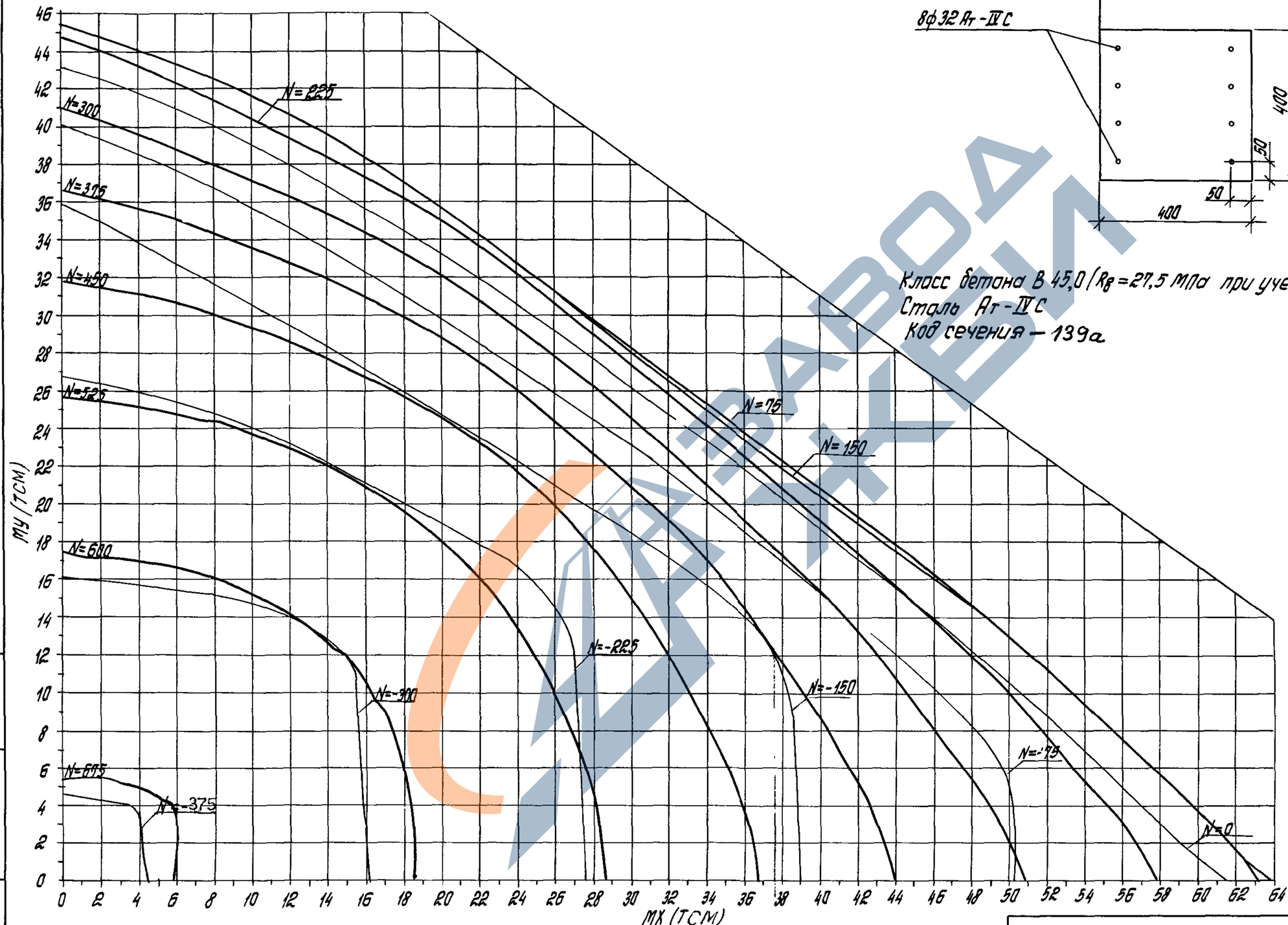

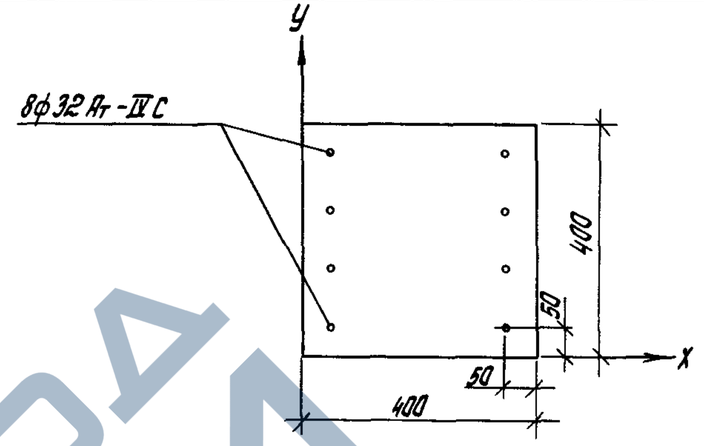

Класс бетона В 45,0 ($R_в$ = 27,5 МПа при учете $\gamma_{в2}$ = 1,10)
Сталь Ат-IV С
Код сечения — 139а

Инв. № подл.	Подпись и дата	Взам. инв. №

1.020. 1-4	0-9 002	Лист 305

24166-03 82

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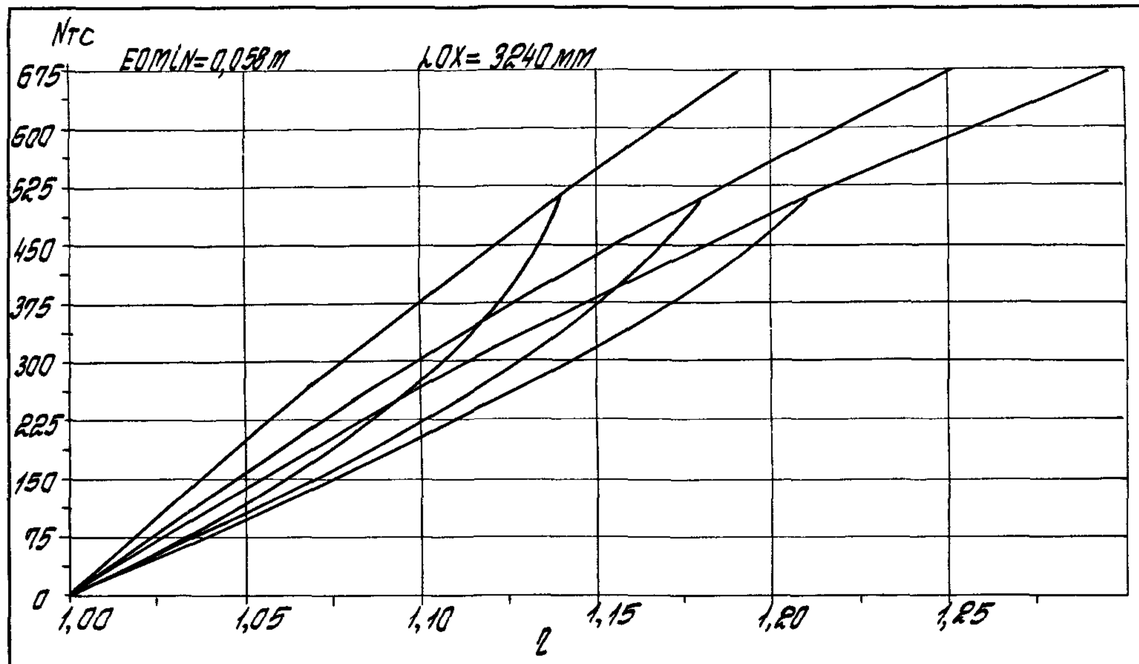

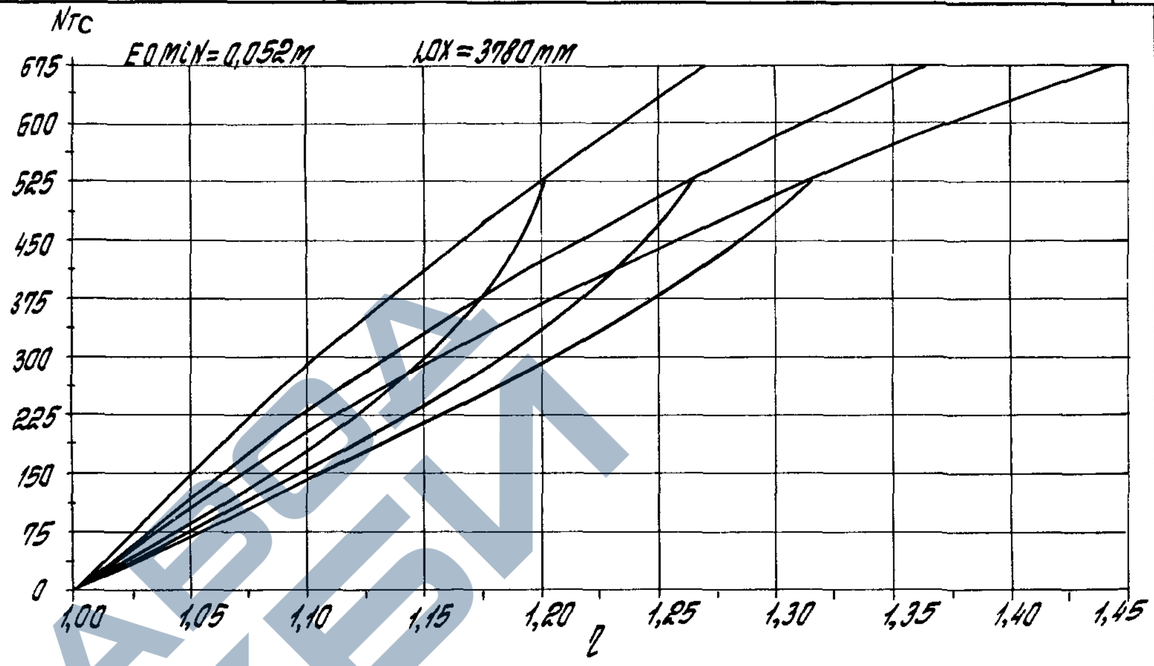

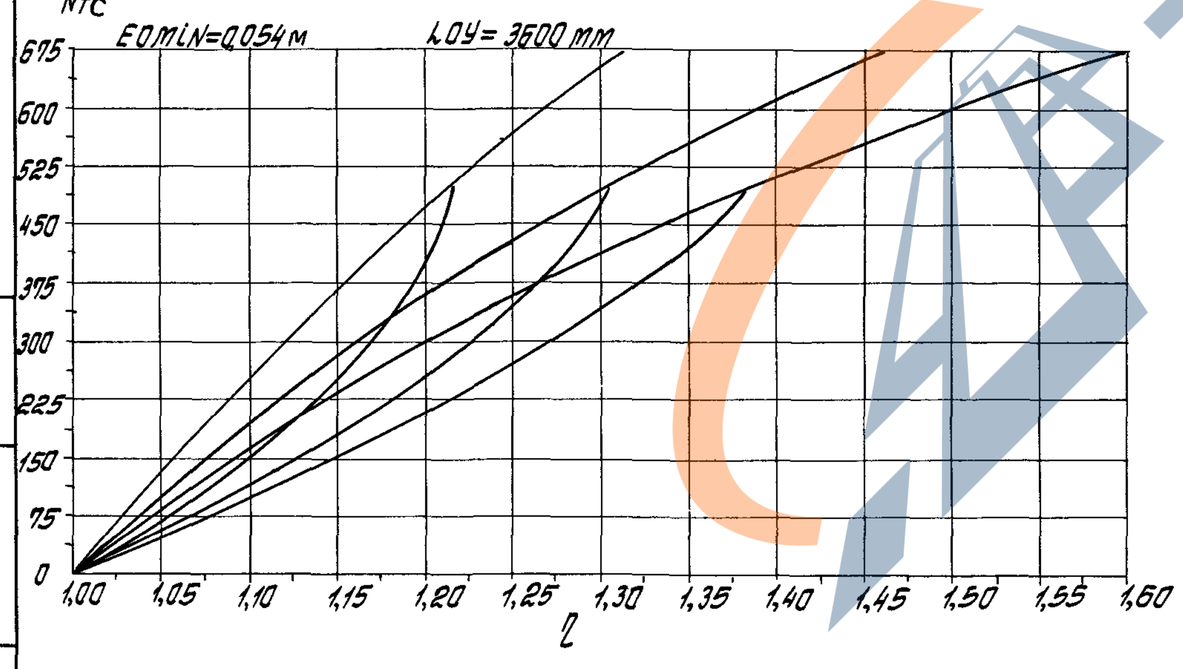

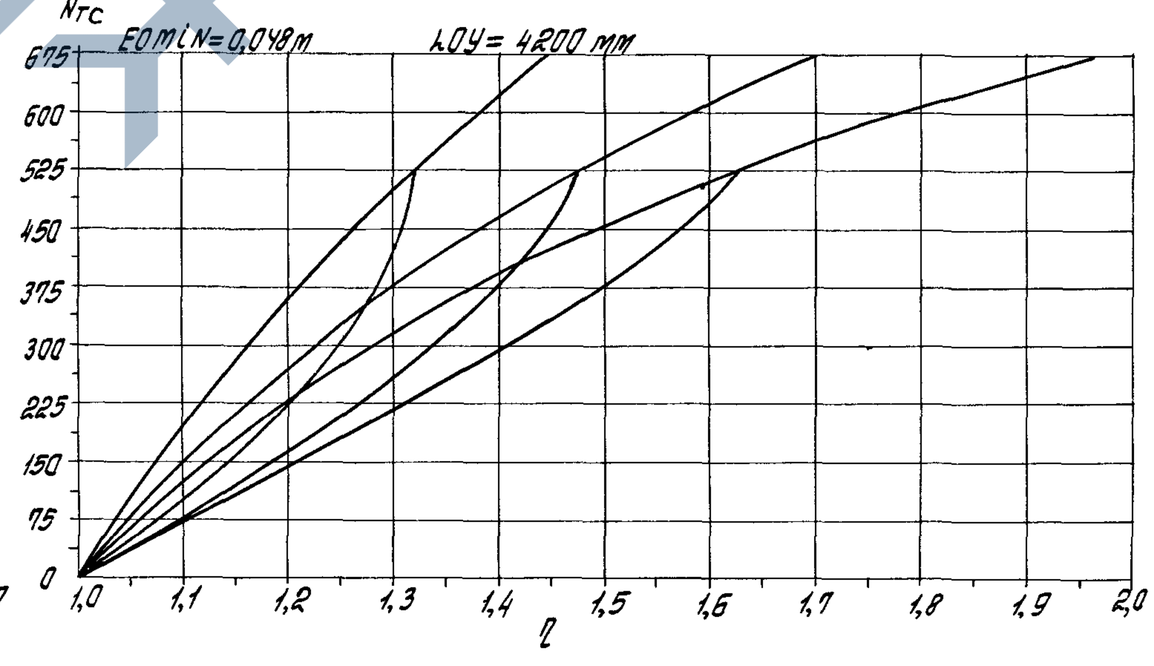

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24166-03 89

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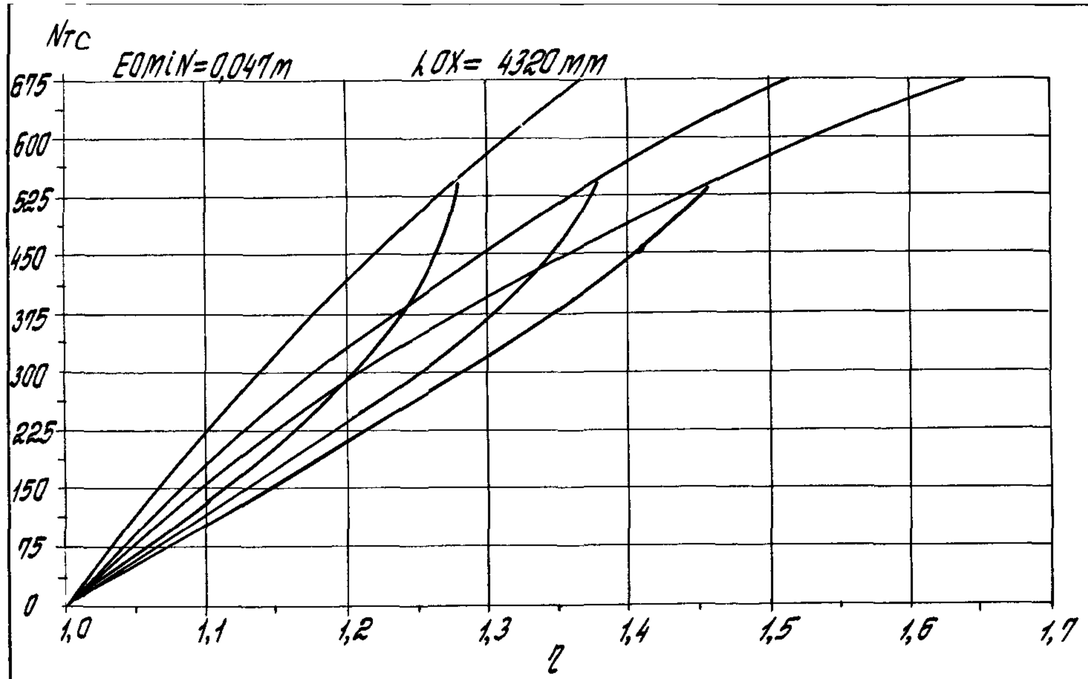

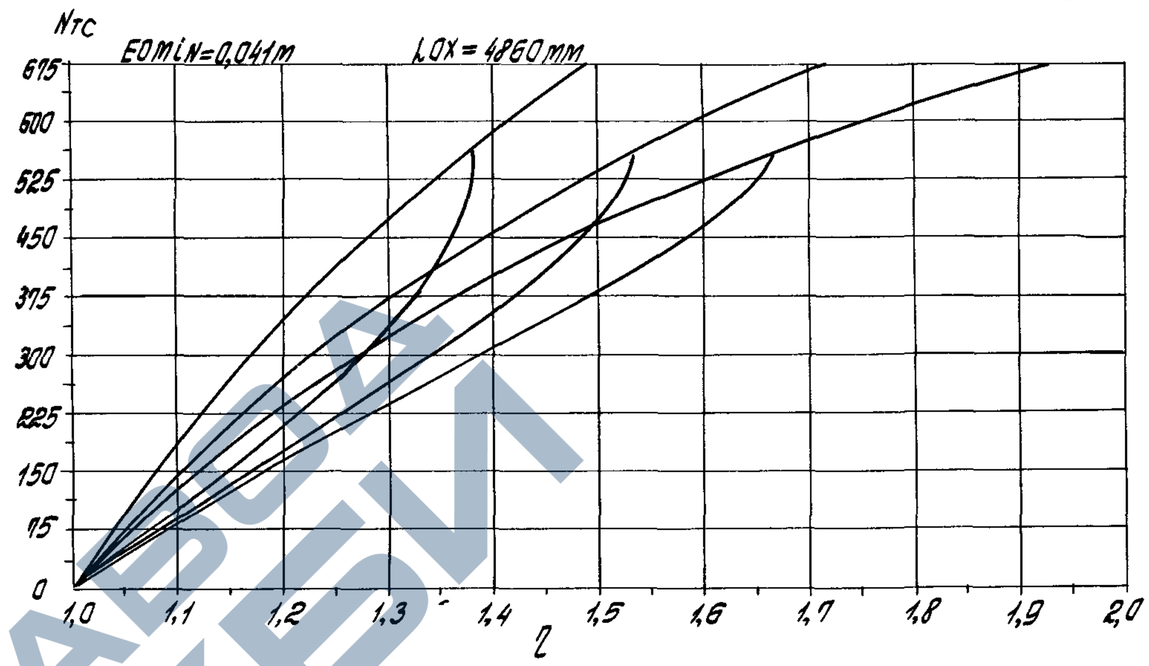

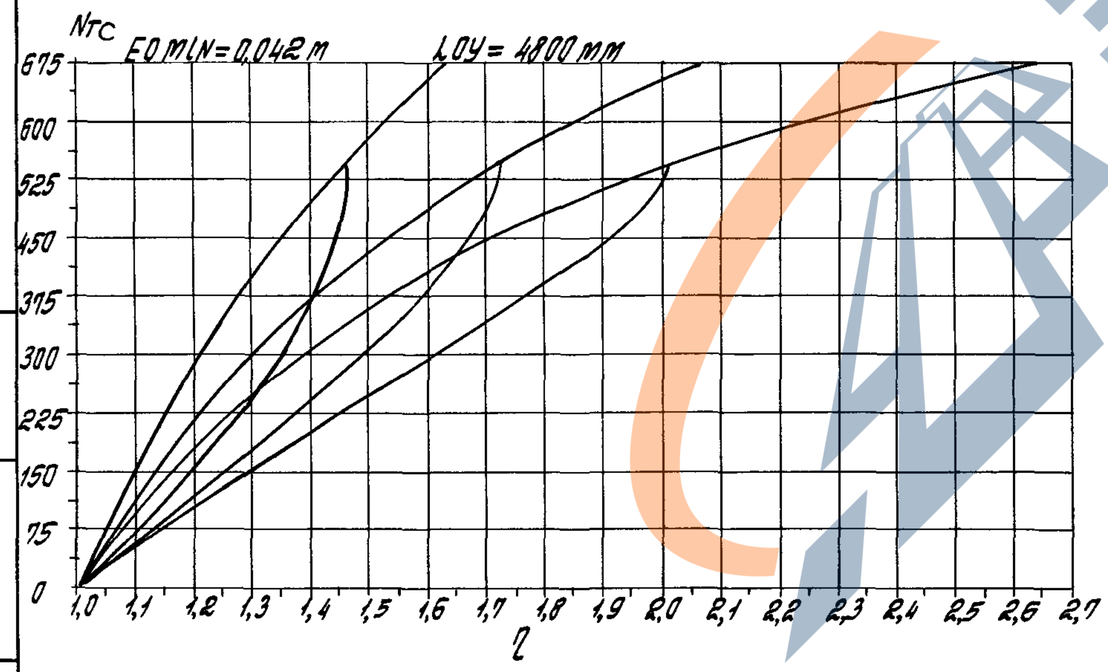

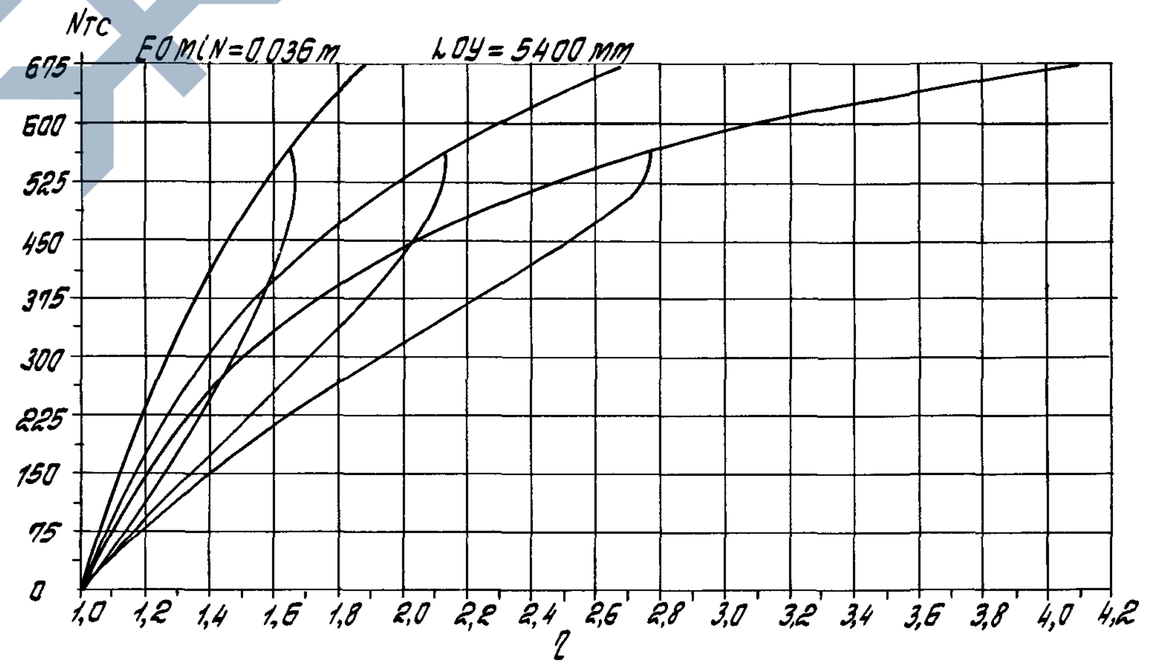

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4	0-9002	Лист 307

24166-03 84

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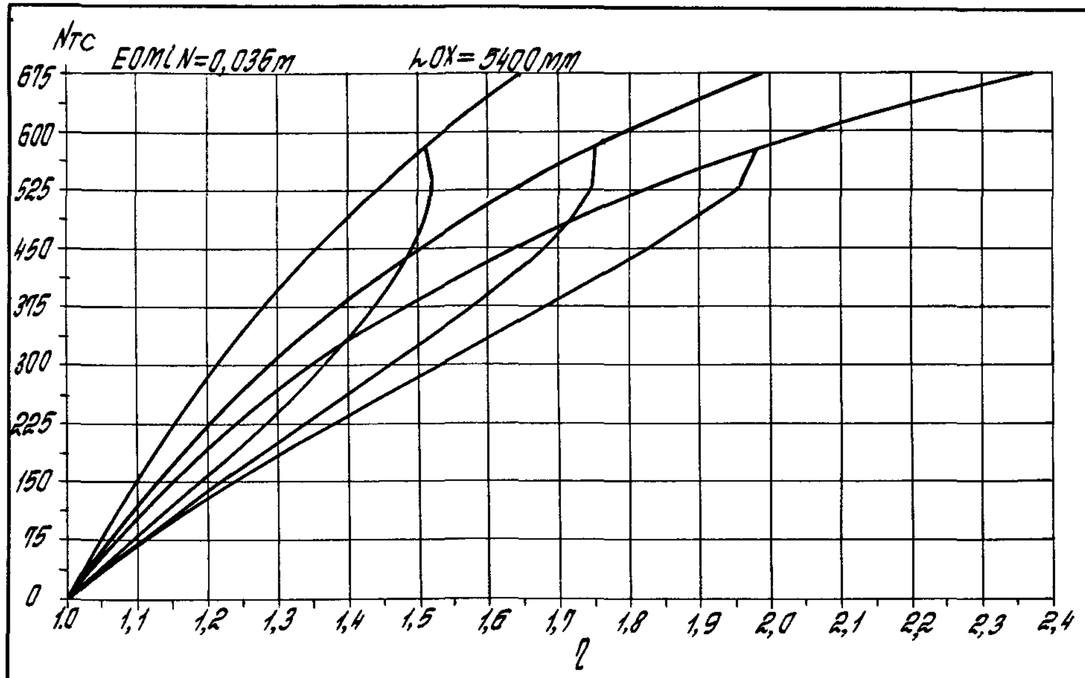

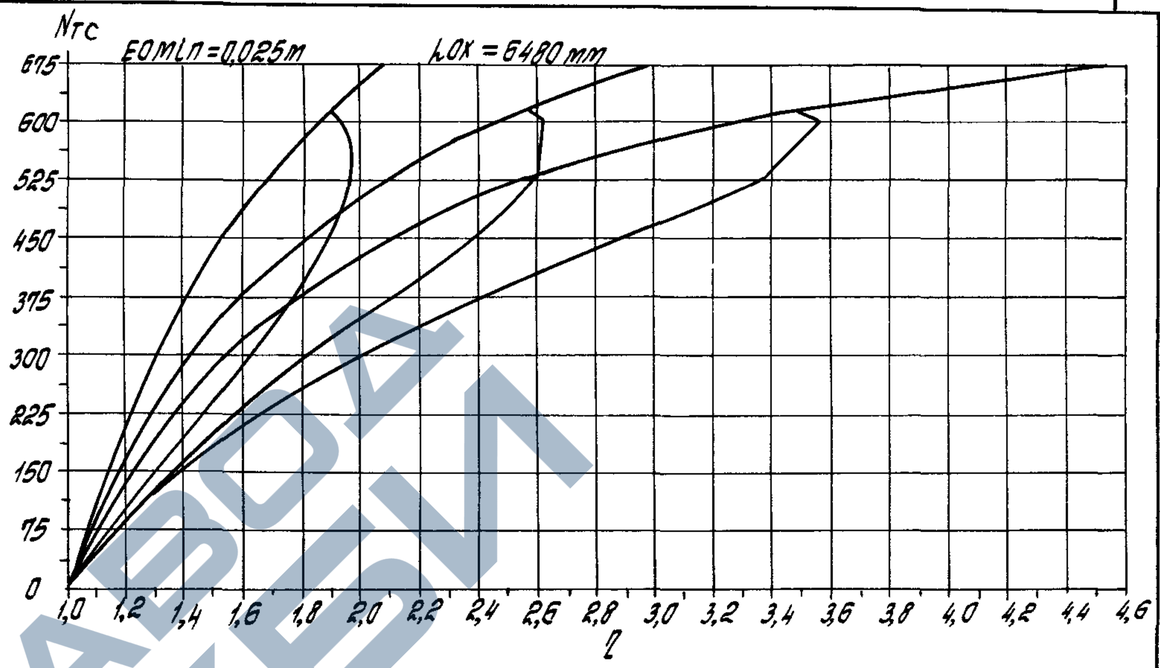

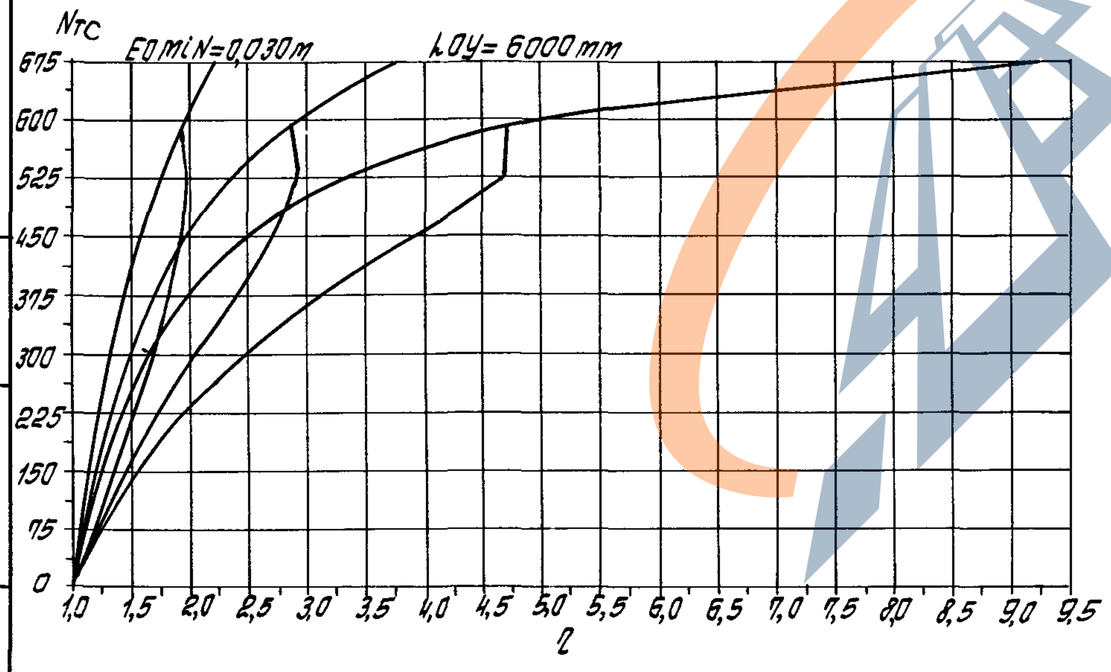

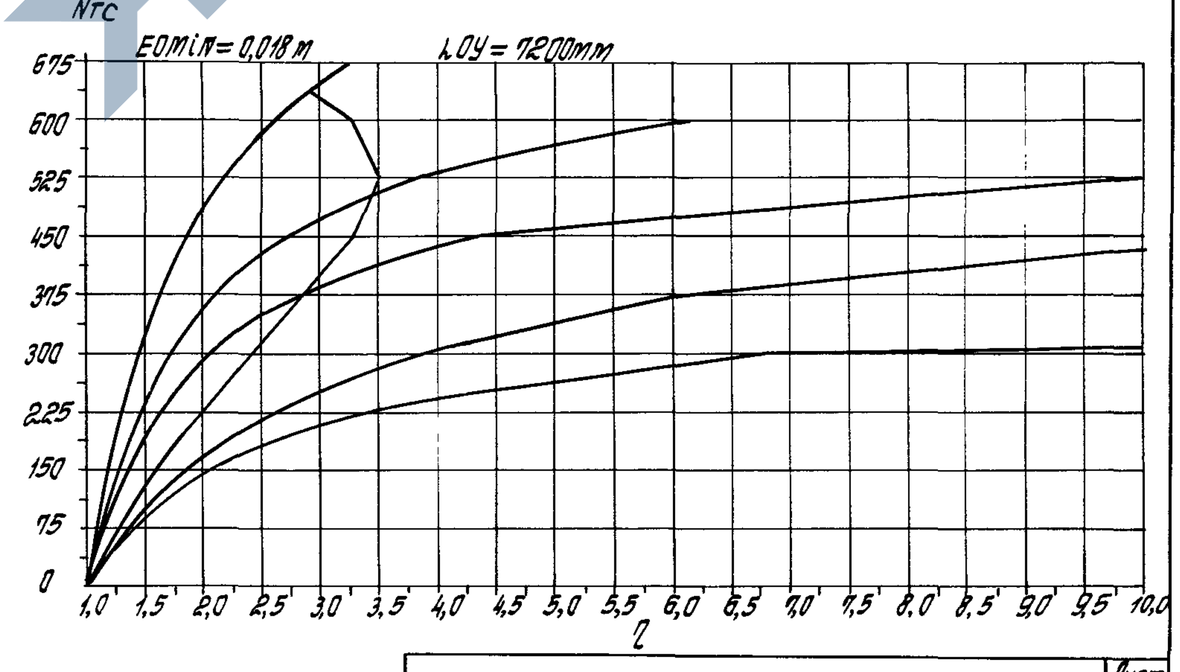

Инв.№ подл. | Подпись и дата | Взам.инв.№

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Лист 308

24166-03 85

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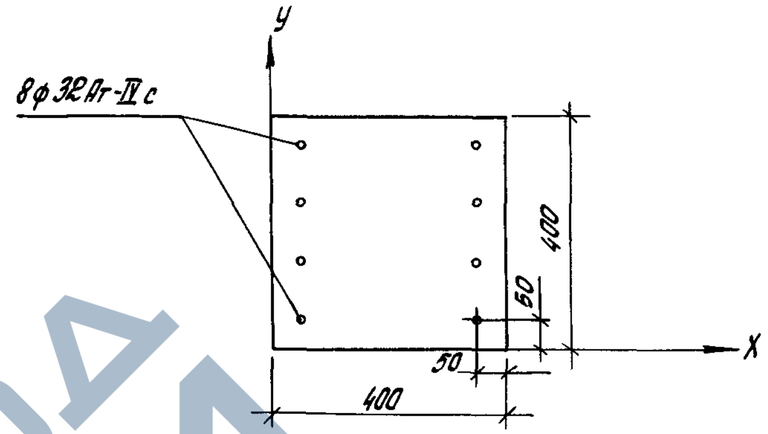
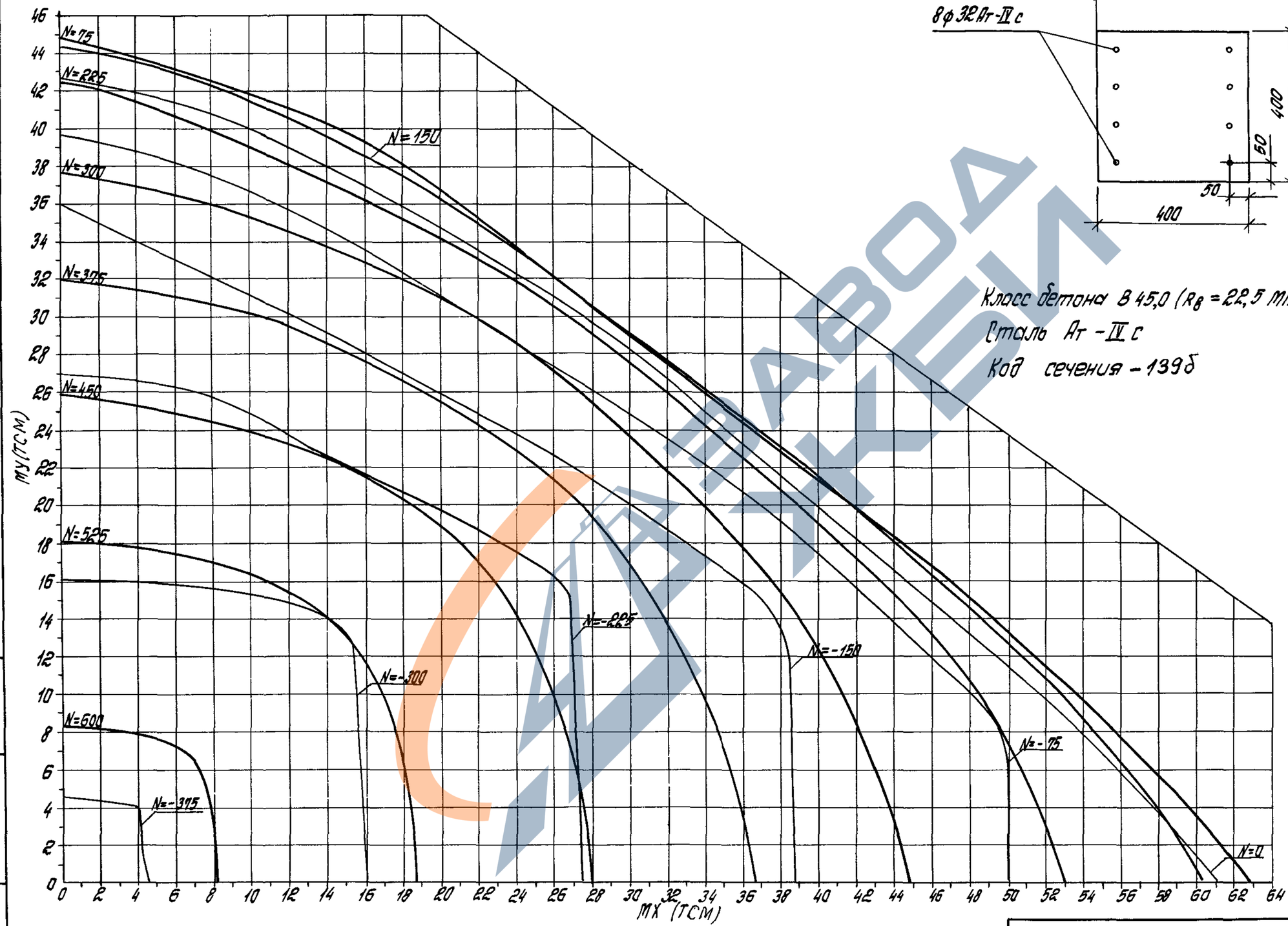


Класс бетона В 45,0 ($R_в$ = 22,5 МПа при учете $\gamma_{в2}$ = 0,90)

Сталь Ат - IV с

Код сечения - 1398



ЗАВОД ЖБИ

Инв.№ подл. | Подпись и дата | Взам. инв.№

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24166-03 86

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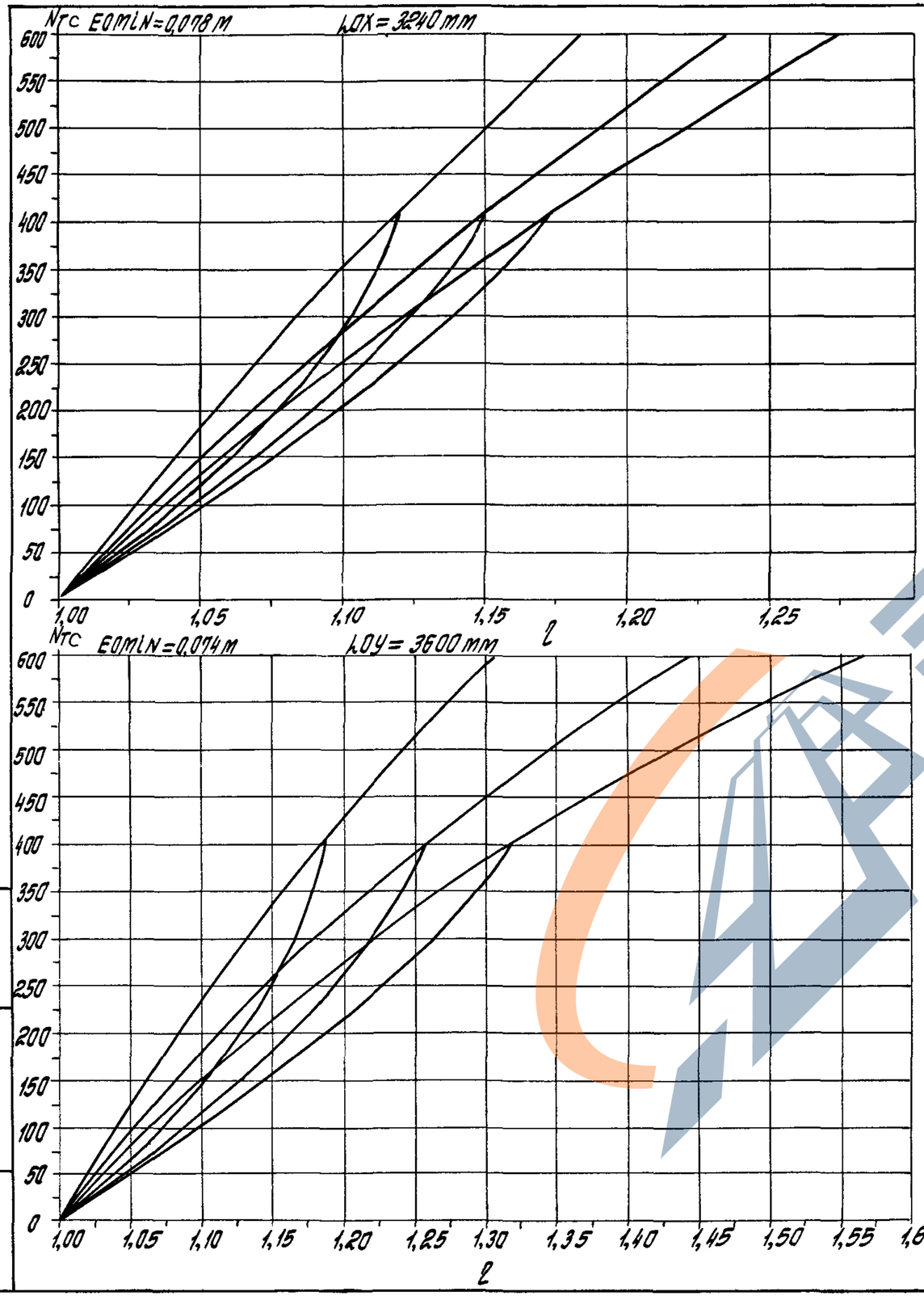

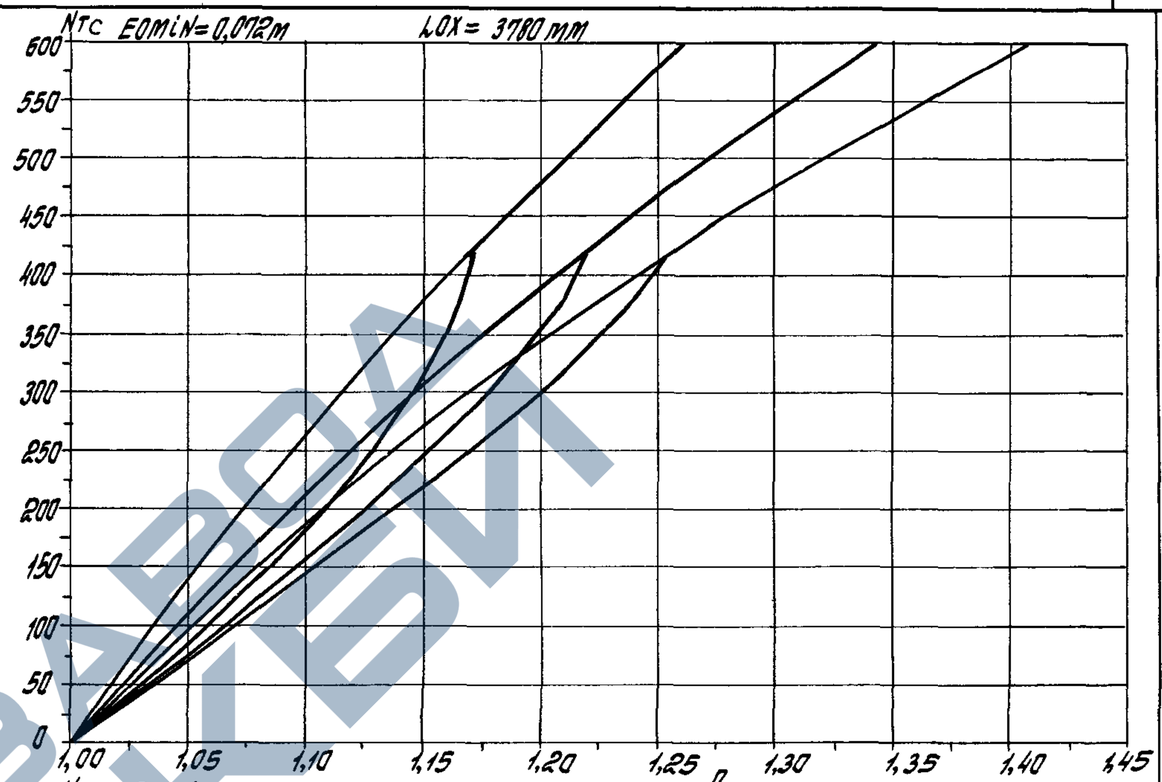

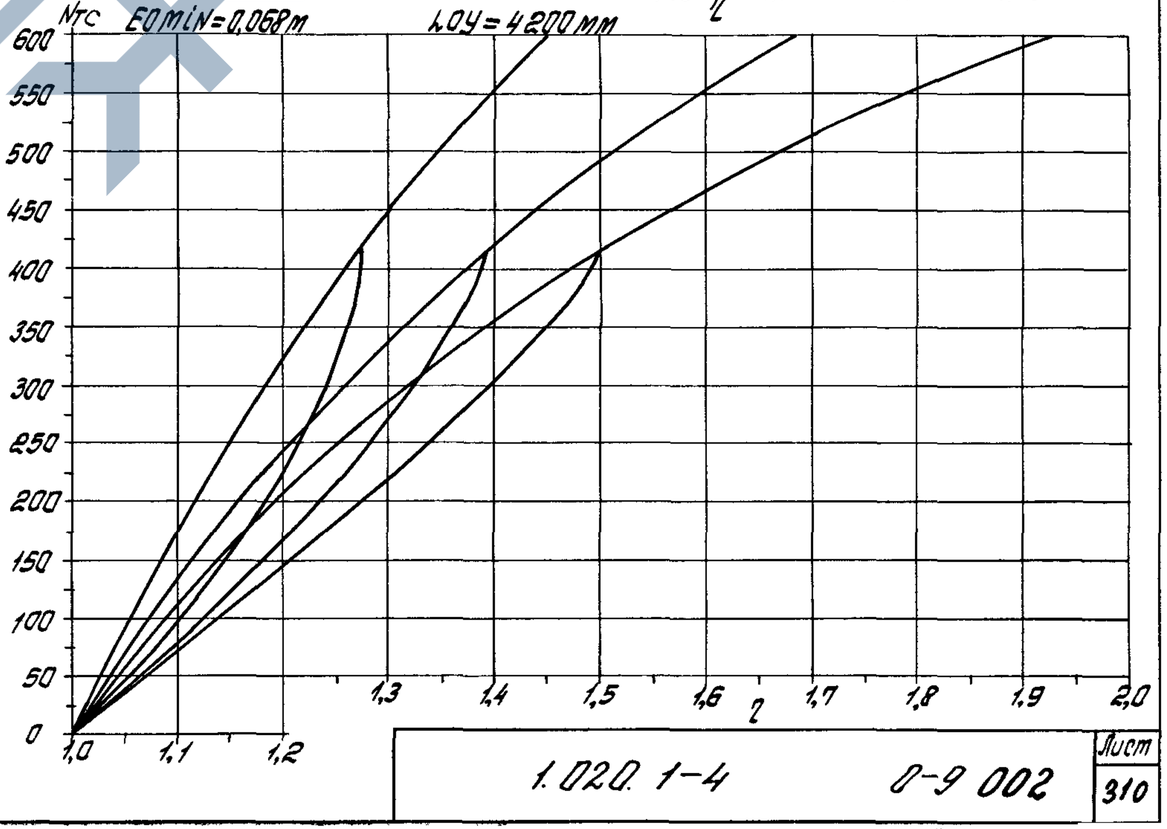

Инв. № подл. | Подпись и дата | Взам. инв. №

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Лист 310

24166-03 87

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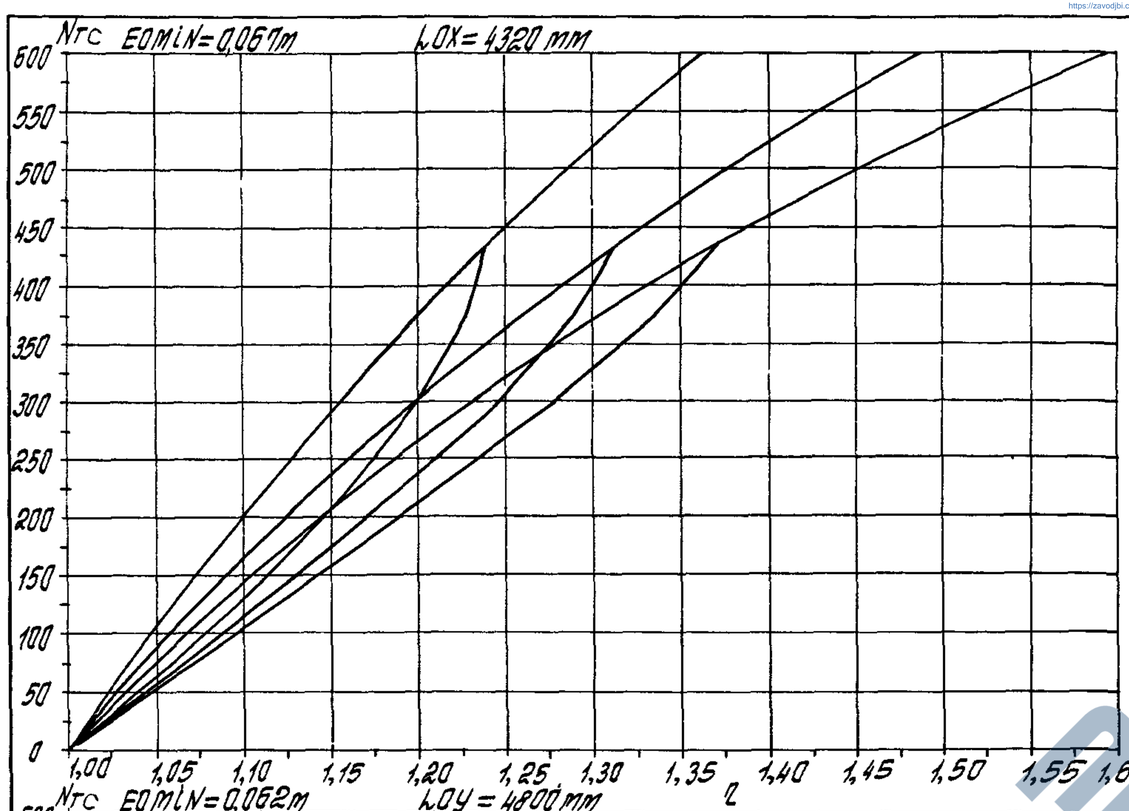
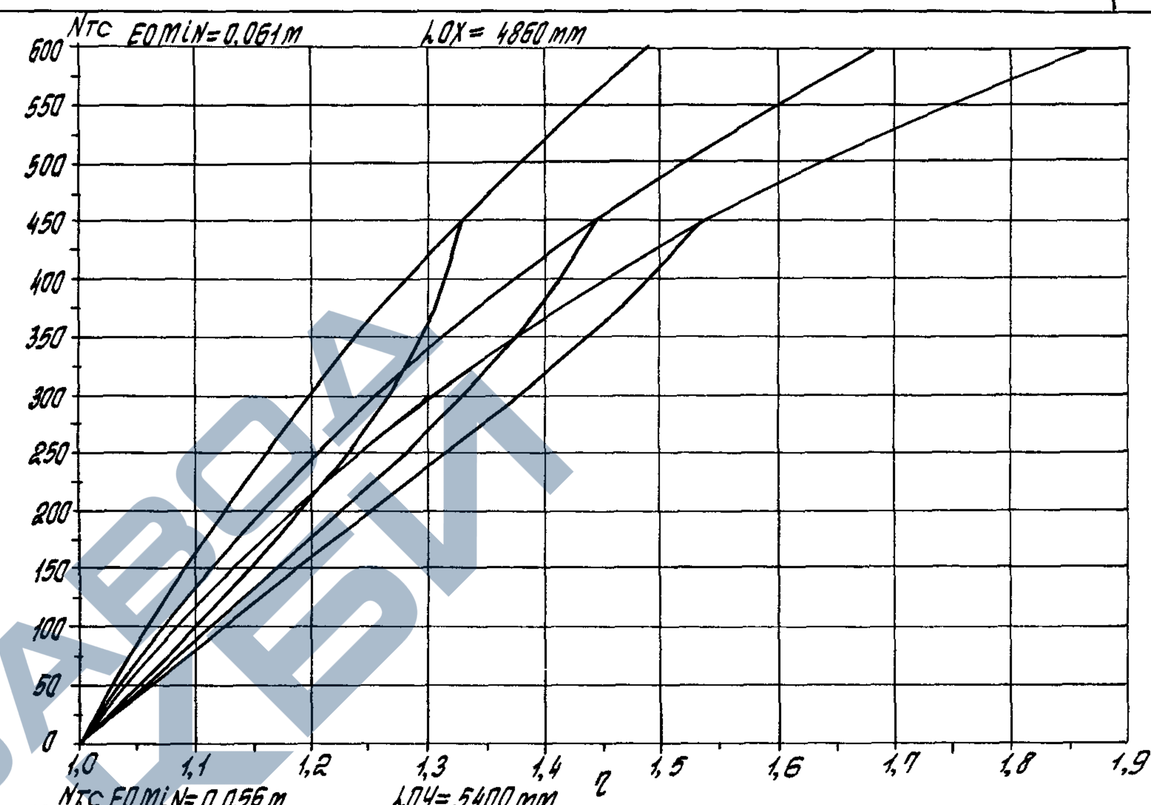
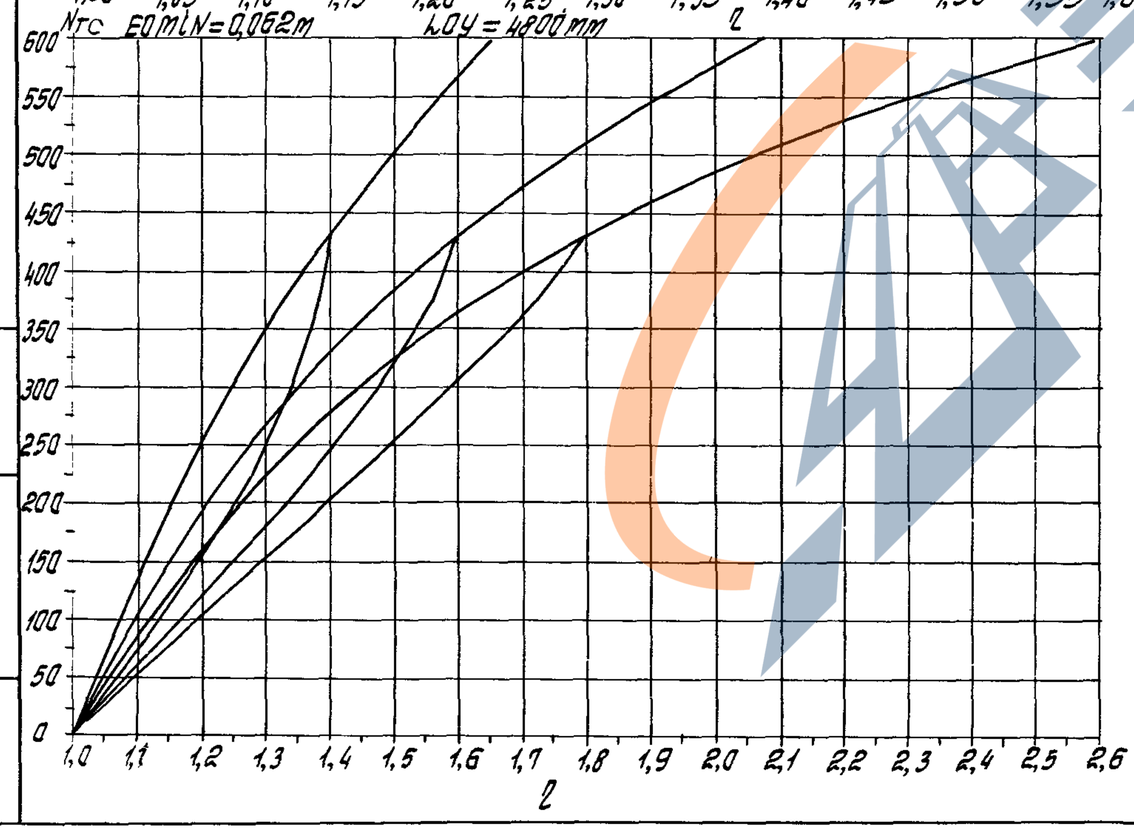
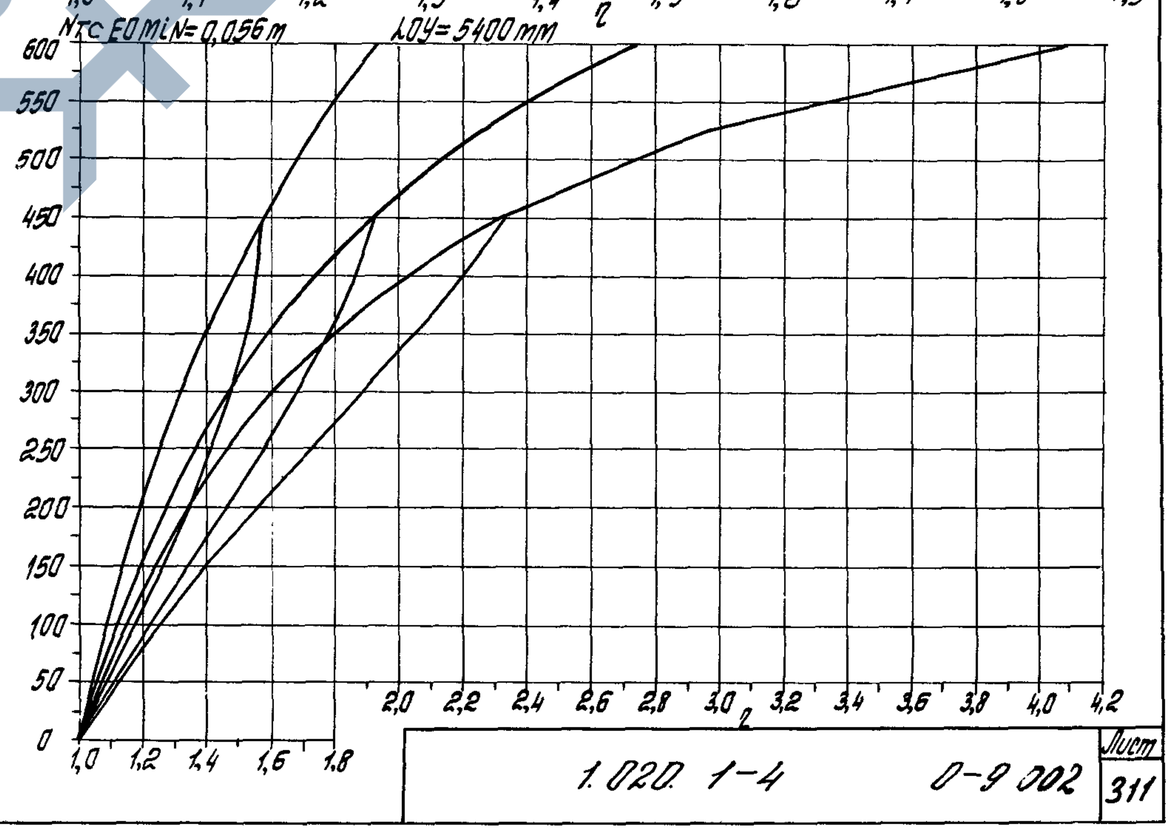
https://zavodjbi.com/









Инв.№ подл. | Подпись и дата | Взам. инв.№

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Лист 311

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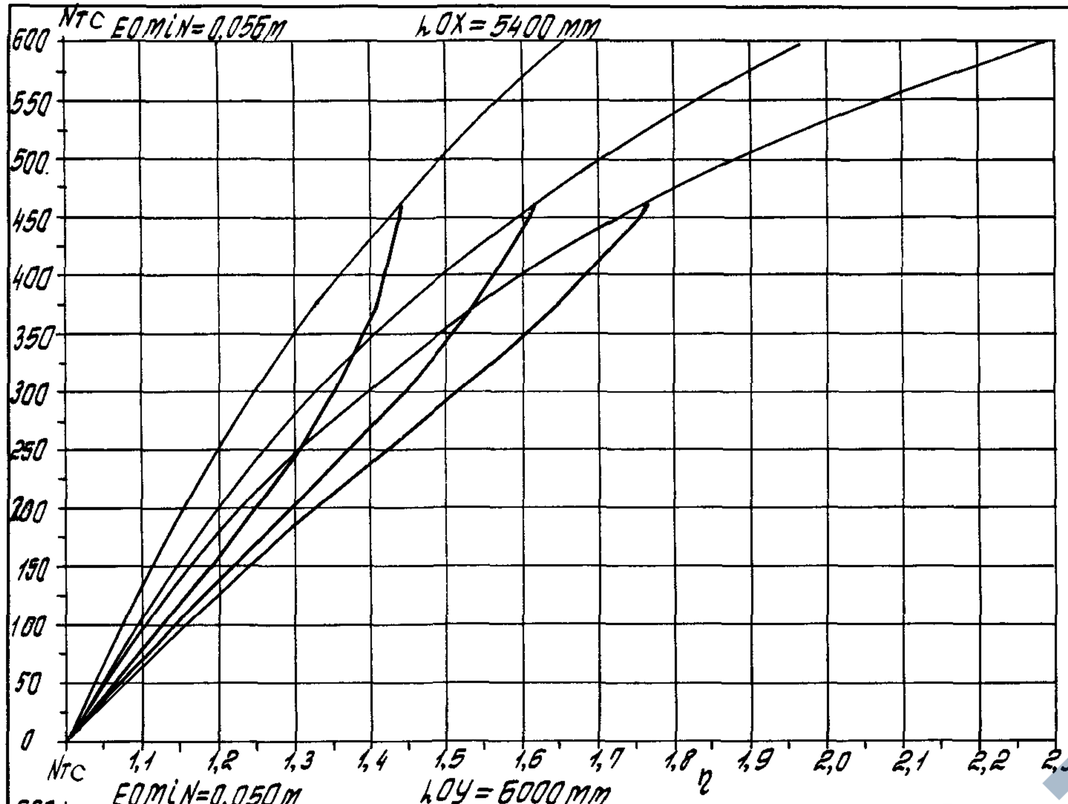

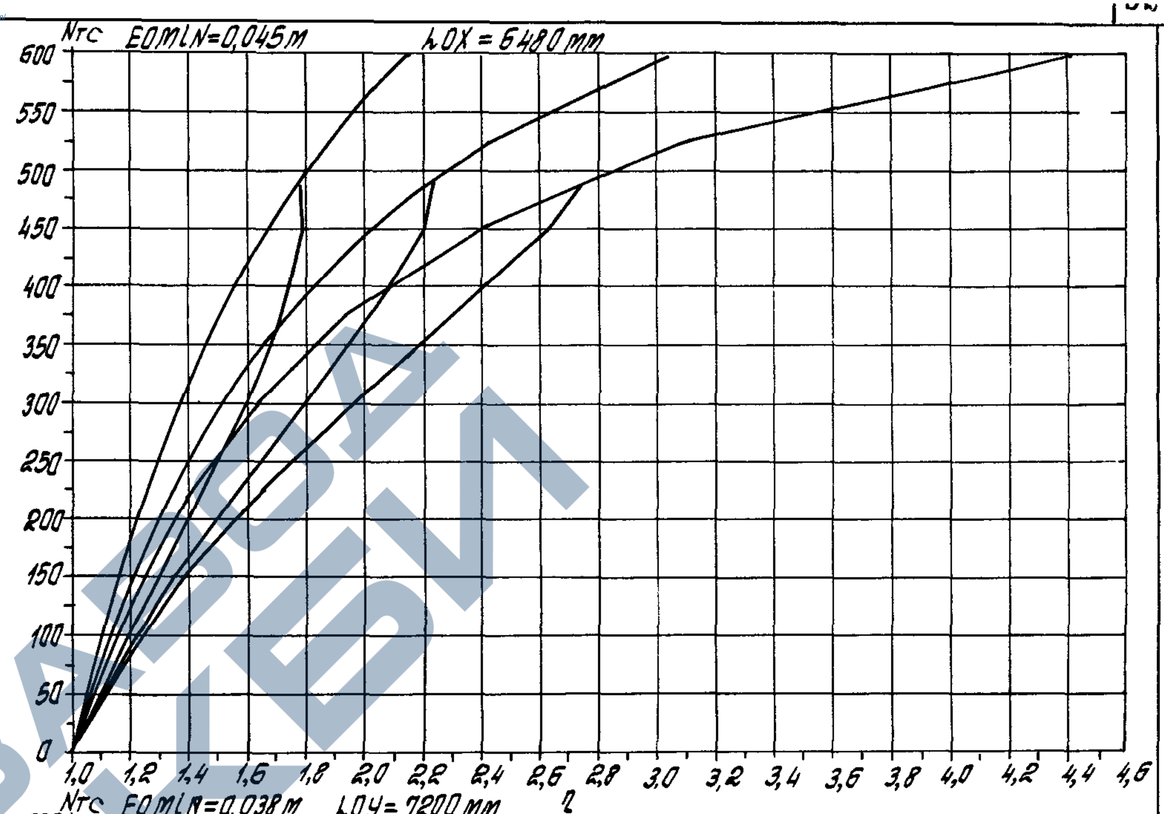

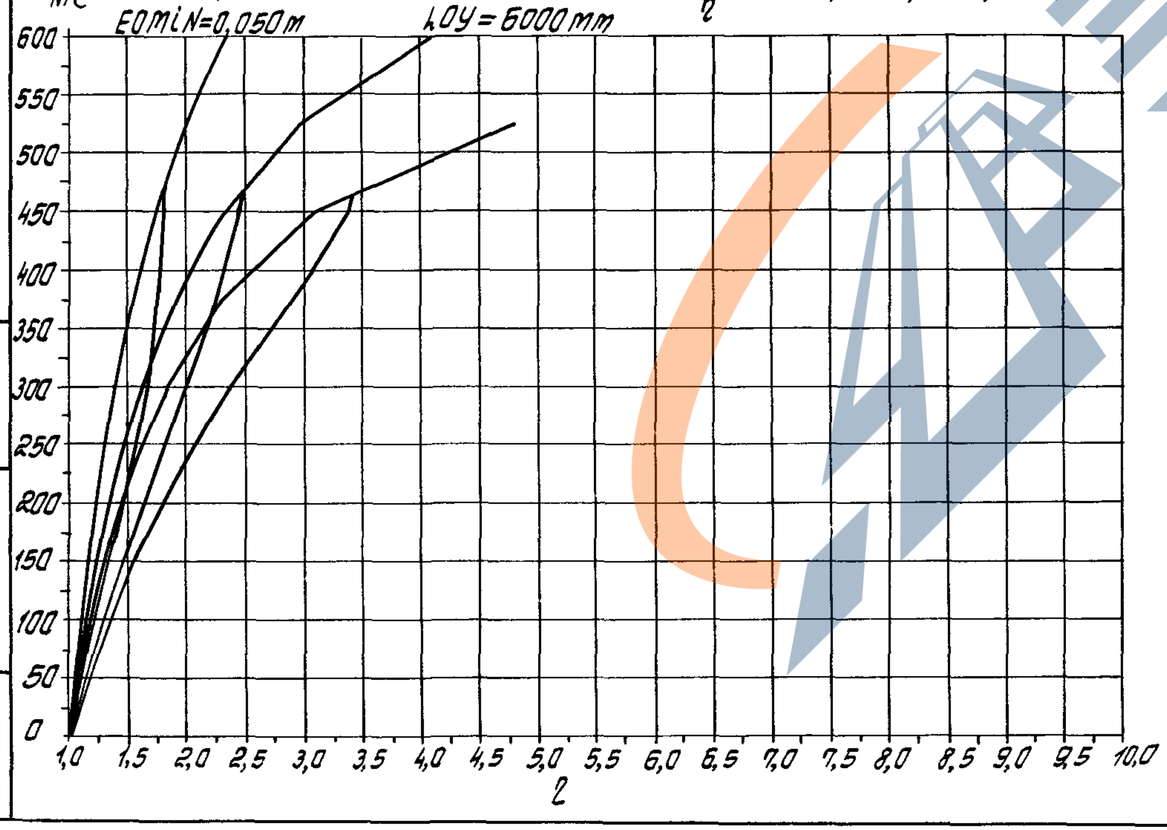

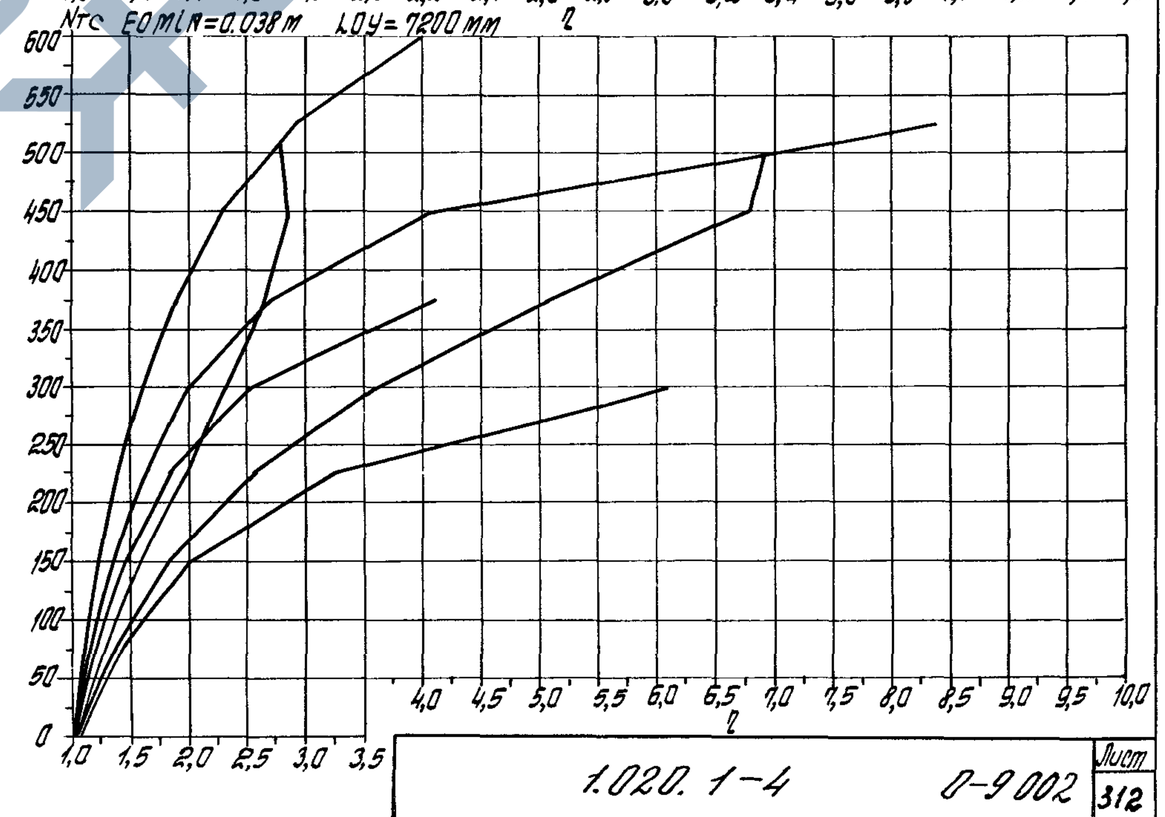

Инв.№ подл. | Подпись и дата | Взам.инв.№

1.020.1-4 0-9002

Лист 312

24166-03 АО

ЗАВОДА ЭЛЕКТРО
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Рис. 1

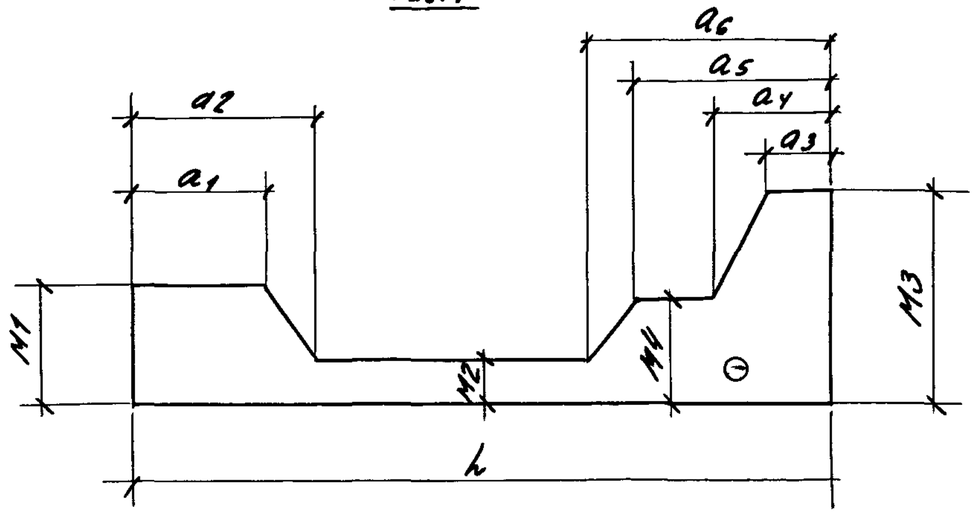


Рис. 2

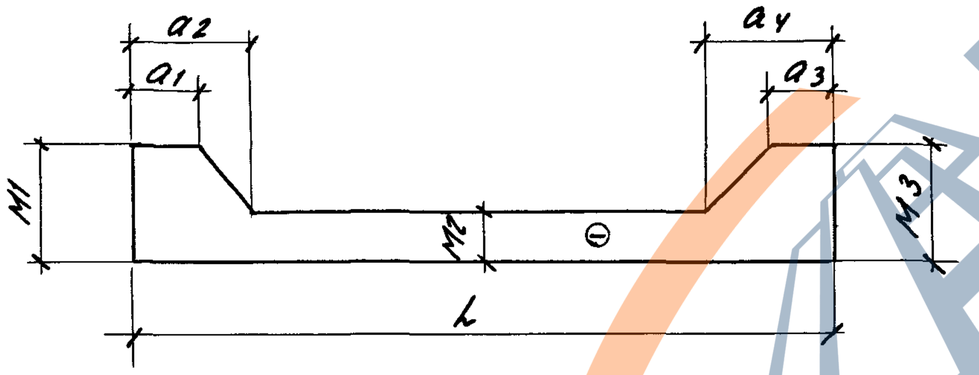
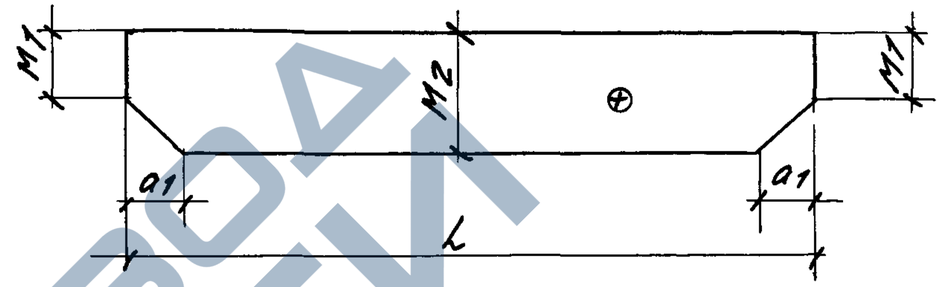


Рис. 3



1. Эпюры на рис. 1-3 рассматривать совместно с табл. 1 на листах
2. Приведенные эпюры соответствуют предельно допустимым изгибающим моментам: в числителе - от расчетной нагрузки, определенным с учетом работы наклонных сечений по изгибающему моменту, предельного раскрытия трещин от постоянных и длительных нагрузок, а также с учетом перераспределения (20%) опорных изгибающих моментов, полученных в упругой стадии в знаменателе - от нормативных постоянных и длительных нагрузок с учетом предельного раскрытия трещин, соответствующих слабо-агрессивной среде.
3. Знак „минус": на эпюрах соответствует действию момента, растягивающего верхнюю грань ригеля, знак „плюс" - растягивающего нижнюю грань ригеля.
4. Длина эпюры L соответствует расстоянию между гранями колонн.

				1.020.1-4 0-9 003	
Нач. отд	Кобыш			Эпюры несущих способностей по изгибающим моментам для ригелей.	Стадия: Р; Лист: 1; Листов: 3
ГИП	Никитин				ЦНИИПРОМЗДАНИЙ
ГИП	Клебанов				
ГИП	Валенкова				
Исполн.	Котова				

Инв. № подл. | Подпись и дата | Взам. инв. №

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Таблица 1

Марка ригеля	L (м)	Параметры эпюр предельных изгибающих моментов *)														Рис.	Mi, тсм		ai, м
		Рис.	Моменты Mi, тс.м					Расстояния ai, м											
			M1	M2	M3	M4		a1	a2	a3	a4	a5	a6				M1	M2	
1РДР6.56 – 50 АтV-К	5,6	1	26,1 / 7,3	4,4	34,0 / 11,9	10,2 / 6,6		0,7	1,6	0,1	1,2	1,8	2,5	3	21,1	28,5	0,7		
1РДР6.56 – 50 АIV-К																31,5			
1РДР6.56 – 70 АтV-К			26,1 / 7,3	4,4	34,0 / 11,9	10,2 / 6,6		0,8	1,6	0,2	1,3	2,0	2,5			28,5			
1РДР6.56 – 70 АIV-К																31,5			
1РДР6.56 – 90 АтV-К			29,6 / 10,1	4,4	53,5 / 17,0	18,7 / 9,0		0,8	1,7	0,4	1,3	1,7	2,5			28,5			
1РДР6.56 – 90 АIV-К																31,5			
1РДР6.56 – 110 АтV-К			37,6 / 13,7	6,5	62,0 / 24,3	27,0 / 13,5		0,7	1,5	0,7	1,5	1,7	2,5			35,2			
1РДР6.56 – 110 АIV-К																35,0			
1РДР6.56 – 145 АтV-К			37,0 / 13,7	8,8	62,0 / 24,3	29,3 / 13,5		1,0	1,7	1,0	1,7	1,7	2,4			41,0			
1РДР6.56 – 145 АIV-К																41,8			
1РДР6.56 – 50 АтV-С		2	34,0 / 11,9	14,6 / 6,6	34,0 / 11,9	–		0,2	1,3	0,2	1,3	–	–	3	21,1	18,8	0,7		
1РДР6.56 – 50 АIV-С																18,8			
1РДР6.56 – 70 АтV-С			34,0 / 17,0	14,6 / 6,6	34,0 / 17,0	–		0,4	1,3	0,4	1,3	–	–			23,0			
1РДР6.56 – 70 АIV-С																22,4			
1РДР6.56 – 90 АтV-С			53,5 / 17,0	18,5 / 9,0	53,5 / 17,0	–		0,4	1,3	0,4	1,3	–	–			31,0			
1РДР6.56 – 90 АIV-С																29,8			
1РДР6.56 – 110 АтV-С			62,0 / 24,3	27,0 / 13,5	62,0 / 24,3	–		0,7	1,5	0,7	1,5	–	–			32,8			
1РДР6.56 – 110 АIV-С																33,1			
1РДР6.56 – 145 АтV-С			62,0 / 24,3	27,0 / 13,5	62,0 / 24,3	–		0,8	1,5	0,8	1,5	–	–			43,9			
1РДР6.56 – 145 АIV-С																43,3			
1РДР6.56 – 30 АтV-Д		2	26,1 / 7,3	27,2 / 7,3	26,1 / 7,3	–		–	–	–	–	–	–	3	22,0	32,8	0,7		
1РДР6.56 – 30 АIV-Д																33,1			
1РОР6.56 – 30 АтV																32,8			
1РОР6.56 – 30 АIV																33,1			
1РДР6.56 – 60 АтV-Д			53,5 / 17,0	37,8 / 17,0	53,5 / 17,0	–		0,7	1,2	0,7	1,2	–	–			32,8			
1РДР6.56 – 60 АIV-Д																34,2			
1РОР6.56 – 60 АтV																33,8			
1РОР6.56 – 60 АIV																34,2			
1РДР6.56 – 100 АтV-Д			62,0 / 24,3	29,0 / 21,7	62,0 / 24,3	–		0,6	1,3	0,6	1,3	–	–			44,1			
1РДР6.56 – 100 АIV-Д																43,3			
1РОР6.56 – 100 АтV																44,1			
1РОР6.56 – 100 АIV																43,3			

*) Приведенные параметры относятся также к ригелям под многопустотные плиты марок 1РДП и 1РОП

Инв. № подл. | Подпись и дата | Взам. инв. №

1.020.1-4 0-9 003

Лист 2

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Таблица 2

Марка ригеля	Рис.	Несущая способность по Q, тс					Предельные значения $A = T + \frac{Qв}{2}$ тсм		
		Q_1	Q_2	Q_3	Q_4	Q_5	A_1	A_2	A_3
1РДР6.56 – 50 $A_{T}\overline{V}$-к	1; 2	65,1	47,7	32,5	26,3	20,3	3,5	2,3	0,9
1РДР6.56 – 50 $A_{I}\overline{V}$-к									
1РДР6.56 – 70 $A_{T}\overline{V}$-к		65,1	52,1	38,9	31,3	21,9	5,7	3,8	1,5
1РДР6.56 – 70 $A_{I}\overline{V}$-к									
1РДР6.56 – 90 $A_{T}\overline{V}$-к		65,1	52,1	38,9	31,3	21,9	5,4	3,6	1,4
1РДР6.56 – 90 $A_{I}\overline{V}$-к									
1РДР6.56 – 110 $A_{T}\overline{V}$-к		65,1	58,1	43,8	35,9	22,3	8,0	5,3	2,1
1РДР6.56 – 110 $A_{I}\overline{V}$-к									
1РДР6.56 – 145 $A_{T}\overline{V}$-к		76,6	65,5	52,9	43,7	25,3	11,1	7,4	3,0
1РДР6.56 – 145 $A_{I}\overline{V}$-к									
1РДР6.56 – 50 $A_{T}\overline{V}$-с		65,1	47,7	32,5	26,3	20,3	3,5	2,3	0,9
1РДР6.56 – 50 $A_{I}\overline{V}$-с									
1РДР6.56 – 70 $A_{T}\overline{V}$-с		65,1	52,1	38,9	31,3	21,9	5,7	3,8	1,5
1РДР6.56 – 70 $A_{I}\overline{V}$-с									
1РДР6.56 – 90 $A_{T}\overline{V}$-с		65,1	52,1	38,9	31,3	21,9	5,4	3,6	1,4
1РДР6.56 – 90 $A_{I}\overline{V}$-с									
1РДР6.56 – 110 $A_{T}\overline{V}$-с		65,1	58,1	43,8	35,9	22,3	8,0	5,3	2,1
1РДР6.56 – 110 $A_{I}\overline{V}$-с									
1РДР6.56 – 145 $A_{T}\overline{V}$-с		76,6	65,5	52,9	43,7	25,3	11,1	7,4	3,0
1РДР6.56 – 145 $A_{I}\overline{V}$-с									

Марка ригеля	Рис.	Несущая способность по Q, тс					Рис.	Предельные значения $A = T + \frac{Qв}{2}$ тсм, при $T \geq \frac{Qв}{2}$		
		Q_1	Q_2	Q_3	Q_4	Q_5		A_1	A_2	A_3
1РДР6.56 – 30 $A_{T}\overline{V}$-д	1	24,2	13,2	11,2	8,5	4,7	2	9,0	6,0	2,7
1РДР6.56 – 30 $A_{I}\overline{V}$-д										
1РОР6.56 – 30 $A_{T}\overline{V}$										
1РОР6.56 – 30 $A_{I}\overline{V}$										
1РДР6.56 – 60 $A_{T}\overline{V}$-д		33,7	18,1	15,6	11,6	5,9		11,6	7,7	3,3
1РДР6.56 – 60 $A_{I}\overline{V}$-д										
1РОР6.56 – 60 $A_{T}\overline{V}$										
1РОР6.56 – 60 $A_{I}\overline{V}$										
1РДР6.56 – 100 $A_{T}\overline{V}$-д		45,4	24,2	20,9	15,2	8,1		11,6	7,7	3,3
1РДР6.56 – 100 $A_{I}\overline{V}$-д										
1РОР6.56 – 100 $A_{T}\overline{V}$										
1РОР6.56 – 100 $A_{I}\overline{V}$										

Рис. 1

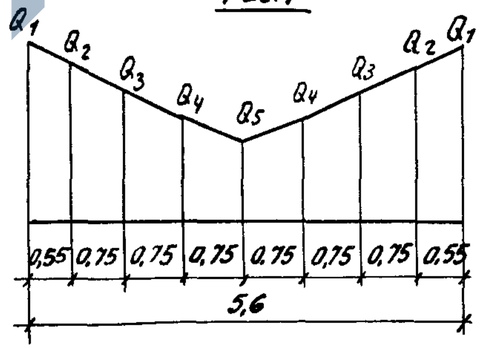
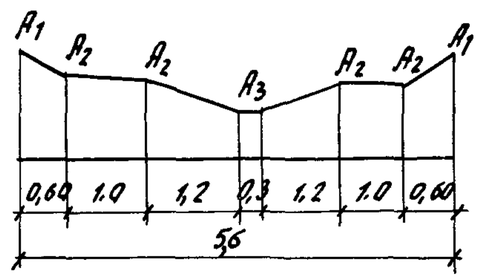


Рис. 2



Приведенные значения несущей способности относятся также к ригелям под многопустотные плиты марок 1РДП и 1РОП.

$A = T + \frac{Qв}{2}$, где T – крутящий момент в сечении; Q – действующая поперечная сила в сечении; $в$ – ширина сжатой зоны = 0,3 м. При этом T должен быть $> \frac{Qв}{2}$; при $T < \frac{Qв}{2}$, Q – сопоставляется с величиной $Q + \frac{3T}{2}$; при определении T учитывать коэффициент 0,7 в случае передачи нагрузки через плиты с замоноличиванием.

Инв. № подл. | Подпись и дата | Взам. инв. №

1.020. 1-4 0-9 003

Лист 3

24166-01 (92)

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